

## **Basin F Subregional Groundwater Model**

Edward Mazion, Jr., James H. May, Benita Abraham, and Maureen K. Corcoran

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## **Basin F Subregional Groundwater Model**

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## **Preface**

This study is a subregional numerical computer groundwater model of the Basin F Area of Rocky Mountain Arsenal (RMA). The study was conducted by the U.S. Army Engineer Research and Development Center (ERDC), Geotechnical and Structures Laboratory (GSL), for the Program Manager's Office, Rocky Mountain Arsenal, Colorado, and is part of the Detailed Analysis of Alternatives (DAA) of the Rocky Mountain Arsenal Feasibility Study (FS). This modeling effort was conducted before ERDC developed the Department of Defense Groundwater Modeling System (GMS). The GMS is widely used for visualizing and numerical modeling of complex groundwater problems.

This report was written by Captain Edward Mazion, Jr., EN, Dr. James H. May, Mrs. Benita Abraham, and Ms. Maureen K. Corcoran, GSL. It was completed under the supervision of Dr. Lillian D. Wakeley, Chief, Engineering Geology & Geophysics Branch, and Dr. Robert Hall, Chief, Geosciences and Structures Division, GSL. Dr. Michael J. O'Connor was Director, GSL.

The GSL gratefully acknowledges the helpful suggestions, constructive criticisms, and information provided by Dr. James W. Warner, Mr. C. Tamayo-Lara, and Dr. A. A. Abdel-Rahman, Civil Engineering Department, Colorado State University.

At the time of publication of this report, Dr. James R. Houston was Director of ERDC, and COL John W. Morris III, EN, was Commander and Executive Director.

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# 1 Introduction and Purpose

### **Purpose of Subregional Groundwater Modeling**

The groundwater flow system at Rocky Mountain Arsenal (RMA) is complex. To evaluate proposed remedial alternatives, interaction of the local groundwater flow system with the present contamination control systems must be understood. The purpose of this modeling effort is to provide a tool for evaluation and relative comparison of groundwater remedial alternatives. The model provides a method to assess the local groundwater impact of each remedial alternative. Results from the modeling effort will be used to compare the preliminary design of various remedial alternatives, and to allow general modification and reconfiguration of those designs to optimize their performance as part of the Detailed Analysis of Alternatives (DAA) of the Feasibility Study (FS).

### **General Description of Model Area**

The RMA is located in Commerce City, Colorado, and is shown in Figure 1. The model boundary is defined in bold outline in Figure 2 and encompasses approximately 3.6 square miles. Portions of the north and west boundaries of the model coincide with the North Boundary Containment Treatment System (NBCTS) and the Northwest Boundary Containment System (NWBCS), respectively.

Groundwater movement in the study area is difficult to predict. Most ground-water flow occurs within alluvial and eolian deposits, which are referred to as "alluvium" in this report. Underlying the alluvium is the Denver Fm, which generally consists of sands, silts and clays, and is commonly less permeable than the alluvium. In parts of the study area, the alluvium is unsaturated. The water table occurs within the upper portion of the Denver Fm in areas of unsaturated alluvium.

The direction of groundwater movement within the model area is generally from southeast to northwest. This natural flow direction is influenced by contamination control systems within the model domain. There are some permeable Denver sands in direct hydraulic connection with the shallow alluvium within the model area. These Denver sands provide sources of water that affect the groundwater flow. Conceptually, some of these areas of subcropping Denver sands act as localized or point sources for the overall water budget for the

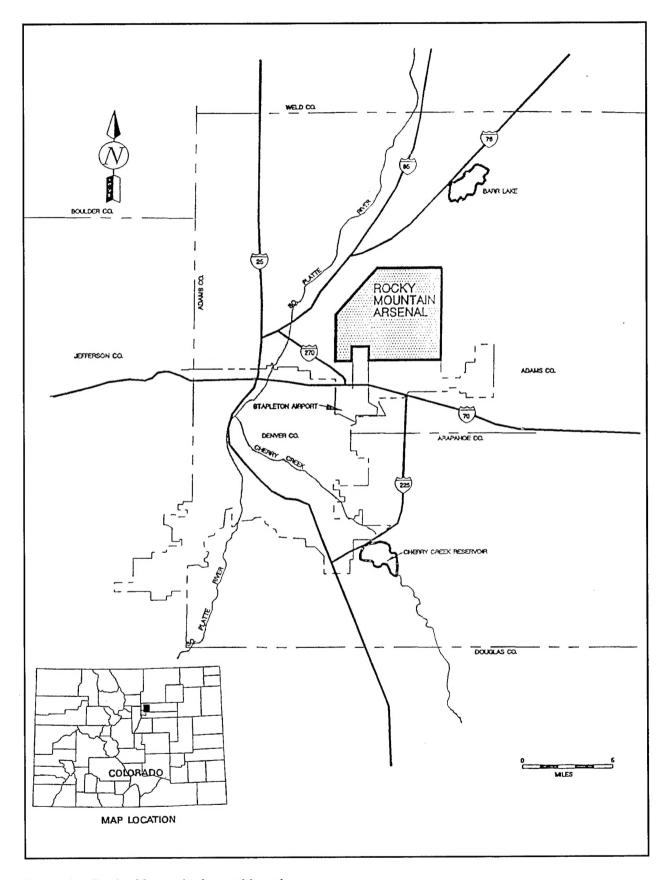


Figure 1. Rocky Mountain Arsenal location map

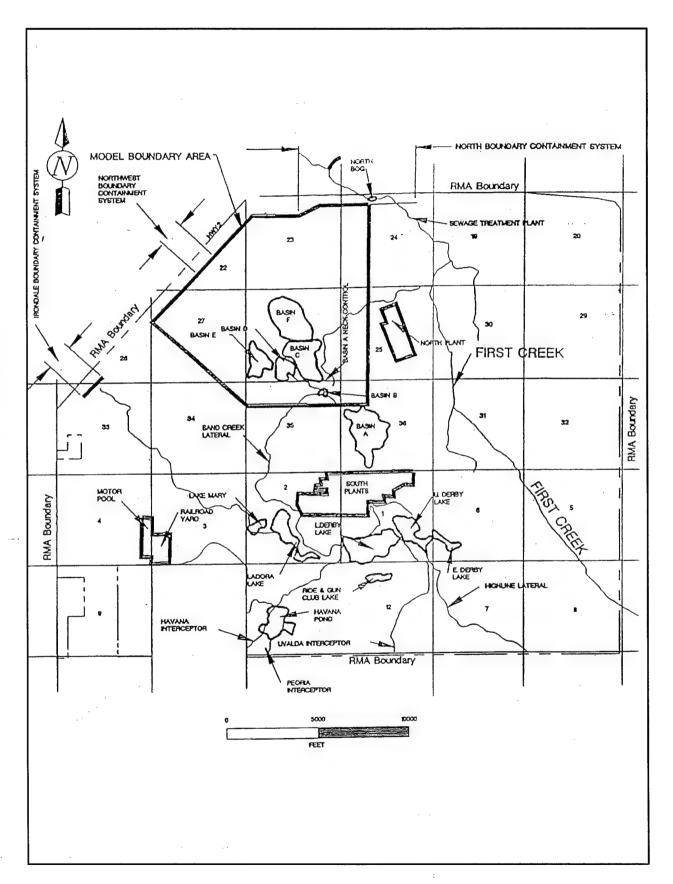


Figure 2. Model boundary area

modeled area. Infiltration from man-made basins and recharge from precipitation are other sources of water influencing groundwater flow within the model area.

### **Modeling Objectives**

Specific objectives of the modeling effort were developed based on the FS modeling needs established by RMA. The objectives of the modeling effort as described by the U.S. Army Program Manager for RMA are as follows:

- a. Represent the unconfined flow system (UFS), which is composed of saturated alluvium and upper Denver Fm, as individual geologic layers through the saturated portion.
- b. Represent equivalent realistic conditions, in terms of groundwater elevations and flux, such that at steady-state calibration, hydraulic heads are within plus-or-minus 3 ft of observed conditions for 90 percent of boundary nodes.
- c. Calibrate the model so that 95 percent of the simulated heads for observation wells are within plus-or-minus 3 ft of observed values.
- d. Reproduce the general form and location of areas of unsaturated alluvium by model simulations.
- e. Grid the model with sufficient detail to allow adequate representation of closely-spaced wells, trenches and/or low-permeability barriers, for the simulation of groundwater control alternatives that incorporate such features. The model's grid must be of such detail that the finite elements that represent Basins C and F are no more than 100 ft across in the direction perpendicular to the perimeter of the basins.
- f. Incorporate particle-tracking capability into the model to allow the delineation of flow lines and to enable evaluation of groundwater control alternatives by particle capture.
- g. Provide sufficient documentation to allow review and evaluation of the model code, parameters used in the model, model setup and calibration, sensitivity analysis, calibration criteria, and results.

Objectives are used to assist in defining the goals and associated scope of work of the modeling effort and address the need for modeling during the DAA of the FS, which requires comparison of remedial alternatives that have been retained. Objectives also allow for some flexibility in the analysis, such as combination or addition of remedial alternatives during subsequent phases of the FS.

### **Approach**

To accomplish the modeling objectives, a numerical groundwater flow model of the study area was developed to represent the conceptual model of the groundwater system which has evolved from previous studies. The degree of complexity of the model is the minimum level required to incorporate available data and accomplish the modeling objectives.

The modeled area (Figure 2) was selected for the following reasons:

- a. The proposed remedial alternatives are centered within the selected model area.
- b. The model objectives require a detailed analysis of groundwater movement near Basins C and F.
- c. Three containment systems, two of which are boundaries of the model area, are located in the study area. These containment systems provide current data on the quantity of groundwater being exchanged through the aquifer at these systems.
- d. The model overlaps with previously developed models; the North Boundary Model to the north and the South Plants/Basin A Model to the south. This overlap allows comparison of model data and results. Part of the modeled area overlaps an area modeled during reevaluation of the NBCTS Interim Response Action (IRA) improvement study.

Data used for the initial model runs were obtained from existing data approved by RMA. Data sources include officially released reports, RMA's established database, and other IRAs and modeling activities. The official data base for RMA is maintained by DP Associates, Inc.

The groundwater flow system in the study area is assumed to exist in a "steady state" or "dynamic equilibrium" for a steady-state calibration. The assumption of steady-state flow conditions was also made by Warner (1979), Earth Technology Corporation (ERTEC) (1982), Morrison-Knudsen Engineers (MKE) (1989), and Harding Lawson Associates (HLA et al.) (1990).

This modeling effort accounts for groundwater flow in the upper Denver Fm. This approach differs from the majority of previous modeling efforts, which treat unsaturated alluvium areas as impermeable and do not address flow in the Denver Fm. Exchange of groundwater between the alluvium and the Denver Fm sands, basins, and precipitation infiltration is handled by areal inputs.

The model was calibrated by applying the existing concepts of flow in the modeled area to reproduce known water levels, groundwater discharge and recharge, and the flux through the aquifer system and across boundaries.

It is the intent of this modeling effort to incorporate all current pertinent hydrogeologic data into the model. Corrections to the RMA database and data from other ongoing modeling activities were incorporated when possible.

### **Model Selection and Applicability**

The selection of the model was based on the following considerations:

- a. The model should be based on existing Colorado State University (CSU) computer code because the model area overlapped areas to the north and northwest previously modeled using CSU code.
- b. The model must have the ability to represent groundwater heads and flux through the UFS allowing for representation of flux across the bottom and side boundaries. Inflow to the UFS from the Denver Fm or outflow from the UFS to the Denver Fm was represented as localized sources or sinks.
- c. The model must have the capability to represent local aquifer hydraulic properties that may vary as a function of groundwater elevations and aquifer saturated thickness.
- d. The model must contain adequate particle-tracking capability to allow the introduction and representation of unretarded, nondegrading particles within the model domain.
- e. The model must have the ability to meet each of the stated objectives.

The model selected is a single-layer, two-dimensional horizontal finite element model (GW Flow) developed by CSU. A copy of the computer code for the model is provided in Appendix A. The CSU model has the ability to adequately simulate the complex flow system and was selected for its ability to represent local aquifer hydraulic properties that may vary as a function of groundwater elevations and aquifer saturated thickness. This allows the model to simulate groundwater extraction, recharge, and flushing alternatives, which may result in substantial changes in water-table elevations and in aquifer saturated thickness.

The assumptions involved in using this groundwater flow model include:

- a. The movement of ground water through the aquifer is described by Darcy's Law.
- b. The aquifer flow system can be adequately simulated as a single-layer, two-dimensional horizontal areal flow system.
- c. The transmissivity of the UFS at any point is equivalent to the sum of the transmissivities of the saturated alluvium and the saturated upper Denver Fm.
- d. Vertical flow between the UFS and the unweathered portions of the Denver Fm only occurs through Denver Fm sands in direct contact with the base of the alluvium.

# 2 Conceptual Model

Hydrogeology of the modeled area has been investigated extensively in past studies, which have examined both the local and regional aspects of the ground-water flow system. Previous studies provided a good conceptual picture of the hydrogeology for the area studied. The concept of the UFS for use in numerical modeling at RMA was formulated by Dr. James May and first used in the ERTEC model (1982). The Basin F Subregional Numerical Model is based on the conceptual model outline discussed in detail in the Revised Regional Groundwater Flow Model by HLA et al. 1990.

The major difference between the conceptualization used in the Revised Regional Groundwater Model and this subregional modeling effort is how the flow through the upper Denver Fm is modeled. The Basin F Subregional Conceptual Model allows for groundwater flow through the upper Denver Fm in areas of both saturated and unsaturated alluvium, whereas the Revised Regional Groundwater model only has flow through the upper Denver Fm in areas of unsaturated alluvium. This modeling effort has groundwater flow occurring through weathered Denver Fm bedrock throughout the entire study area. Other than the flow in the upper Denver Fm, the conceptualization of the Basin F subregional model is the same as that of the revised regional model. The following paragraphs discuss only the notable features of the conceptual model.

### **Unconfined Flow System**

Unconsolidated alluvium is the uppermost water bearing unit within the model domain. The alluvium consists of alluvial fill, eolian sands and silts, glacial outwash, fluvial sands, gravel, silts, and clays (Ebasco et al. 1989b). The thickness of the alluvium is highly variable, ranging from 0 to approximately 80 ft (HLA et al. 1990). Thicker areas of alluvium are commonly found in numerous paleochannels that are incised into the Denver Fm. The materials in the paleochannels are coarser grained and more permeable than those in areas outside the channels (MKE 1987).

Underlying the alluvium throughout the study area is the Denver Fm, which consists of shales, sandstones, siltstones, claystones, low-grade coal, and lignite (May 1982, Ebasco et al. 1989b). The Denver Fm is referred to as bedrock in this report, and the interface between the Denver Fm and the alluvium is the bedrock surface. At locations where the water table lies below the bedrock

surface, the alluvium is unsaturated. The flow system in the model area is conceptualized as a two-dimensional unconfined flow system as shown in Figure 3. The base of the UFS is interpreted as always being below the bedrock surface. Theoretically, the base of the UFS is defined as the elevation where the potentiometric head in the Denver Fm and the water table in nearby alluvial material coincide.

The UFS flow through the model area is under unconfined conditions. Deeper water-bearing zones in the same area may be confined or semi-confined. The groundwater moves through the saturated alluvium and through the weathered upper Denver Fm. The majority of flow through the upper Denver Fm of the UFS is in areas of unsaturated alluvium. It is in these areas that more severe oxidation and weathering would most likely occur. Therefore, shallow groundwater flow occurs within a single UFS that consists of alluvium and the upper Denver Fm.

#### **Sinks and Sources**

The UFS within the model domain is affected by any water exchange to or from the system. Therefore, it is important to understand the relationship between the groundwater within the UFS and any activity that adds or removes water from the UFS.

Water exchange within the UFS is characterized by all significant activities that recharge water to the UFS (sources) or remove water from the UFS (sinks). The following factors were considered as sources of water exchange for this study: (1) infiltration from basins, (2) infiltration of precipitation, (3) groundwater flow from Denver Fm sands into the UFS, (4) groundwater pumping and injection, and (5) boundary flow. A detailed analysis of each water-exchange activity will be made and discussed in subsequent parts of this report. Although downward gradients are common in the modeled area, the low permeability associated with most of the Denver Fm seems to prohibit significant downward movement of water. Water flows into the weathered Denver Fm and then flows laterally, reentering the alluvium at a lower elevation.

### Summary

Groundwater flow of the model area is conceptualized as a two-layered UFS consisting of alluvium and upper Denver Fm. The groundwater flow system is affected by water exchange involving surface-water bodies, precipitation, flows from the Denver Fm, groundwater pumping and injection, and boundary flow.

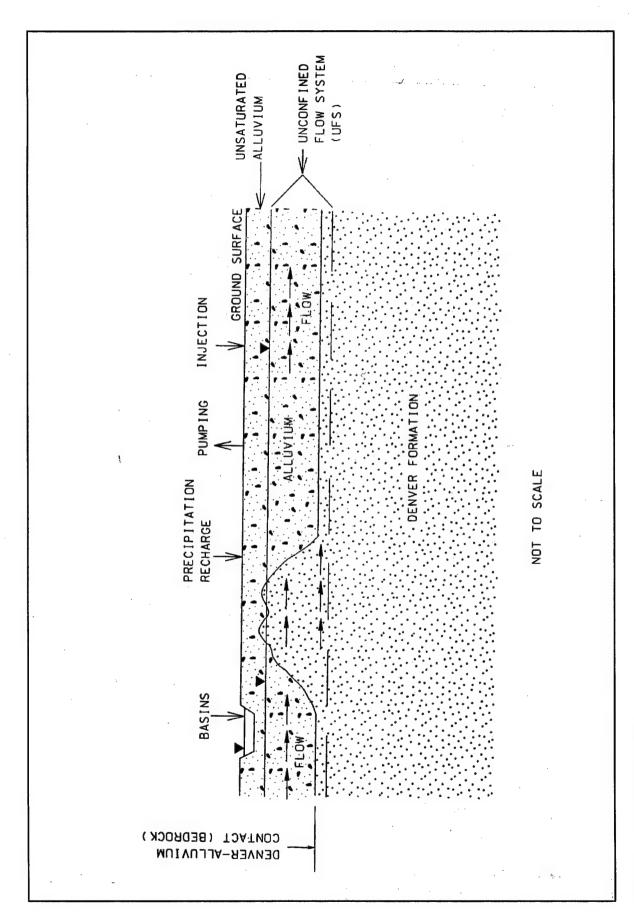


Figure 3. Conceptual model

# 3 Modeling Procedure

#### **Numerical Model**

The numerical model used in this study analyzes two-dimensional horizontal movement of groundwater. The use of a two-dimensional areal model is justified because the dominant flow of groundwater and contaminants is areal and because downward-moving groundwater intersects low-permeability clay zones and moves back into the alluvium. Vertical movement of groundwater between the UFS and other aquifers is not simulated in this study except as recharge or discharge to the horizontal flow system.

The finite-element procedure used to model the groundwater flow system requires the discretization of the modeled area into discrete subregions called elements. The model allows for the modeled area to be divided into distinct areas which are formed as loops (Figure 4) using the mesh generator. Once an area is broken out as a loop, it can then be divided into as many elements as required. In this study, the discretization procedure resulted in a mesh of ten loops consisting of 6,466 triangular elements and 3,359 nodes (Figure 5). Figures 6 and 7 show an enlarged portion of the mesh with the element and node numbers. The mesh encompasses an area of 3.64 square miles. The shape and discretization level of the constructed mesh were governed by the following criteria:

- a. A discretization level with sufficient detail to allow the adequate representation of closely spaced wells, trenches and/or low-permeability barriers for simulation of groundwater control system alternatives.
- b. An adequate representation of the three contaminant control systems located on the boundaries of the model area.
- c. A discretization level with sufficient detail to represent areas where rapid changes in groundwater levels exist.
- d. A minimum number of total elements and nodes needed to accomplish the objectives.

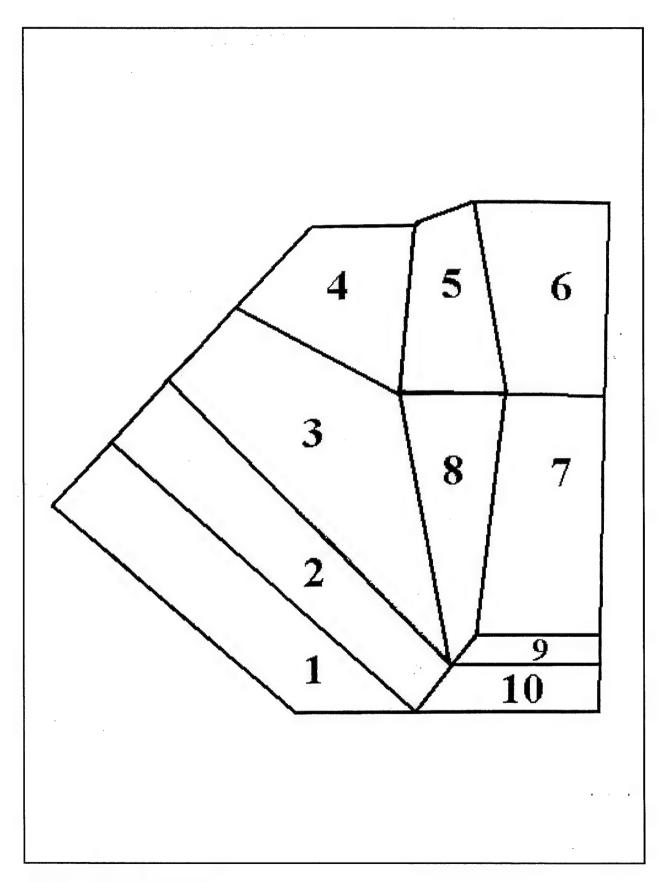


Figure 4. Mesh of ten loops

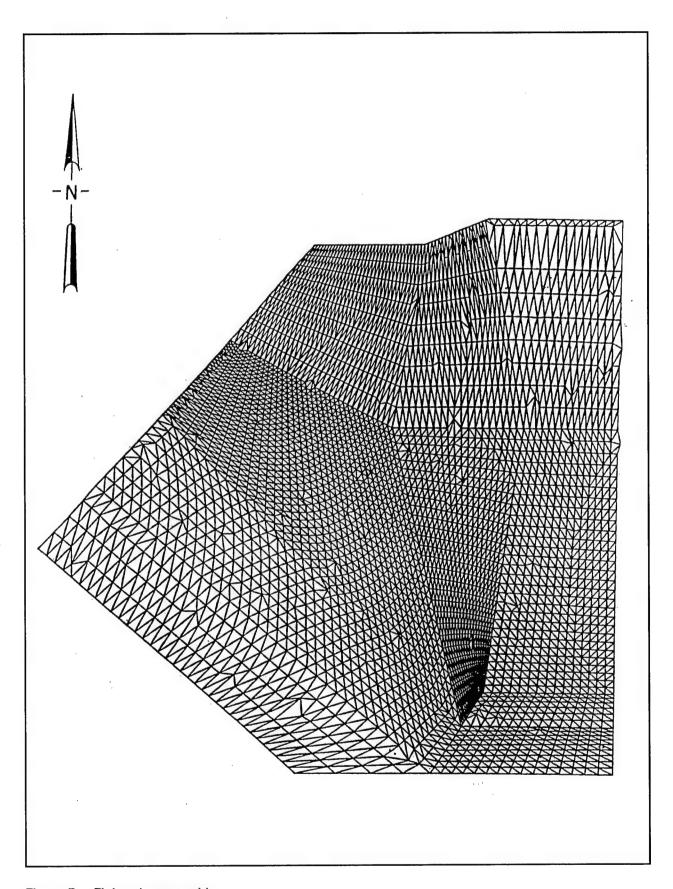


Figure 5. Finite element grid

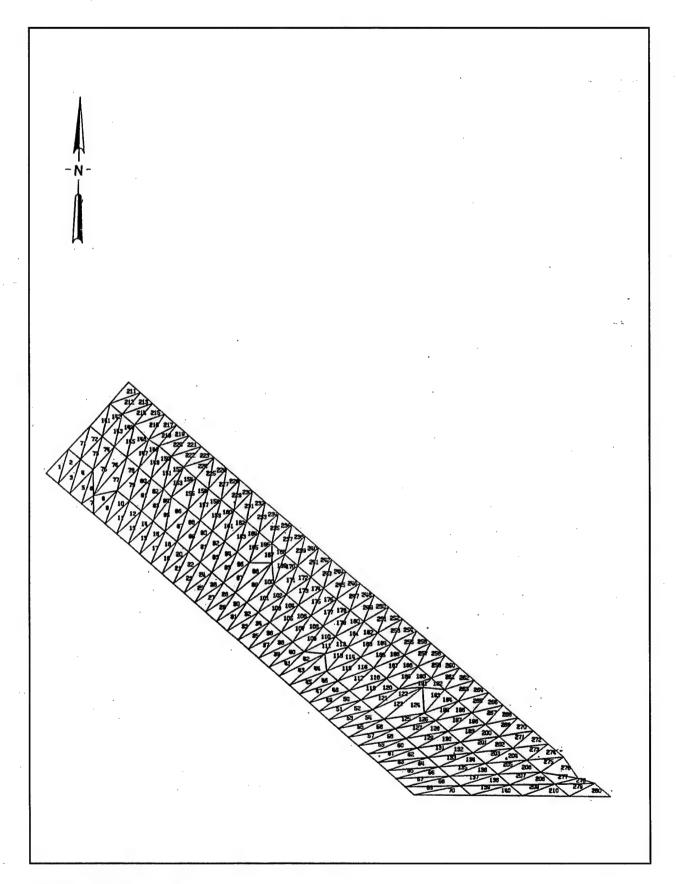


Figure 6. Grid element numbers

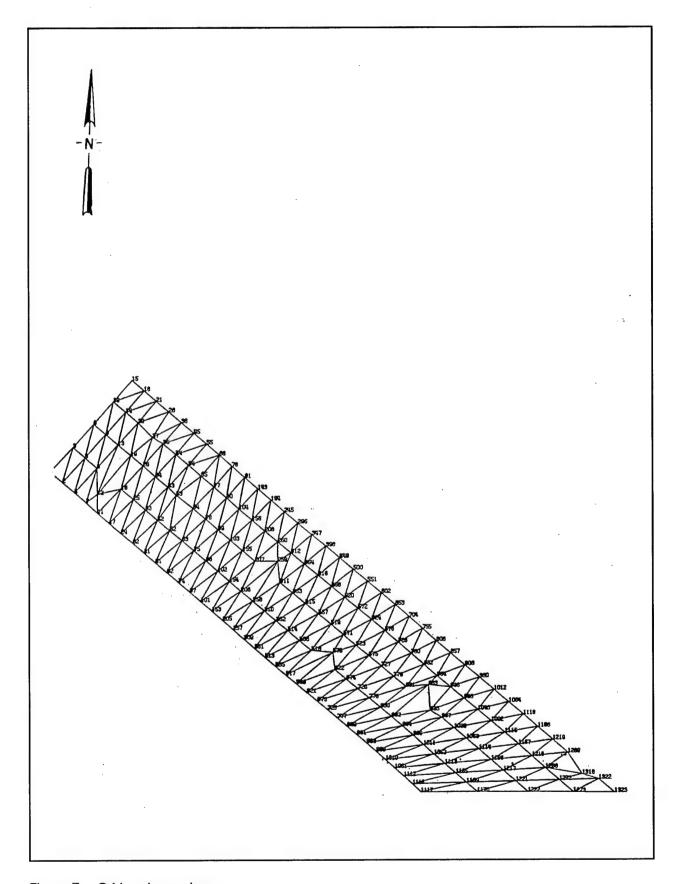


Figure 7. Grid node numbers

### **Model Inputs**

For simulations, the CSU numerical model, GW Flow, requires input of parameters that characterize transmissive properties of the groundwater flow system and the fluxes that represent quantitative contributions to and losses from the groundwater flow system. As stated earlier, the initial input data used in this modeling effort were taken from technical reports officially released by the Program Manager's Office for Rocky Mountain Arsenal, and from the RMA official database.

The quantitative definition of the following types of information and parameters describing the groundwater flow system were required: (1) ground-surface elevations, (2) water-table elevations, (3) hydraulic conductivity, (4) spatial distribution of basin and precipitation infiltration, (5) groundwater pumping and injection, and (6) boundary conditions. Each of these component inputs is discussed in terms of the data used and the method used to assign values to nodal points/or elements within the model.

#### **Ground-surface elevations**

The ground-surface elevations were taken from the official RMA data base. The elevation of the bedrock surface and the base of the UFS were taken from the 1989 Final Water Remedial Investigation Report (FWRIR) released by RMA and prepared by Ebasco. Contour maps of bedrock elevation and base of UFS elevation in the study area were prepared as part of the FWRIR (Plates 7 and 14, Ebasco et al. 1989b). Contour maps of each surface were digitized to produce a numerical data file in the form of X coordinate, Y coordinate, and surface elevation Z at each X and Y. The procedure produced an X, Y, and Z value for each point within the digitized area at 75 ft intervals. The X, Y, Z data file representing each surface elevation was used as input for the portion of the CSU code that generates the data file required for model simulation. To generate this data file. the model applies an internal inverse distance routine to each X, Y, Z data file to determine a Z value (surface elevation) at each node location within the model domain. The resulting data file consisted of the surface elevation at each node. Additional data approved by RMA and obtained from other agencies, activities, and modeling efforts were also incorporated into the data files. Data files representing the ground surface, bedrock surface, and base of UFS surface were used as input to the model for steady-state calibration. Elevation contour maps of the ground surface, bedrock surface, and UFS base surface used for calibration are shown in Figures 8, 9, and 10, respectively.

#### Water-table elevations

Water-table elevations used to represent the observed steady-state flow field are based on the summer 1990 water-table elevation contour map of the UFS taken from the Comprehensive Monitoring Program's Annual Ground Water Report for 1990 (Figure 4.1-4, Stollar & Assoc. et al. 1990). The contour map of summer 1990 water-table elevation is based on hydraulic head data collected from monitoring wells, and on estimates and interpretations of the hydraulic

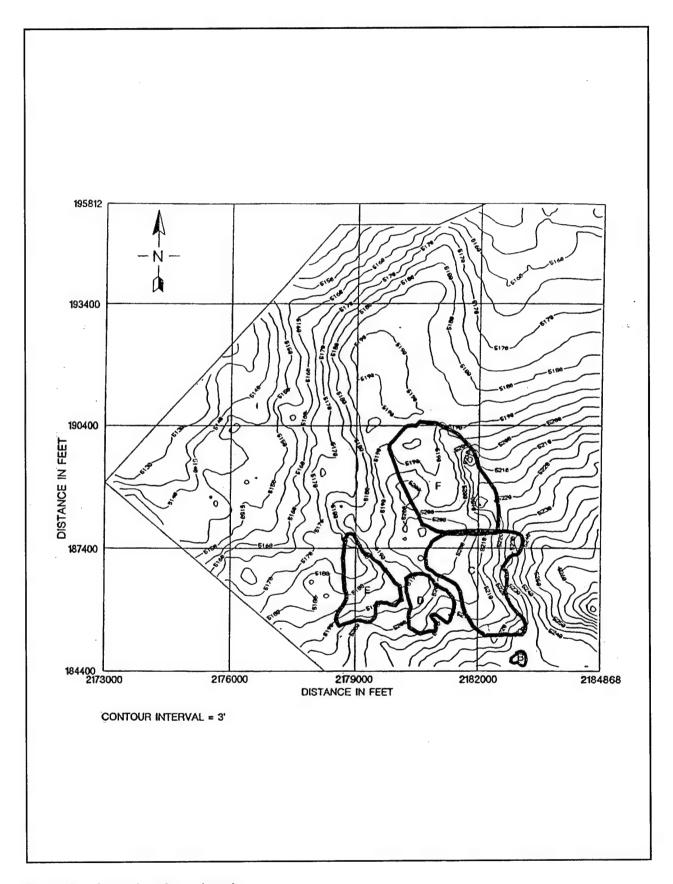


Figure 8. Ground surface elevation

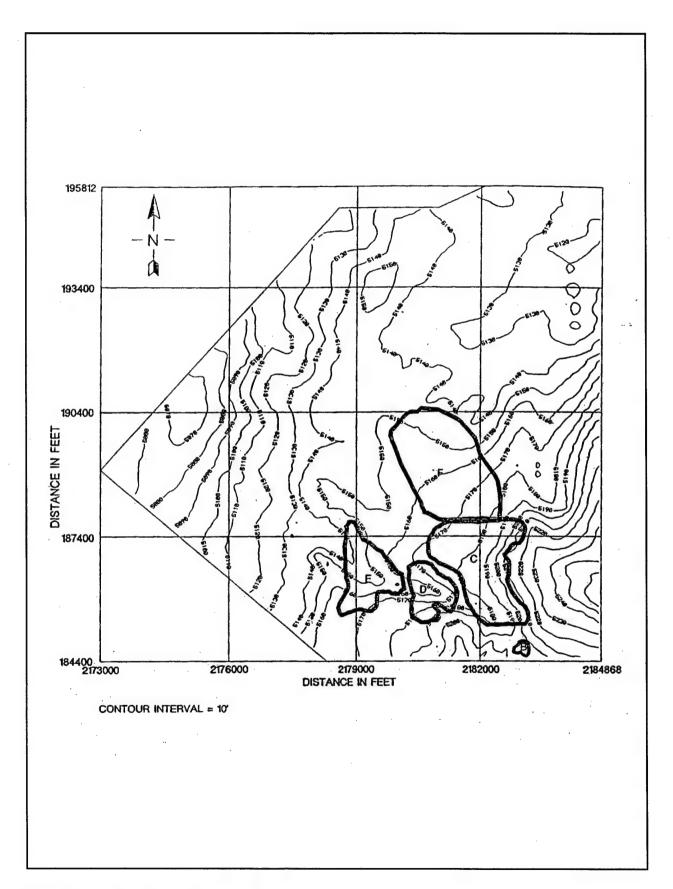


Figure 9. Bedrock surface elevation

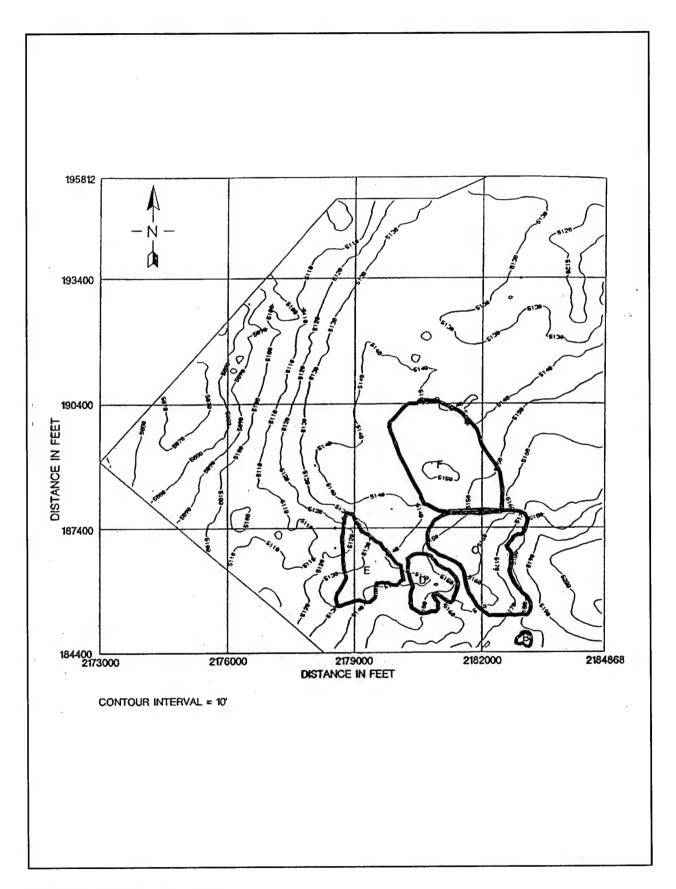


Figure 10. UFS base elevation

head made from hydrogeologic data. Because the map is interpretive, the model steady-state calibration is based primarily on observed hydraulic heads from monitoring wells. Hydraulic heads from 74 monitoring wells were selected as the basis for model calibration. Wells were selected because they did not exhibit highly variable head changes over a 5-year period or any other signs that would indicate poor well construction. Locations of observation wells used for calibration are shown in Figure 11.

The summer 1990 water-table contour map was digitized to generate the X, Y, Z data file needed to produce the data file used for model calibration. The same process used to produce model input data files for the surface elevations was taken to produce the water-table elevation input data file used as the basis for model calibration. A contour map of the water-table elevation data file used to model steady-state calibration is shown in Figure 12. The map indicates that the prevailing flow direction in the shallow groundwater is from southeast to northwest.

The summer 1990 water levels were taken as the basis for model steady-state calibration. Calibration of the model is based on the model's ability to accurately reproduce the observed water levels. The use of 1990 water levels as the basis for steady-state calibration is justified with the assumption that the water levels are in a state of dynamic equilibrium. The summer 1990 water levels were used because they were the most complete set of water levels available at the start of this modeling effort.

#### **Hydraulic conductivity**

The CSU code simulates the UFS as one aquifer requiring two different hydraulic conductivities at each node. The alluvium portion of the UFS requires a hydraulic conductivity data file different from that of the upper Denver Fm portion of the UFS.

The hydraulic conductivity value assigned to each node for the initial model calibration run was determined from a map produced in the Final Water Remedial Investigation Report (FWRIR) (Plate 16, Ebasco et al. 1989).

The hydraulic conductivity map divides the model area into different zones based on boring logs, aquifer test analyses, and geologic interpretations of depositional materials. Different material classifications were used, each characterized by a representative hydraulic conductivity and a possible range of conductivity values.

A more detailed hydraulic conductivity zonation of the study area near the Northwest Boundary System was provided by Woodward-Clyde Federal Services. These additional data were produced from boring logs and seismic tests conducted as part of their Northwest Boundary System modeling effort. Based on this new data, modifications were made to the FWRIR conductivity zones in the area west of the North Boundary System. The hydraulic conductivity zones map representing the initial hydraulic conductivity of the study area is shown in Figure 13.

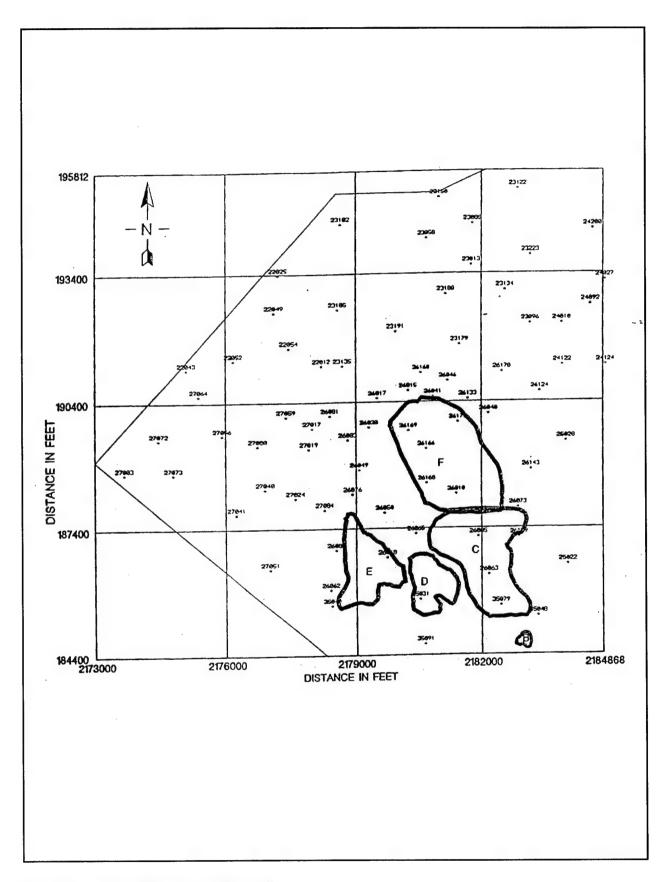


Figure 11. Calibration observation well

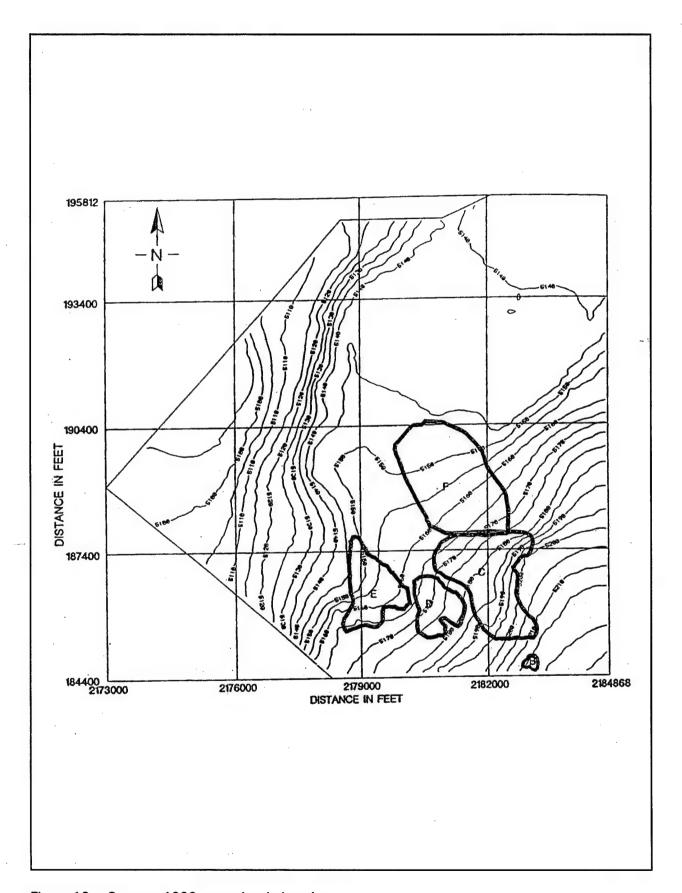


Figure 12. Summer 1990 water level elevation

The hydraulic conductivity map from the FWRIR (Plate 16, Ebasco et al. 1989) was digitized to produce a data file of X, Y, and Z coordinates consisting of hydraulic conductivity (Z values) representative of each material type on the map. The resulting data file represented known alluvium hydraulic conductivities (Z values) for specific X and Y coordinates. The X, Y, and Z data file was used by the inverse distance subroutine to determine the alluvium hydraulic conductivity at each node. The alluvium hydraulic conductivity used for calibration ranged from 2 to 1,500 ft/day.

The weathered upper Denver Fm hydraulic/conductivity data file was produced by initially assigning a constant hydraulic/conductivity value of 2.8 ft/day to the entire Denver Fm within the model area. This value was determined to be representative of the upper Denver Fm within the model area based on the hydraulic conductivity zone map produced in the FWRIR (Plate 16, Ebasco et al. 1989) and on the data produced by the Regional Groundwater Study of RMA (May 1982). The upper Denver Fm hydraulic conductivity of 2.8 ft/day is similar to the value of 3 ft/day used in the Revised Regional Groundwater Flow Model (HLA et al. 1990) in areas corresponding to the modeled area. Hydraulic conductivities ranging from 0.0014 to 283 ft/day within the Denver Fm were reported by MKE (1989). The Denver Fm hydraulic conductivities at calibration ranged from 0.1 to 14 ft/day. The variability in hydraulic conductivity values illustrates the uncertainties associated with the hydraulic conductivity of the upper Denver Fm.

The hydraulic conductivities and the saturated thickness of the UFS are required to produce the transmissivity of the UFS. The transmissivity of the UFS is the parameter required by the model and consists of the product of the hydraulic conductivity and the thickness of the material. The transmissivity for the UFS is the sum of the transmissivity of the alluvium and upper Denver Fm which is effectively a weighted average. The equation the model applies to determine the transmissivity at each node with saturated alluvium is shown in Figure 14.

A contour map of the resulting transmissivity distribution used for steadystate calibration is shown in Figure 15.

# Spatial distribution of basin and precipitation infiltration

The recharge of water to the UFS is from precipitation infiltration, inflow from subcropping Denver Fm sands, and basin infiltration. Recharge to the UFS from these sources is represented by an areal flux. This areal flux is represented by applying a prescribed flux to the elements covering the desired area. Elements within the specific locations are assigned an identification code which is then used to apply the desired flux.

A percentage of precipitation moves beyond the root zone and ends up as recharge to the shallow unconfined aquifer. Estimates of the areal recharge of precipitation are variable. An infiltration study conducted by MKE in 1987 estimated an infiltration rate of 0.25 in. per year as a reasonable value for

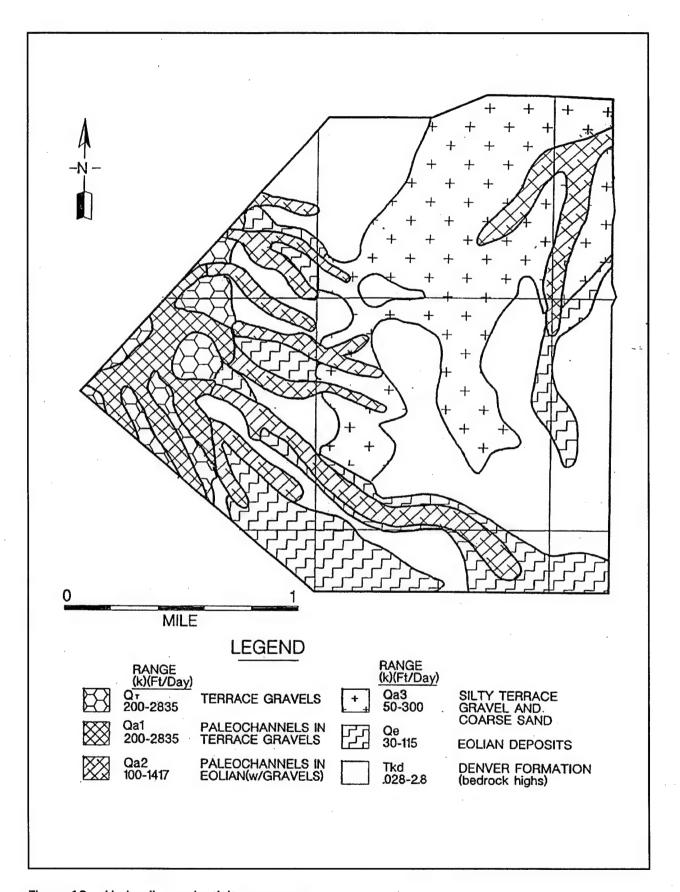


Figure 13. Hydraulic conductivity zone map

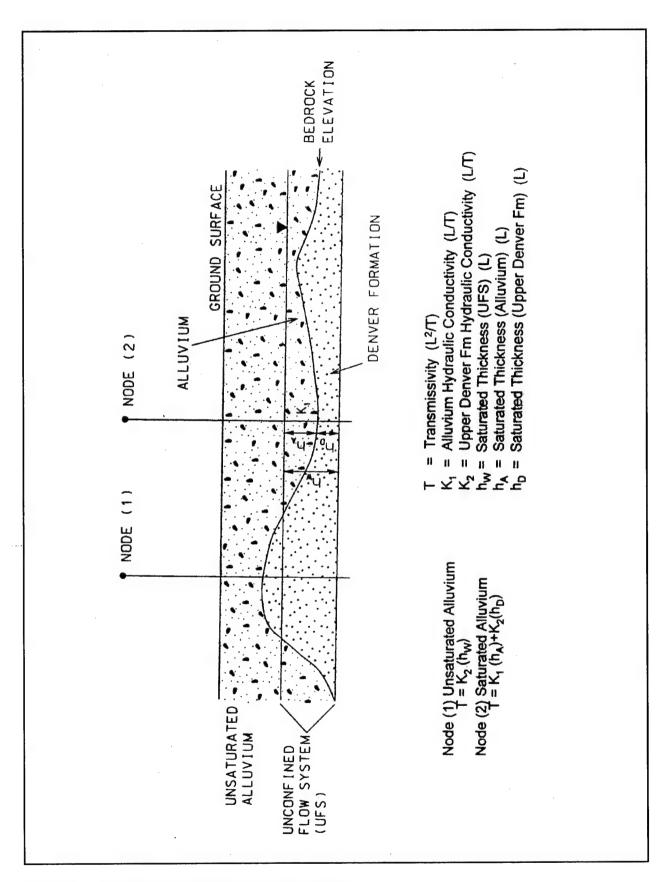


Figure 14. Equation for calculation of transmissivity

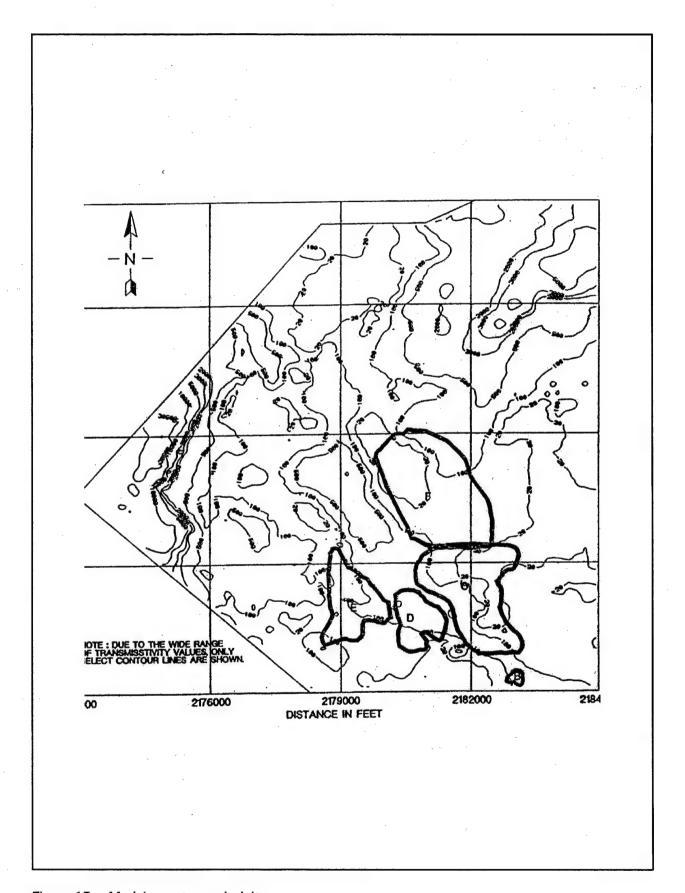


Figure 15. Model area transmissivity

vegetated areas at RMA. Other studies resulted in an estimated infiltration rate of 1.41 in. per year for similar conditions. For this modeling study an infiltration rate of 0.9 to 1.3 in. per year is applied to the model during steady-state calibration. The infiltration rate applied to the model domain is represented by an areal water flux of 0.0003 to 0.0002 ft/day/ft². Higher surface elevations have the rate of 0.0003 ft/day/ft², and lower surface elevations have the rate of 0.0003 ft/day/ft². This approach is consistent with the fact that lower surface elevations receive more precipitation runoff and have more infiltration. The surface elevation within the model domain slopes downward from east to west, and infiltration rates are applied accordingly. The water flux values are multiplied by the area of each element and applied over the model domain.

The second recharge source considered is from the basins within the model area. The infiltration recharge quantities from Basins B through F used for the initial calibration run were taken from the Revised Regional Model (HLA et al. 1990) and are summarized in Table 1. In order to improve the steady-state calibration, it was necessary to reduce the basin infiltration recharge rate within the model area to zero. The only recharge from these basins within the model area is from precipitation infiltration, which is consistent with the fact that the basins were no longer in use in 1990. Basin F has no precipitation infiltration recharge because the basin was lined before 1990. The infiltration associated with Basin F is collected as runoff and discharged. The Basin F runoff discharge rate is applied with the Denver sands recharge rate located near the basin.

Table 1 Basin Recharge Infiltration Rates						
Recharge Basin	Area (acres)	Recharge (cfs)	Infiltration (ft/day)			
В	1.77	0.006	0.006724			
С	78	0.0	0.0			
D	20	0.034	0.0033719			
E	29.4	0.0	0.0			
F	92.7	0.0	0.0			

The third recharge source that was considered is the influx of water from the Denver Fm underlying the UFS. Interactions between the Denver Fm and the UFS is probably the least understood hydrogeologic process at RMA. The recharge of water to the UFS from the underlying bedrock subcropping sands is represented by an areal flux into the UFS. The locations of Denver Fm subcrops within the study area were identified from maps delineating subcrop areas for bedrock units underlying RMA (Plate 9, FWRIR, Ebasco et al. 1989). The major sand subcrops within the model domain which provide notable quantities of water into the UFS are shown in Figure 16.

The quantity of the prescribed flux from the Denver Fm sands into the UFS used for the initial calibration run was taken from the Revised Regional Groundwater Flow Model (HLA et al. 1990). The flux was changed as a calibration parameter during calibration. The flux calculated by the regional model that represents the total prescribed influx from the Denver Fm into the UFS for the

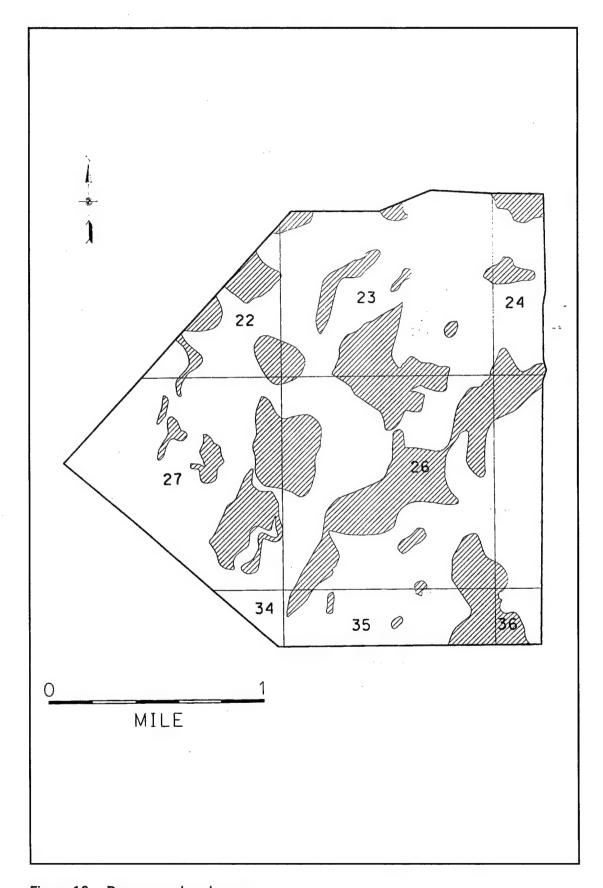


Figure 16. Denver sands subcrops

RMA was taken and equally distributed to the major sand subcrops within the RMA. The total computed inflow to the UFS within the RMA from Denver Fm sources is 0.427 cfs (191 gpm) (HLA et al. 1990). The Denver Fm sand subcrops located within the model domain represented 17 percent of the total RMA sand subcrops; an equivalent percentage of the total prescribed flux was calculated and applied to the sand subcrops for the initial calibration run.

The total inflow to the UFS within the model area from the Denver Fm used for the initial calibration run is 0.0726 cfs (32 gpm). The total inflow to the UFS from the Denver Fm subcropping sands applied in the steady-state calibration is 76 gpm.

#### Groundwater pumping and injection

There are three operational containment systems within the model domain currently pumping water from the UFS and/or injecting water into the UFS, the NBCTS, NWBCS, and the Basin A Neck Control System. As previously stated, the NWBCS and part of the NBCTS are boundaries of the model domain. The model domain includes pumping wells from the two systems, but the systems' injection wells are outside the model area. Thus these become discharge for the model. The entire Basin A Neck Control System is within the model domain; both the system's pumping and injections wells are represented as nodes within the model. Each well is assigned a nodal identification code, which in turn is assigned a recharge or discharge rate based on the operation of the system. The location of some system wells are too close together for the model grid; because of this some wells have the same identification code. The recharge/discharge rates for ID codes representing more than one well is the sum of the rates for each well. The slurry wall portion of the boundary systems was represented as no flow boundaries.

Well locations along with average pumping and injection rates for each system were taken from the RMA data base. Pumping rates used for model calibration are 85 gpm for the portion of the NBCTS within the model area, and 314 gpm for the NWBCS. The pumping/injection rates for the Basin A Neck System applied for calibration are 16.5 gpm. The well numbers and rates for NBCTS, NWBCS, and Basin A Neck containment system used for steady-state calibration are shown in Tables 2 through 4.

#### **Boundary conditions**

The CSU model allows four possible boundary conditions: No-Flow, Prescribed Flux, Constant Head, and General Head. The model boundary corresponding to the NBCTS and NWBCS low-permeability barriers are no-flow boundaries. All other model boundaries are Constant Head boundaries. Constant Head was the boundary condition that best represented the flow through each boundary node based on a constant head boundary condition; those computed fluxes were used to change the southern and western boundaries of the model to a prescribed flux. Boundary conditions resulting from model steady-state calibration consist of three boundary conditions as shown in Figure 17.

Table 2 North Boundary Containment System Pumping Rates for Steady-State Simulation

Well No.	Well ID Code	Rate (gpm)
23301	17	0.190
23302	18	3.762
23303	19	7.452
23304	20	1.794
23305	21	10.671
24306	22	16.546
24307	23	6.370
24308	24	4.401
24309	25	3.712
24310	26	4.728
24311	27	1.126
24312	28	4.421
24313	29	9.219
23330	11	0.002
23331	12	0.001
23332	13	4.401
23333	14	0.405
23334	15	4.356
23335	16	1.238

Table 3 Northwest Boundary Containment System Pumping Rates for **Steady-State Simulation** 

Well No.	Well ID Code	Rate (gpm)
22301	41	122.00
22302	41	43.72
22303	40	3.23
22304	40	64.34
22305	39	51.84
22306	39	2.06
22307	38	90.98
22308	38	101.33
22309	37	3.78
22310	37	49.28
22311	30	0.03
22312	31	14.17
22313	32	6.72
22314	33	5.16
22315	34	22.34
22316	35	0.00
22317	36	0.00

Table 4 Basin A Neck Containment System Pumping/Recharge Rates for **Steady-State Simulation** 

Discharge			Recharge <sup>2</sup>			
Well No.	Well ID Code	Rate (gpm)	Well No.	Well ID Code	Rate (gpm)	
35301	42	0.104	46	Trench A	1.37	
35302	43	2.656	47	Trench A	1.37	
35303	44	2.132	48	Trench A	1.37	
35304	42	1.995	49	Trench A	1.37	
35305	43	5.530	50	Trench B	1.37	
35306	44	1.368	51	Trench B	1.37	
35307	44	0.681	52	Trench B	1.37	
23311	45¹	2.0	53	Trench B	1.37	
			54	Trench C	1.37	
			55	Trench C	1.37	
			56	Trench C	1.37	
			57	Trench C	1.37	

Basin F IRA discharge water is represented by ID Code 45.
 The system's recharge water is entered through the Basin A Neck recharge trench system. Each recharge trench is represented by a series of 4 wells.

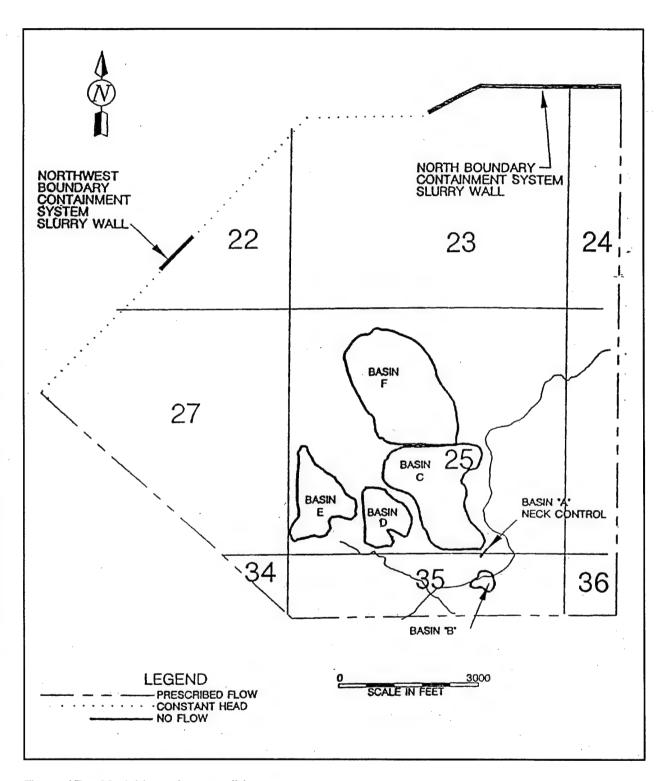


Figure 17. Model boundary conditions

### 4 Model Steady-State Calibration

The calibration procedure consists of adjusting model parameters so the model-computed water level elevations approximate as closely as possible measured and estimated values of water level elevations that were "observed." The parameter adjusted most during steady-state calibration of the model was hydraulic conductivity. Other parameters adjusted to a lesser degree were the prescribed inflows from the Denver Fm sand subcrops and the saturated thickness of the upper Denver Fm.

Some subareas within the model domain were subject to major changes in hydraulic conductivity during calibration. In an effort to improve model calibration, the saturated alluvium hydraulic conductivity in some areas was changed significantly from the initial values taken from the hydraulic conductivity zonation map. The alluvium nodal hydraulic conductivity used for steady-state calibration of the model is given in Figure 18.

The initial hydraulic conductivity of many major areas of saturated upper Denver Fm (bedrock highs) within the UFS was determined to be too low. Areas of saturated upper Denver Fm appeared to be more weathered than previously thought and, therefore, an increase in hydraulic conductivities was required to calibrate the model to the observed heads in areas of large bedrock highs. The largest hydraulic conductivity applied to areas of upper Denver Fm is 14 ft/day. This value may be considered high when compared with measured hydraulic conductivities for the Denver Fm (FWRIR, Ebasco et al. 1989b). The Regional Groundwater Study of RMA by May (1982) indicated that some areas of severely weathered upper Denver Fm may have hydraulic conductivities as high as 50 ft/day. This high variability in conductivity illustrates the uncertainty of flow parameters in the upper Denver Fm. The upper Denver Fm nodal hydraulic conductivity used for steady-state calibration of the model is given in Figure 19.

Changes in saturated thickness were made to the upper Denver Fm during calibration. The upper Denver Fm saturated thickness in some areas was subject to interpretation and consequently required adjustments. A study is currently being conducted to better determine the base of the UFS, which will affect the saturated thickness of the model area. The preliminary results of that study indicate that the base of the UFS is much lower than previously thought

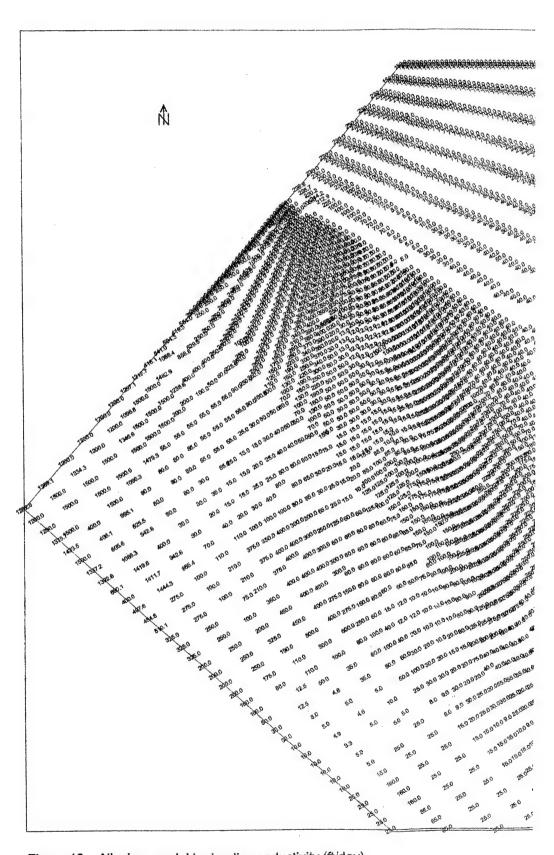
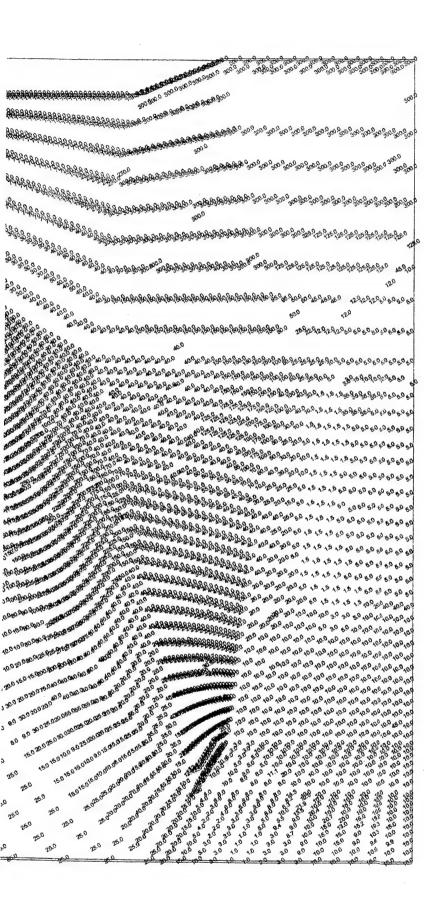


Figure 18. Alluvium model hydraulic conductivity (ft/day)



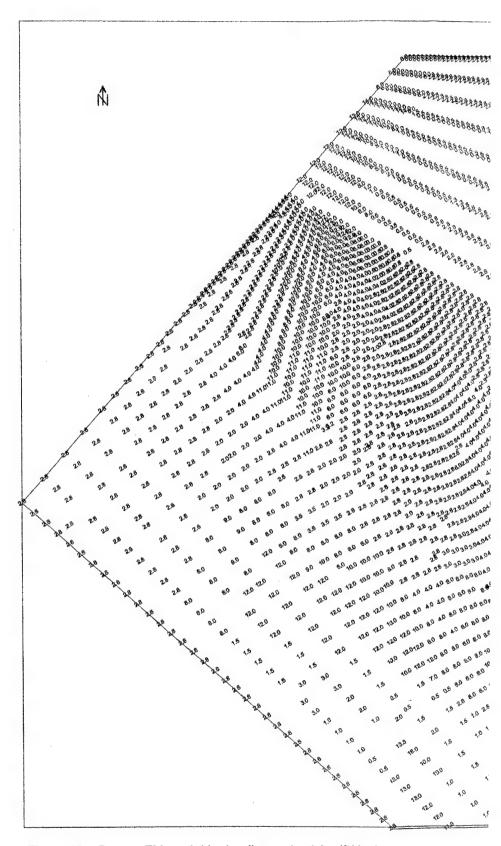
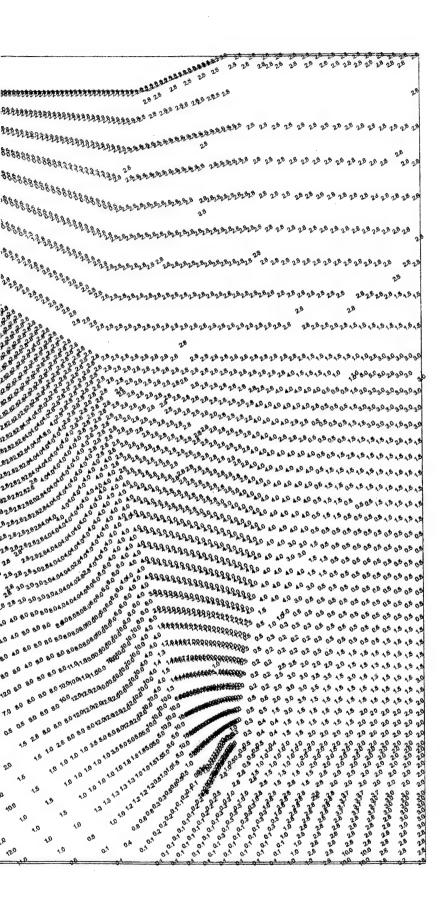


Figure 19. Denver FM model hydraulic conductivity (ft/day)



(Sturdivant 1993). This finding supports the minor changes to the saturated thickness. The saturated thickness of the alluvium and the weathered Denver Fm is given in Figures 20 and 21. The alluvium has areas that are saturated and unsaturated.

Areas of unsaturated alluvium occurring in the summer of 1990 are shown in Figure 22. The areas of unsaturated alluvium resulting from steady-state calibration are shown in Figure 23. A comparison of the two figures indicates that the calibrated model reproduced the summer 1990 unsaturated alluvium areas within previously stated criteria. In some areas of the model domain, the summer 1990 saturated areas are less than 2 ft from being unsaturated, which explains why the two figures have minor differences. The calibrated model water level elevation can be within 2 ft of the observed water level elevation and still change unsaturated areas to saturated areas, and vice versa.

During the calibration process more than 500 runs were made using the method previously described. After the completion of each calibration run, a contour map of the difference (residual) between observed and computed heads was prepared to locate areas where differences remained above plus or minus 3 ft. The residual contour map was overlaid on maps showing the saturated and unsaturated areas, the observed water-level contour, and the most recent hydraulic conductivity so that new adjustments could be made in these parameters for the next run. The model was assumed to be calibrated when the residual values were as low as possible and further runs did little to decrease the residual, and when the following criteria were met:

- a. Ninety-five percent of all observation wells were within plus or minus 3 ft of their observed values (Table 5).
- b. The mass balance was within 95 percent (Table 6).
- c. The groundwater flows across the NBCTS, NWBCS, and the Basin A Neck system were within 95 percent of observed flows.

The computed heads from the model calibration shown in Figure 24 is a reasonable duplication of the observed heads shown in Figure 13 and the general flow pattern of the groundwater. A contour map of the differences between observed and computed heads, referred to as the calibration residual map, for the calibrated model is shown in Figure 25. Positive areas indicate where the model-computed heads are greater than observed heads, and negative values indicate locations where computed heads are less than observed heads.

#### Flow Paths

The particle tracking algorithm of the model was used to determine some groundwater flow paths within the model area. Several flowlines or streamlines indicating groundwater flow paths taken by particles of water moving through the model domain have been generated with the steady-state calibrated

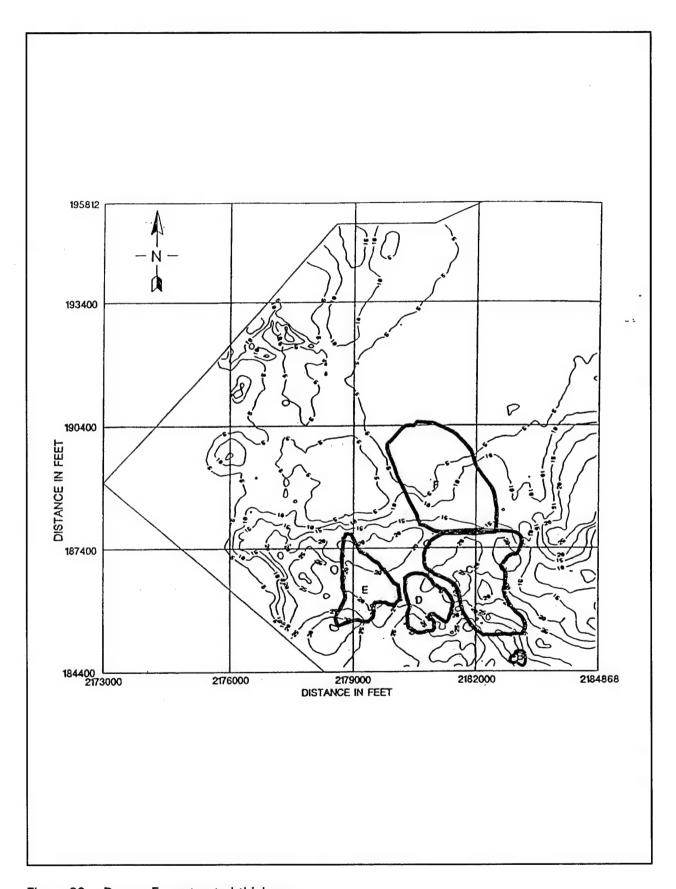


Figure 20. Denver Fm saturated thickness

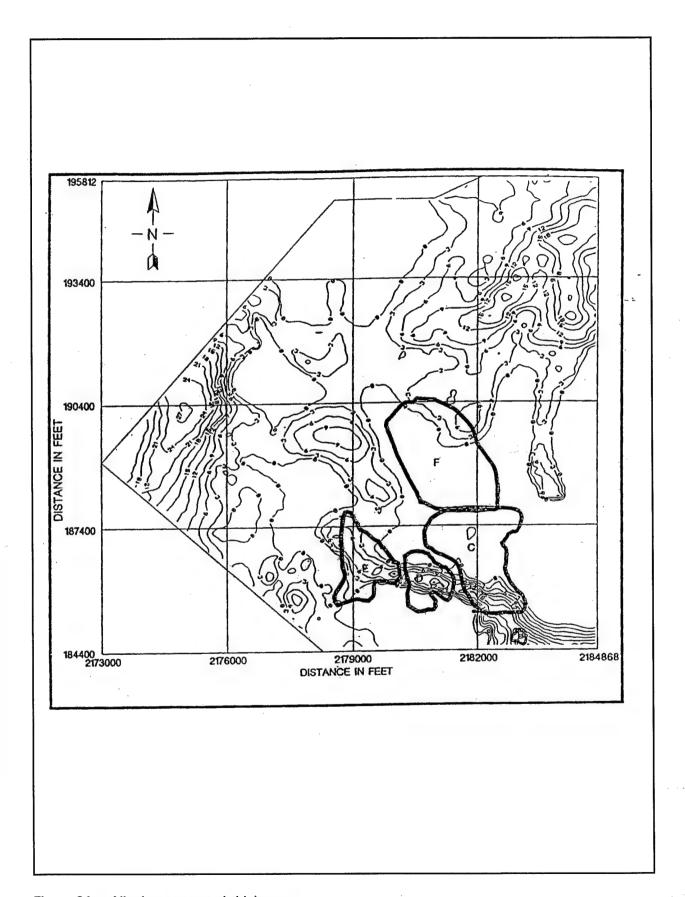


Figure 21. Alluvium saturated thickness

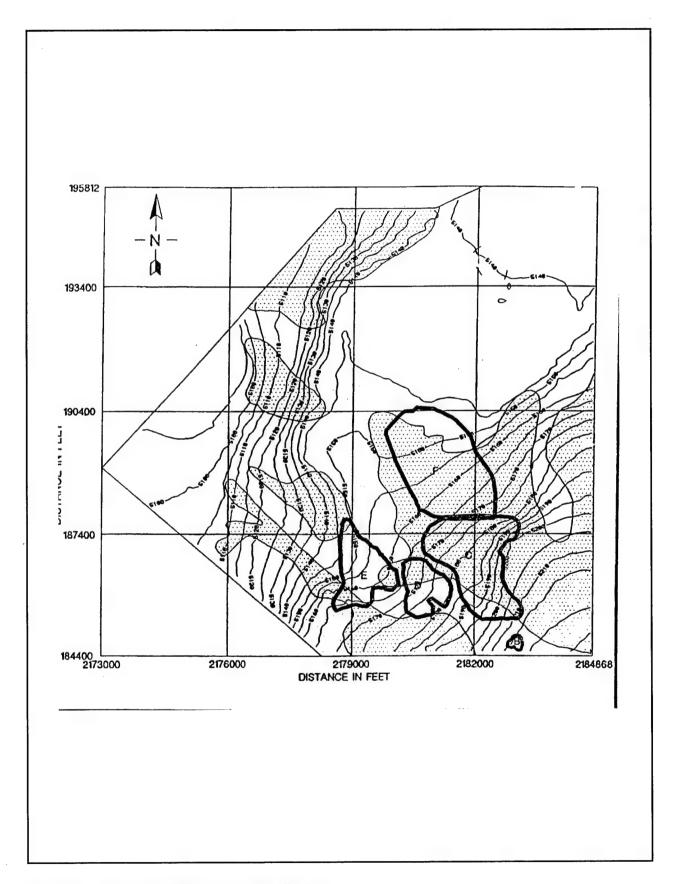


Figure 22. Summer 1990 unsaturated alluvium

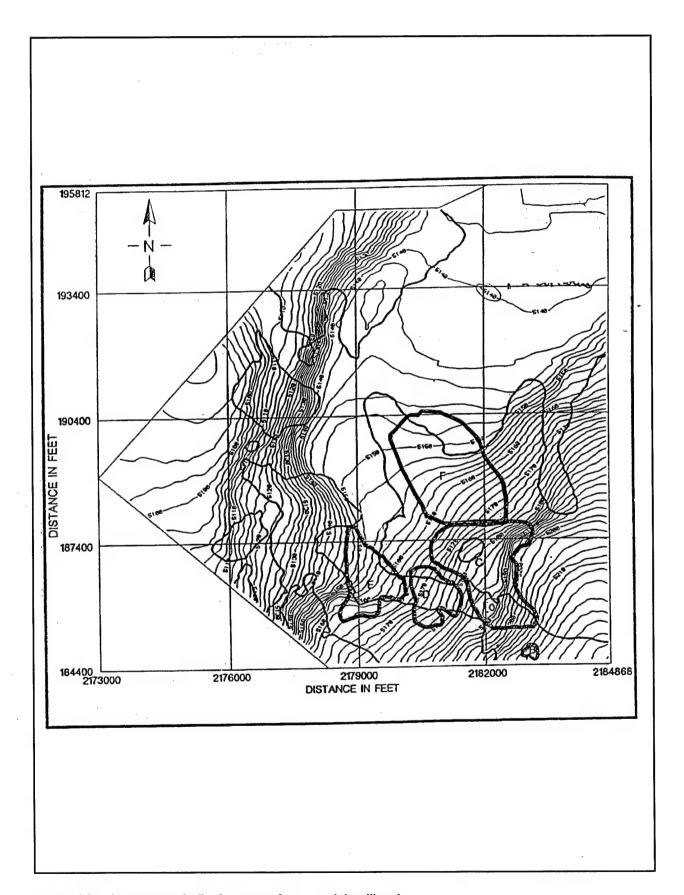


Figure 23. Unsaturated alluvium area from model calibration

Table 5 **Observation Wells Transient Calibration** Steady State Calibration Observed Calculated Head Observed Calculated Head Observation Head Head Diff. Head Head Diff. Well No. ft ft ft ft ft ft 22012 5143.50 5140.63 2.87 5143.47 5141.04 2.43 5109.64 -0.37 5109.18 5108.90 0.28 22025 5109.27 5092.42 5092.31 5091.86 5092.32 -0.46 22043 0.11 22049 5110.36 5110.29 0.07 5110.01 5108.95 1.06 5090.26 5092.43 -2.17 22052 5090.94 5093.38 -2.44 5111.38 5112.70 -1.32 22054 5111.90 5114.35 2.45 23013 5141.02 5139.39 5138.24 5140.63 -2.39 1.63 5139.10 5140.81 23058 5140.12 5139.37 0.75 -1.71 23085 5139.60 5138.07 5138.25 5139.54 -1.29 1.53 23096 5140.50 5140.77 -0.275138.97 5141.66 -2.6923122 5136.30 5135.94 0.36 5135.63 5138.17 2.54 5139.82 23134 5139.60 0.22 5138.18 5140.63 -2.4523135 5145.00 5143.49 1.51 5144.10 5144.84 -0.7423150 5139.10 5137.82 1.28 5138.05 5139.34 -1.29 5140.85 -0.59 5139.86 5141.86 2.00 23179 5140.26 23182 5112.80 5115.02 -2.22 5112.84 5114.97 -2.13-2.59 23185 5144.70 5141.84 2.86 5139.99 5142.58 5140.12 5138.70 5141.31 2.61 23188 5140.15 0.03 23191 5140.37 5142.38 -2.01 5139.98 5142.98 -3.00 23223 5138.80 5138.87 -0.07 5137.20 5139.74 2.54 5139.59 5142.36 24010 5140.20 5141.81 -1.61 2.77 -2.77 24092 5139.10 5141.70 -2.605139.24 5142.01 5154.13 2.94 5155.85 5152.94 2.91 5157.06 24122 24200 5138.17 5138.76 0.59 5137.56 5138.94 -1.38 5212.88 -0.15 25022 5213.78 5212.74 1.04 5212.73 5179.16 25028 5180.40 5178.78 1.62 5179.11 -0.05 5161.95 5163.73 -1.78 5161.76 5164.11 -2.35 26010 26015 5144.52 5145.64 -1.12 5145.66 5145.55 0.11 5145.45 -2.75 5147.67 5148.20 26017 5145.19 -2.48 -0.09 5149.17 5149.26 5148.65 5149.73 -1.08 26020 26040 5147.03 5148.36 -1.33 5147.03 5147.32 -0.29-0.57 5145.79 5145.65 0.14 26041 5145.37 5145.94 5145.68 5144.61 1.07 26046 5145.30 5144.73 0.57 26049 5150.71 5150.76 -0.05 5150.88 5151.19 -0.315154.45 2.47 2.89 5156.92 26050 5156.97 5154.08 5162.27 5160.52 1.75 26062 5163.07 5160.09 2.98 (Continued)

Table 5 (C	Table 5 (Concluded)							
	Stead	y State Calibrat	ion	Tra	nsient Calibrati	on		
Observation Well No.	Observed Head ft	Calculated Head ft	Head Diff. ft	Observed Head ft	Calculated Head ft	Head Diff. ft		
26063	5182.16	5185.03	-2.88	5183.15	5185.58	-2.43		
26065	5161.70	5160.95	0.75	5161.12	5161.89	-0.77		
26068	5158.96	5159.38	-0.42	5159.03	5159.96	-0.93		
26073	5176.95	5178.99	-2.04	5176.06	5178.17	-2.12		
26076	5151.19	5151.22	-0.03	5151.41	5151.78	-0.37		
26081	5148.00	5147.39	0.61	5147.43	5147.71	-0.28		
26083	5150.20	5149.13	1.07	5152.55	5149.61	2.94		
26085	5179.38	5178.47	0.91	5178.84	5179.07	-0.23		
26088	5142.91	5144.81	-1.91	5142.30	5145.09	-2.79		
26124	5154.31	5154.45	-0.15	5154.41	5153.34	1.07		
26133	5146.14	5146.42	-0.28	5146.72	5145.95	0.77		
26143	5174.73	5174.56	0.17	5173.80	5173.88	-0.08		
26159	5201.04	5199.01	2.03	5199.75	5198.85	0.90		
26160	5143.90	5144.35	-0.45	5144.46	5144.33	0.13		
26166	5151.44	5152.65	-1.20	5151.11	5152.79	-1.68		
26168	5155.51	5157.33	-1.82	5155.80	5158.26	-2.46		
26169	5148.09	5149.43	-1.34	5148.27	5149.46	-1.19		
26170	5140.77	5142.71	-1.94	5141.82	5143.32	-1.50		
26173	5147.71	5148.97	-1.26	5148.60	5148.18	0.42		
27003	5097.70	5097.46	0.24	5097.81	5097.68	0.13		
27017	5148.10	5145.82	2.28	5147.63	5145.76	1.87		
27019	5148.53	5145.58	2.95	5148.06	5145.48	2.58		
27024	5125.80	5125.96	-0.16	5124.79	5126.53	-1.74		
27040	5120.80	5120.91	-0.11	5119.70	5120.86	-1.16		
27041	5113.70	5112.14	1.56	5112.72	5113.98	-1.26		
27051	5128.30	5126.25	2.05	5128.39	5126.01	2.38		
27056	5098.40	5097.59	0.81	5097.33	5097.53	-0.20		
27059	5127.30	5126.71	0.59	5126.41	5126.64	-0.23		
27064	5093.69	5093.52	0.17	5093.25	5093.57	-0.32		
27072	5095.80	5095.80	-0.01	5095.75	5096.06	-0.31		
27073	5097.90	5098.79	-0.89	5097.93	5098.98	-1.05		
27080	5120.00	5117.14	2.86	5119.07	5118.03	1.04		
27084	5136.40	5138.70	-2.30	5135.82	5138.49	-2.67		
35031	5174.21	5172.79	1.42	5173.22	5172.54	0.68		
35040	5165.08	5162.63	2.45	5164.40	5162.94	1.46		
35048	5216.78	5213.85	2.93	5216.27	5214.46	1.81		
35079	5197.98	5196.61	1.37	5199.06	5198.85	0.21		
35091	5182.20	5184.75	-2.55	5182.04	5184.98	-2.94		

Table 6 Steady-State Mass Balance							
Item	Recharge rate (gpm)	Discharge rate (gpm)					
Precipitation	128.28						
Denver Sands	82.8						
Boundary Inflow	622.64	434.26					
Basin A Neck Containment System	14.46	14.46					
North Boundary Containment Treatment System		84.6					
Northwest Boundary Containment System		314.69					
Basin F IRA	2.0	2.0					
Total	850.21	850.21					

model. The particles move through the model domain by using computed velocity vectors from each node. Forty separate particles were released in the model domain. The resulting flowlines are shown in Figure 26. The release point for each particle was selected so that the resulting flowlines would generally follow major groundwater flow routes. The flowlines indicate that the model can generally predict contaminant flow paths within the model domain.

### Water Budget

The water budget under steady-state conditions is based on various inflow and outflow components within the model area. The hydrologic budget results illustrate which inflow and outflow components have an impact on the model area.

The largest source of recharge water into the model area is boundary inflow (underflow), which accounts for 73 percent of all recharge water. The remaining 27 percent of recharge water is from precipitation (16 percent), Denver Fm sands (9 percent), and the Basin A Neck containment system (2 percent), respectively.

The water budget indicates that the largest discharge mechanisms are boundary outflow (underflow), which accounts for 50 percent of all discharge water. The remaining 50 percent of discharge water is to the NWCS (38 percent), NBCTS (10 percent), and the Basin A Neck Containment System (2 percent). These results confirm that the containment systems have a major influence on the total flow system within the model domain.

Boundary inflow (underflow) accounts for the largest amount of both recharge and discharge within the model area. The boundary volumetric flows were computed by the model based on a constant head boundary condition. A summary of the inflow and outflow components affecting the groundwater flow is shown in Table 6. The flow components and their relative locations are

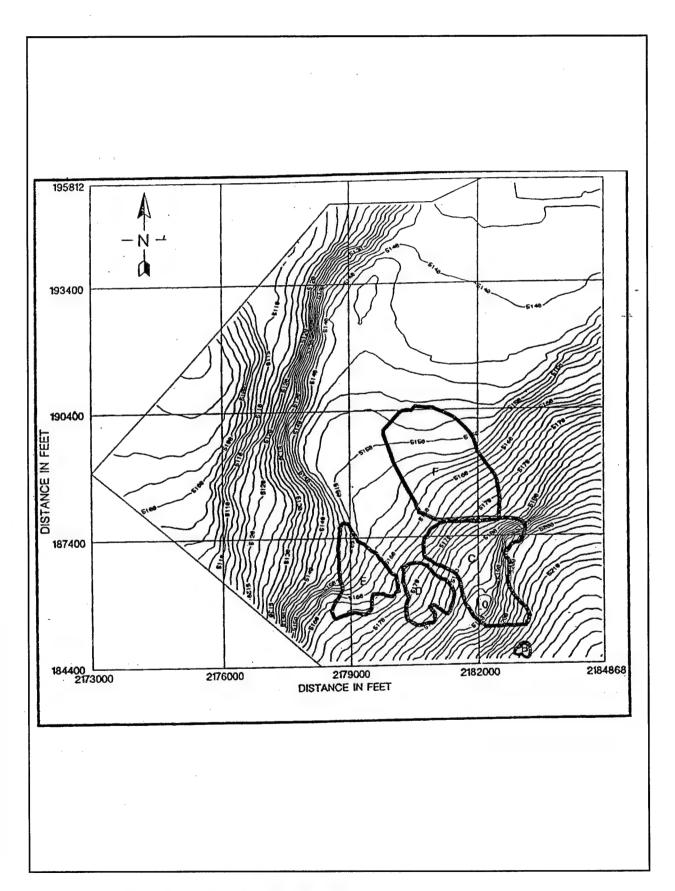


Figure 24. Computed heads from model calibration

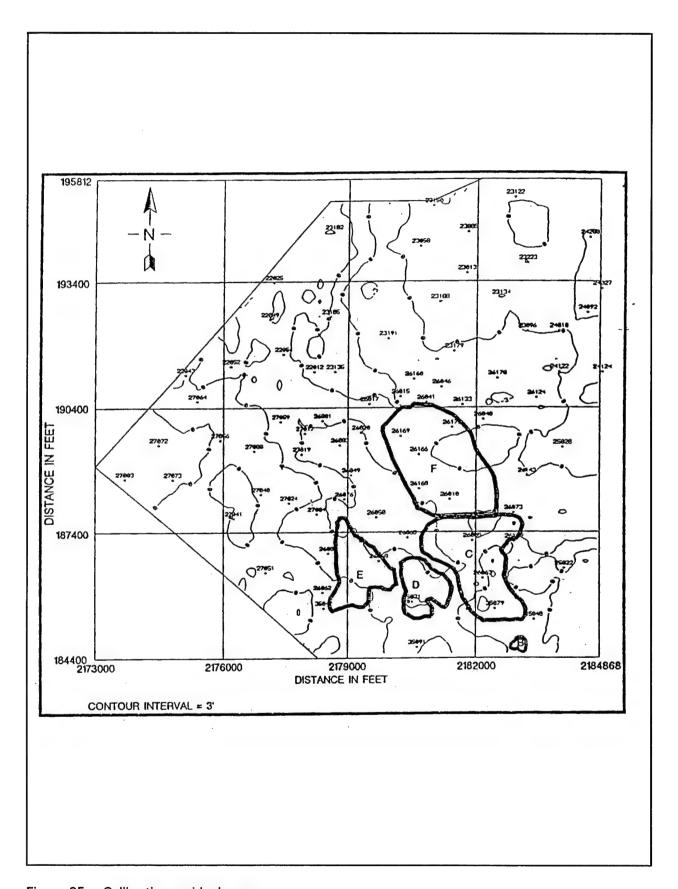


Figure 25. Calibration residual map

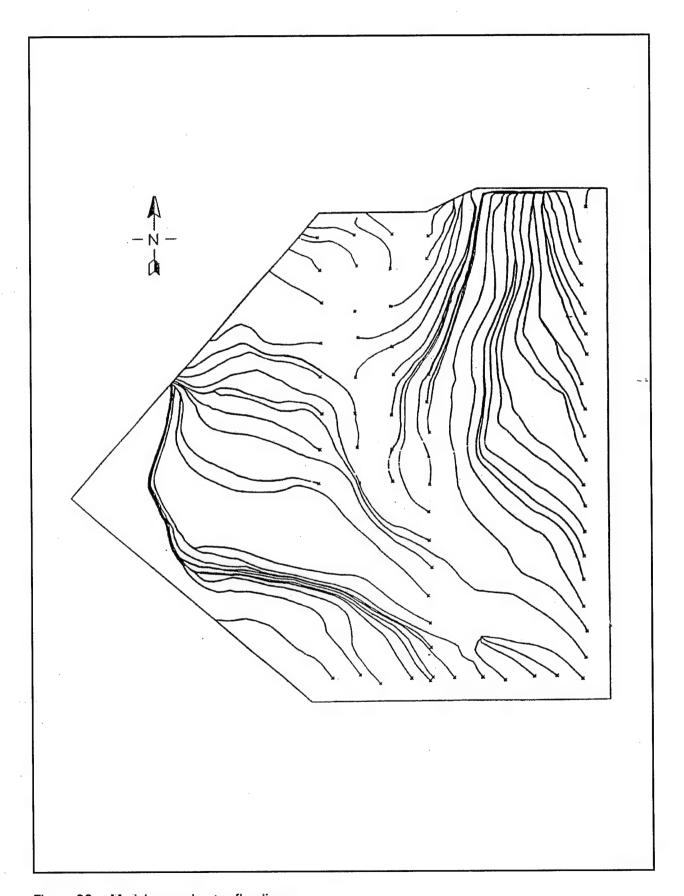


Figure 26. Model groundwater flowlines

shown graphically in Figure 27 which illustrates the flows entering and exiting the model area from recharge sources, boundary containment systems, and model boundaries.

#### **Calibration Results**

The steady-state model calibration resulted in flow paths, mass balance, and fluxes across contamination control systems that are realistic and that compare well with previous work. The results from the calibration of the Basin F Subregional Model are acceptable as measured by the criteria provided by Ebasco. The results of the model based on the criteria used are provided in detail within this report. A copy of the steady-state calibration input data file is given in Appendix B. Based on the successful results of the steady-state calibration, a transient calibration of the model was performed.

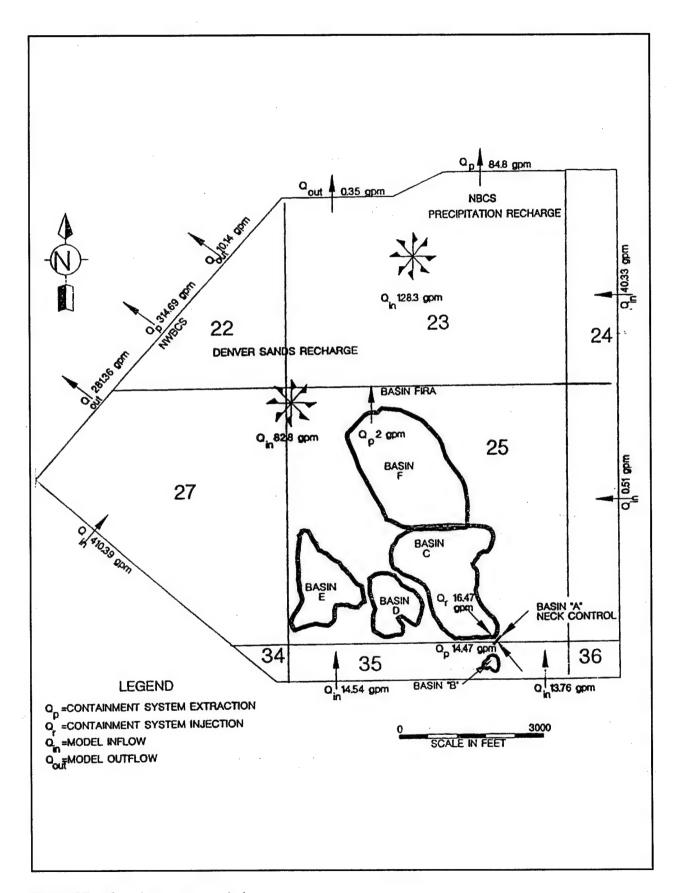


Figure 27. Steady-state mass balance

### 5 Transient Model Calibration

The reliability of parameters used for steady-state calibration of the ground-water model can be verified with transient simulations. Unlike the steady-state calibration, transient simulations, which indicate how the hydrologic system will respond to stress require that water levels change with time. Therefore, the steady-state calibration data must be converted to transient data. The transient calibration procedure consists of the following steps:

- a. Determine the time parameters for the transient calibration simulations. The parameters include the length of the calibration simulation, the length of the stress period, the length of the time step, and a multiplication factor for increasing the size of the time step. The length of the simulation determines the time period to calibrate the model. The time period selected is usually based on the amount of data available on the model area. The time period selected for the transient calibration of this model is the 2nd quarter of the 1992 Fiscal Year (FY). The length of the simulation is one and a half years. The length of the stress period is quarterly (90 days), the time step is 1 hr, and the time multiplication factor is 1.5.
- b. Collect and adjust input data. All parameters (input data) that have changed over time, and parameters not applied for steady-state calibration but are required for transient calibration were collected. The data collected consist of measured (observed) well water-level elevations, measured and estimated recharge/discharge values, and estimated storage coefficients. The observed head values for the 74 wells that the model will attempt to match during transient calibration are shown in Table 5. The observation well water level elevation data were provided by DP Associates, Inc. The measured pumping and injection rates for the NBCTS, NWBCS, and Basin A Neck containment system used for transient calibration are shown in Tables 7 through 9. Measured precipitation values used for model calibration are shown in Table 10. Table 11 summarizes the transient mass balance. Precipitation data were provided by RMA and compiled as part of their ongoing precipitation data collection program. The storage coefficients used for model calibration range from 0.05 to 0.25. The North Boundary Model Report reference indicated that results from long term (72 hr) pump testing produced a range of storage coefficient values from 0.25 down to 0.001.

Table 7
North Boundary Containment System Pumping Rates for Transient Simulation

		Rate (gpm)					
Well No.	Well ID Code	FY 91 QTR 1	FY 91 QTR 2	FY 91 QTR 3	FY 91 QTR 4	FY 92 QTR 1	FY 92 QTR 2
23301	17	0.250	0.250	0.250	0.250	0.189	0.350
23302	18	2.775	2.775	2.775	2.775	0.000	0.350
23303	19	3.875	3.875	3.875	3.875	7.490	6.800
23304	20	3.450	3.450	3.450	3.450	0.489	7.000
23305	21	5.800	5.800	5.800	5.800	0.000	1.600
24306	22	7.775	7.775	7.775	7.775	0.031	0.000
24307	23	11.43	11.43	11.43	11.43	0.092	8.000
24308	24	1.246	1.246	1.246	1.246	0.092	0.000
24309	25	1.173	1.173	1.173	1.173	0.092	0.000
24310	26	2.052	2.052	2.052	2.052	0.092	0.000
24311	27	2.346	2.346	2.346	2.346	15.01	0.000
24312	28	4.032	4.032	4.032	4.032	0.000	1.000
24313	29	15.98	15.98	15.98	15.98	0.000	0.650
23334	15	1.300	1.300	1.300	1.300	0.000	0.000

- c. Adjust and update boundary conditions. Constant-head nodes were assigned as boundary conditions for the steady-state calibration of the model. Constant-head boundary nodes were changed to prescribed flux nodes to fix the amount of underflow through the boundaries during the application of changing stresses associated with the operation of the containment systems. The boundary fluxes used for the transient simulation were calculated by the model.
- d. Calibration of the model. Data inputs were made, boundary conditions were adjusted, and model transient calibration simulations were performed. Model adjustable parameters were adjusted so the model-computed heads approximate as closely as possible measured (observed) monitor well head values. When 95 percent of all observation wells had a residual value within plus or minus 3 ft and previously stated criteria were met, the model was considered calibrated.

Table 8 Northwest Boundary Containment System Pumping/Recharge Rates for Transient Simulation									
		Rate (gpm)							
Well No.	Well ID Code	FY 91 QTR 1	FY 91 QTR 2	FY 91 QTR 3	FY 91 QTR 4	FY 92 QTR 1	FY 92 QTR 2		
			Pi	umping					
22301	41	47.40	47.76	16.54	3.08	8.66	17.25		
22302	41	47.40	47.76	16.54	3.08	8.66	17.25		
22303	40	20.03	1.27	23.32	14.78	25.04	26.09		
22304	40	20.03	1.27	23.32	14.78	25.04	26.09		
22305	39	0.01	0.01	0.00	21.15	16.90	14.19		
22306	39	0.01	0.01	0.00	21.15	16.90	14.19		
22307	38	33.71	38.88	30.41	22.06	32.07	31.27		
22308	38	33.71	38.88	30.41	22.06	32.07	31.27		
22309	37	15.38	15.45	44.24	26.25	27.60	29.75		
22310	37	15.38	15.45	44.24	26.25	27.60	29.75		
22311	30	0.04	0.02	0.19	0.19	0.205	0.157		
22312	31	30.20	36.86	33.05	25.98	28.41	22.15		
22313	32	19.71	24.47	14.55	0.00	22.43	25.45		
22314	33	0.51	0.00	0.0015	0.00	7.17	19.70		
22315	34	37.13	43.42	41.06	38.58	42.55	28.98		
22316	35	35.08	7.52	0.37	0.00	0.00	0.87		
22317	36	34.76	29.66	28.92	3.15	2.14	2.06		
			Re	charge					
27422	58	0.00	0.00	0.00	36.90	17.90	50.10		
27423	58	0.00	0.00	0.00	81.60	62.60	35.50		
27424	59	0.00	0.00	0.00	54.80	76.60	79.60		
27425	59	0.00	0.00	0.00	73.10	69.80	67.60		

#### **Transient Calibration Results**

The results from the transient calibration of the Basin F Subregional Ground-water Model are acceptable, as measured by the previously stated criteria. The model calibration resulted in a close approximation of the measured head values of 74 observation wells. The parameter adjusted during the transient calibration of the model was the storage coefficient. The residual values for the 74 observation wells are given in Table 5. All wells are within the 3 ft criteria. A copy of the transient calibration input data file is given in Appendix C. Transient calibration of the Basin F Groundwater Model adds validity to the parameters and input data used for the modeling effort.

Table 9 Basin A Neck Containment System Pumping/Recharge Rates for **Transient Simulation** 

		Rate (gpm)					
Well No.	Well ID Code	FY 91 QTR 1	FY 91 QTR 2	FY 91 QTR 3	FY 91 QTR 4	FY 92 QTR 1	FY 92 QTR 2
	Pumping						
35301	42	1.628	1.140	1.265	1.165	0.461	0.329
35302	43	3.440	2.408	2.673	2.465	2.693	1.925
35303	44	1.131	0.792	0.878	0.809	1.359	0.970
35304	42	1.628	1.140	1.265	1.165	0.461	0.329
35305	43	3.440	2.408	2.673	2.465	2.693	1.925
35306	44	1.131	0.792	0.878	0.809	1.359	0.970
35307	44	1.131	0.792	0.878	0.809	1.359	0.970
23311	45 <sup>1</sup>	0.007	0.030	0.340	0.030	1.13061	1.500
			Rech	arge²			
46	Trench A	0.189	0.146	0.180	0.187	0.298	0.338
47	Trench A	0.189	0.146	0.180	0.187	0.298	0.338
48	Trench A	0.189	0.146	0.180	0.187	0.298	0.338
49	Trench A	0.189	0.146	0.180	0.187	0.298	0.338
50	Trench B	0.474	0.366	0.450	0.468	0.348	0.438
51	Trench B	0.474	0.366	0.450	0.468	0.348	0.438
52	Trench B	0.474	0.366	0.450	0.468	0.348	0.438
53	Trench B	0.474	0.366	0.450	0.468	0.348	0.438
54	Trench C	0.259	0.200	0.245	0.256	0.234	0.294
55	Trench C	0.259	0.200	0.245	0.256	0.234	0.294
56	Trench C	0.259	0.200	0.245	0.256	0.234	0.294
57	Trench C	0.259	0.200	0.245	0.256	0.234	0.294

Basin F IRA discharge water is represented by ID Code 45.
 The system's recharge water is entered through the Basin A Neck recharge trench system. Each recharge trench is represented by a series of 4 wells.

Table 10 Transient Precipitation Rates							
Total Precipitation Infiltration Rates							
			High Elevation (8.28%) Low Elevation (5.529				
Period	in.	ft/day	ft/day	in./qtr	ft/day	in./qtr	
FY 91, QTR 1	2.58	0.002389	0.000198	0.214	0.000132	0.143	
FY 91, QTR 2	1.60	0.001481	0.000123	0.133	0.000082	0.089	
FY 91, QTR 3	6.55	0.006065	0.000502	0.542	0.000335	0.362	
FY 91, QTR 4	8.58	0.007944	0.000658	0.711	0.000439	0.474	
FY 92, QTR 1	3.56	0.003296	0.000273	0.295	0.000182	0.197	
FY 92, QTR 2	7.73	0.00438	0.000363	0.392	0.000242	0.261	

Table 11 Transient Mass Balance							
Item	Recharge rate (gpm)	Discharge rate (gpm)					
Precipitation	160.60						
Denver Sands	61.88						
Boundary Inflow	297.25	385.69					
Basin A Neck Containment System	4.28	8.91					
North Boundary Containment System		25.75					
Northwest Boundary Containment System		336.46					
Wells Section 27 (NWBCS)	232.80						
Basin F IRA	2.0	2.0					
Total	758.81	758.81					

## 6 Sensitivity Analysis

Data used in any groundwater modeling effort are estimated, interpreted, and inferred from other data. Because of the uncertainties in the values of key parameters such as the hydraulic conductivity and recharge, it was determined that a sensitivity analysis should be performed. The analysis can determine the sensitivity of the flow field to the variation of key parameters. Each parameter was uniformly varied by a multiple of the calibrated value over the model area while all other parameters and variables were held constant. The measured water levels at 74 observation wells were compared to the computed water levels for the same wells for each parameter variation to determine the effect of the parameter change on the average water levels.

The Root Mean Square Error (RMSE) method was applied to the observed and calculated heads to determine the sensitivity of the model to specific parameter adjustments. The RMSE was calculated as,

$$RMSE = \sqrt{\frac{\sum_{i=1}^{N} \left(H_i^m - H_i^c\right)^2}{N}}$$
(3)

where

N = number of observations

 $H_i^m$  = the measured water level, in ft

 $H_i^c$  = the computed water level, in ft

The RMSE indicates the average amount the measured water levels differ from calculated water levels. The RMSE for the transient calibrated model was 1.5 ft, which indicates that on the average the difference between the measured and calculated heads for the 74 observation wells is 1.5 ft. The smaller the RMSE value, the better the calculated head matches the measured head.

The parameter adjustments applied were 0.1, 0.5, 1.5, 2.0, and 3.0 times the calibrated values for the two parameters. The RMSE values for each parameter variation depicting the range of sensitivity are shown in Figure 28; a multiple of one indicates the calibrated RMSE value. The model flow field was defined as sensitive to changes in parameter values when the RMSE was 10 percent greater than the RMSE of the calibrated model. Based on the established criteria, the

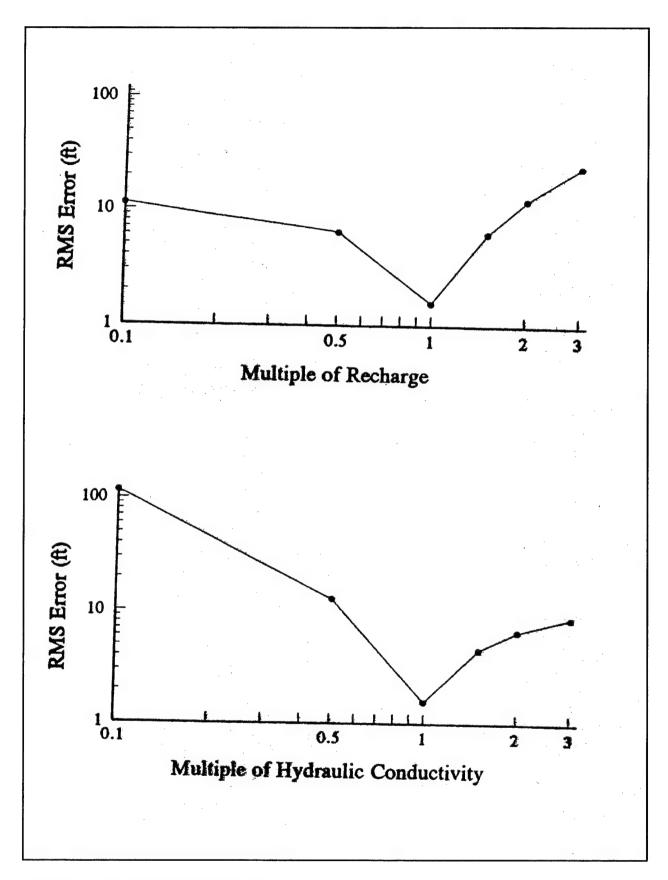


Figure 28. Sensitivity analysis results

flow field is sensitive to all hydraulic conductivity and recharge multiples, as shown in Figure 28. Therefore, the model is sensitive to adjustments in these parameters.

Sensitivity analysis is useful in evaluating the degree that errors in parameters affect the accuracy of the model. If an investigation indicates that a modification of any one of the parameters is required and the parameter's RMSE increased considerably by the change, then a new calibration would be suggested.

### 7 Simulation of Remedial Alternatives

Contaminant migration at RMA is largely controlled by advective flow. To assist in the evaluation of nine remedial alternatives, the Basin F Subregional Flow Model was used to simulate each alternative under steady-state conditions. The results of each simulation will be used to determine the feasibility, the effectiveness of each remedial alternative and its impact on existing control systems, and the regional groundwater flow. The alternative simulations and their results are discussed in this section.

# Description of the Simulated Remedial Alternatives

A list of nine possible groundwater remedial alternatives was identified for the RMA Detailed Analysis. Illustrations of the components to be simulated for each alternative variations are given in Figures 29 through 37. In all figures, pumping wells are represented by solid circles, and recharge wells are represented by open circles. The wells are located at appropriate node locations on the grid. The locations of slurry walls are indicated as solid lines covering nodes which are used to represent the low-permeability slurry wall. The location and extent of low permeability surface cover or clay cap is indicated as a shaded area. The remedial alternative simulation identification codes and a brief description of the alternatives are as follows:

- a. NC-2. Existing Basin F IRA pumping well only.
- b. NC-3A. Extraction system of 13 pumping wells.
- c. NC-3B. Extraction system of 13 pumping wells with 14 recharge wells.
- d. NC-3C. Extraction and recharge system as simulation NC-3B with one slurry wall.
- e. NC-3D. Extraction system of 16 pumping wells.

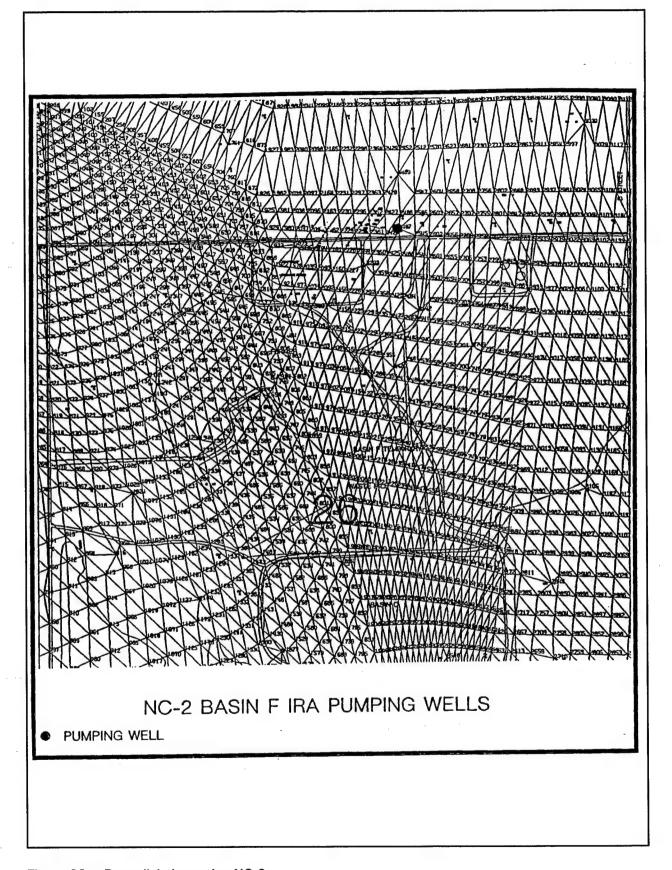


Figure 29. Remedial alternative NC-2

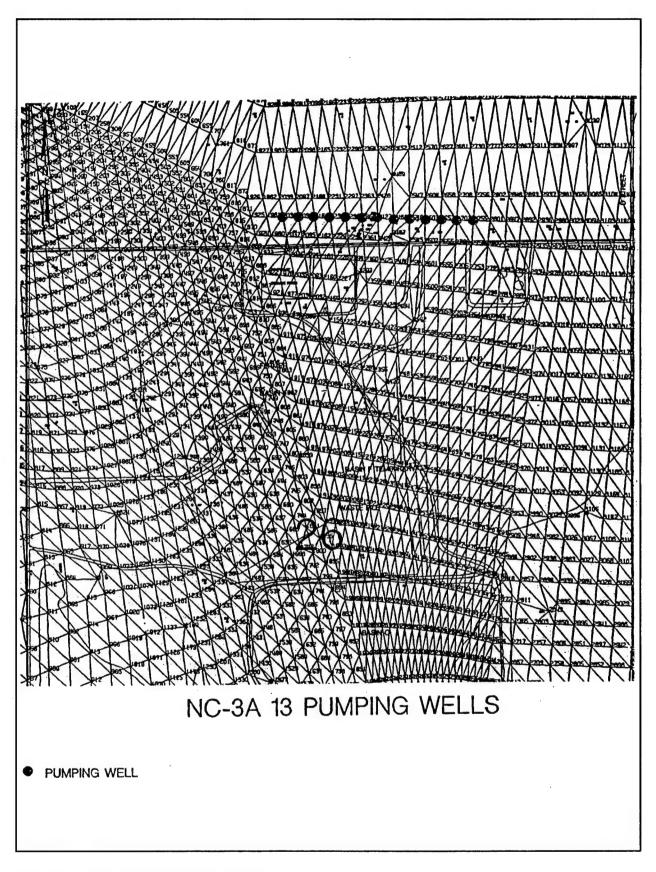


Figure 30. Remedial alternative NC-3A

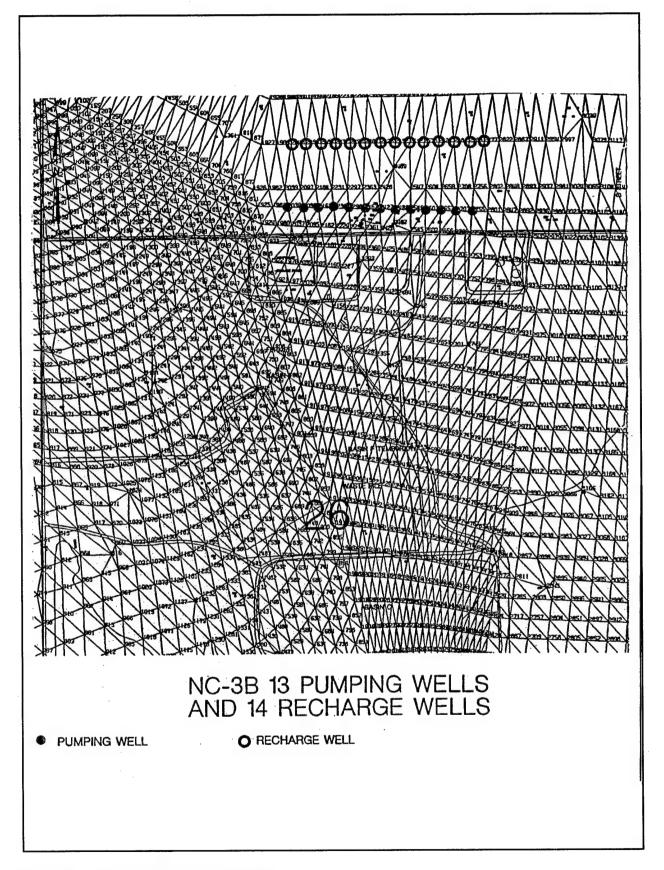


Figure 31. Remedial alternative NC-3B

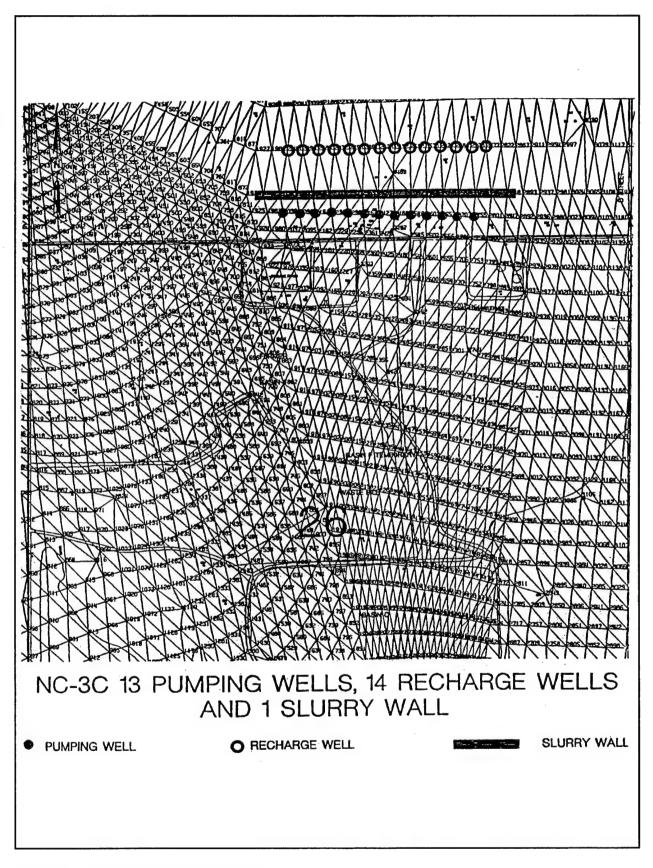


Figure 32. Remedial alternative NC-3C

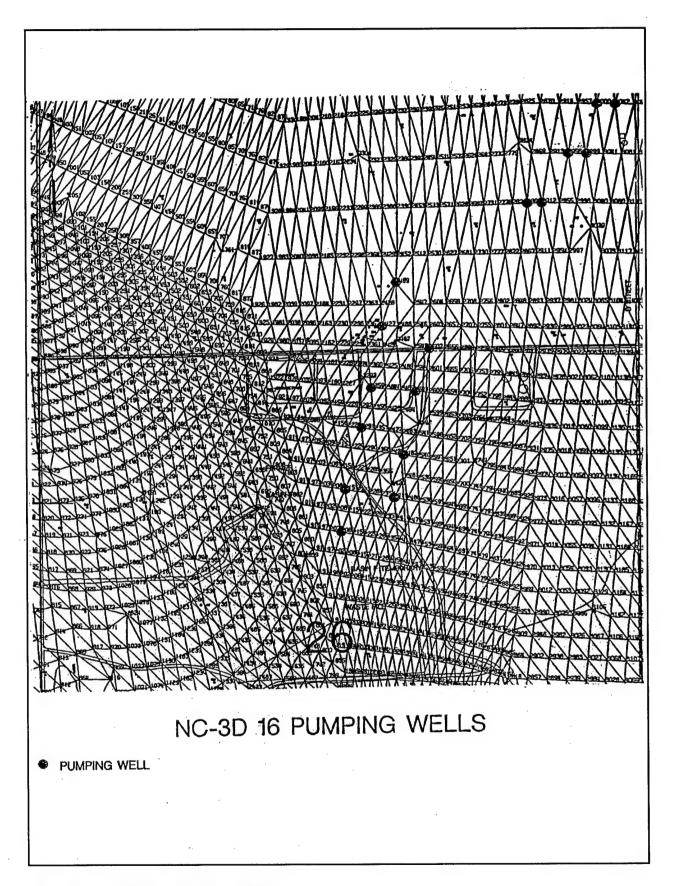


Figure 33. Remedial alternative NC-3D

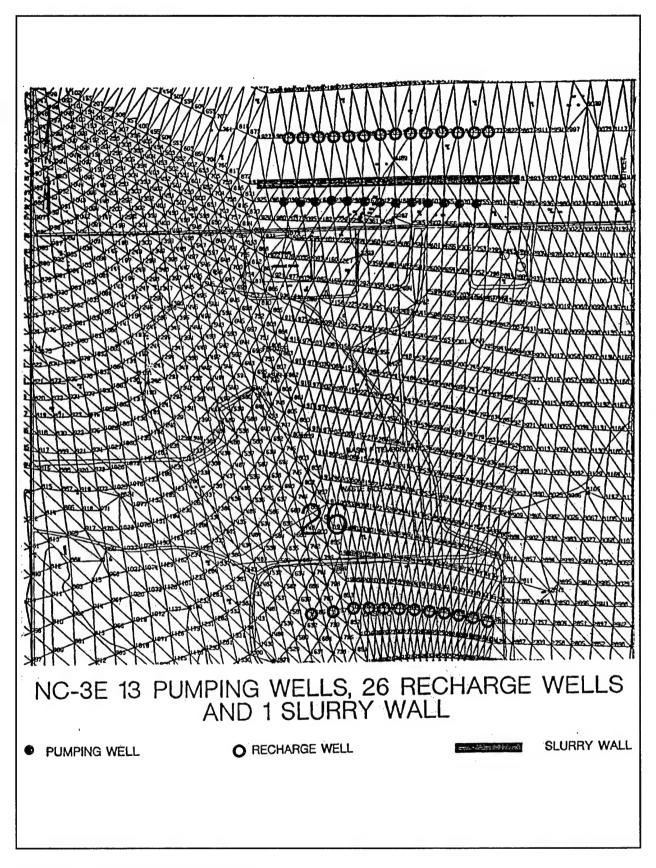


Figure 34. Remedial alternative NC-3E

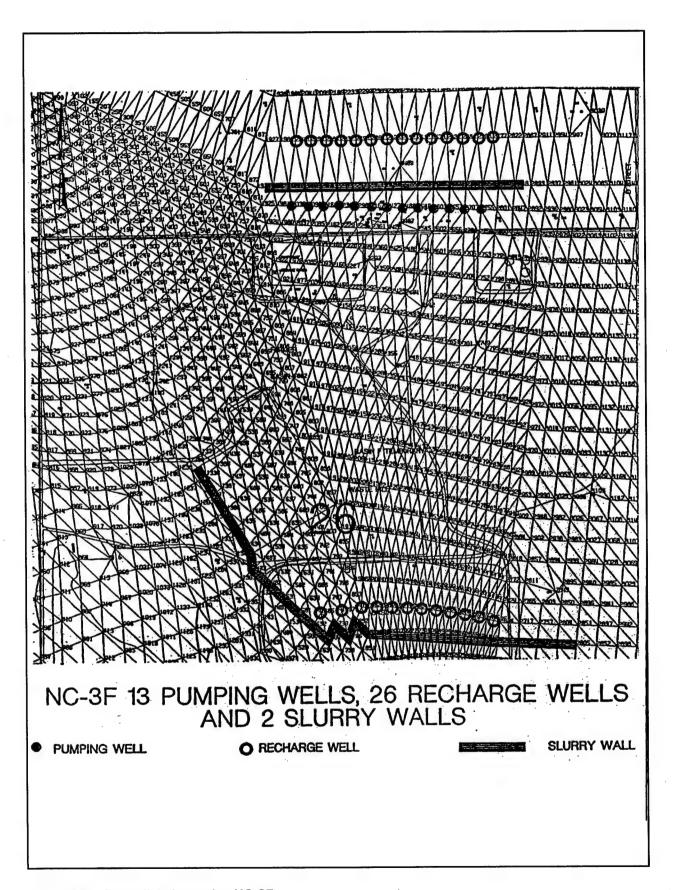


Figure 35. Remedial alternative NC-3F

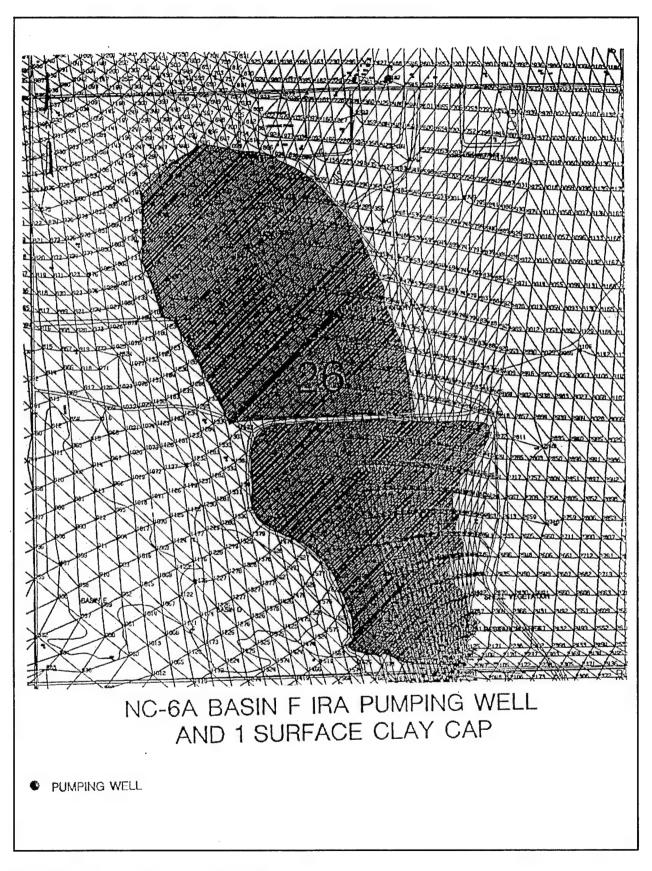


Figure 36. Remedial alternative NC-6A

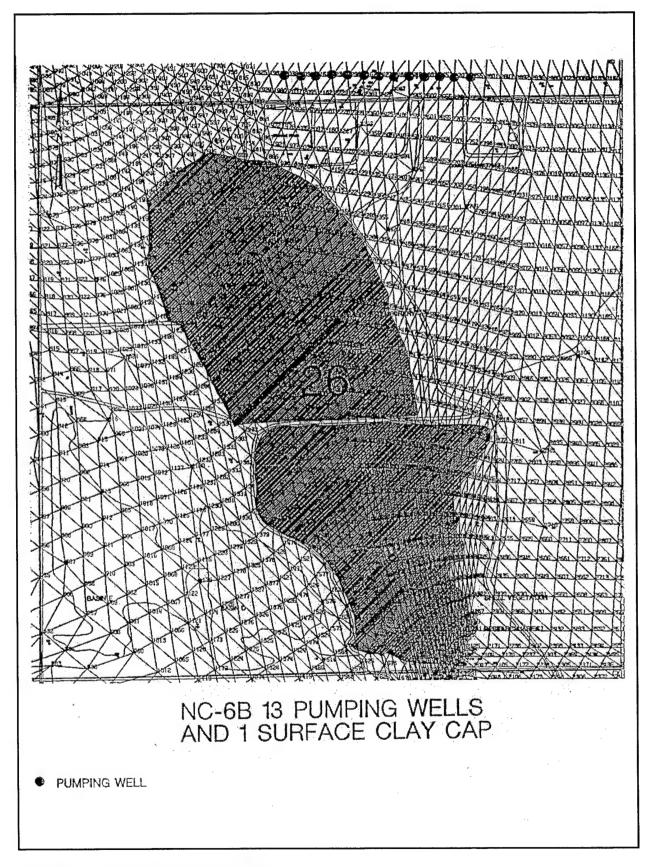


Figure 37. Remedial alternative NC-6B

- f. NC-3E. Extraction, recharge, and slurry wall system of simulation NC-3C, with 12 additional recharge wells.
- g. NC-3F. Extraction, recharge, and slurry wall system of simulation NC-3E, with an additional slurry wall.
- NC-6A. Existing Basin F IRA pumping well with a clay cap over Basins F and C.
- NC-6B. Extraction system of 13 pumping wells, with a clay cap over Basins F and C.

#### **Simulation Approach**

The approach taken for each simulation was to fix the water level elevation (constant head) at each extraction well to establish the flux to the well. The resulting flux of the extraction system must be sufficient to provide contaminant (particle) capture at the extraction wells. Contaminant capture is verified with a particle-tracking program. If the extraction rate is not sufficient to provide particle capture, then the ground-water elevations at the pumping wells are lowered and the process is repeated. The extracted water is recharged at specified locations at a rate equivalent to the extraction system rate. For simulations with slurry walls, the walls are simulated as having a thickness of three feet and a conductivity equivalent to  $10^{-7}$  cm/sec. The clay cap covering Basin F and C was simulated by setting the effective recharge from precipitation to zero on the capped areas.

#### Simulation Results

The resulting pumping and recharge rates from the simulation of each remedial alternative are shown in Tables 12 through 20. The remedial alternatives have no major impact on the overall subregional groundwater flow within the model area or on the present contamination control systems. Because of the minor effect of the alternatives on the overall flow system, they will not be discussed individually or in any detail. The results from simulation of alternative NC-3A and NC-3B indicate that more water is flowing across the 9th Avenue northward from the Basin F area than was previously reported. Because the flow rate is a function of the hydraulic conductivity and the saturated thickness, the model indicates that both these parameters should be verified in the area of these alternatives. The bedrock and USF base elevations drive the saturated thickness, and it is this parameter which is most important to verify.

The quantitative results provided from the simulation of each alternative are within a reasonable margin of error and can be used for the relative comparison of the remedial alternatives to aid in the remedial alternative selection process.

Table 12 Alternative NC-2 Simulation Results					
	Location				
Well No.	X-Coord (ft)	Y-Coord (ft)	Pumping rate (gpm)		
23311	2181488	191226	4.713		

Table 13 Alternative NC-3A Simulation Results					
		Location			
Well No.	X-Coord (ft)	Y-Coord (ft)	Pumping rate (gpm)		
P1	2180519	191392	1.25		
P2	2180659	191387	0.50		
Р3	2180800	191383	0.50		
P4	2180940	191378	0.50		
P5	2181080	191374	0.50		
P6	2181221	191369	0.50		
P7	2181361	191365	0.50		
P8	2181501	191360	0.50		
P9	2181642	191356	0.50		
P10	2181782	191352	0.75		
P11	2181923	191348	1.00		
P12	2182063	191344	1.00		
P13	2182203	191339	1.75		
Total			9.75		

Table 14 Alternative NC-3B Simulation Results							
Pumping				Rec	harge		
	Loca	tion			Loca	tion	
Well No.	X-Coord (ft)	Y-Coord (ft)	Rate (gpm)	Well No.	X-Coord (ft)	Y-Coord (ft)	Rate (gpm)
P1	2180519	191392	1.25	RW1	2180546	191984	0.696
P2	2180659	191387	0.50	RW2	2180682	191984	0.696
Р3	2180800	191383	0.50	RW3	2180817	191984	0.696
P4	2180940	191378	0.50	RW4	2180953	191985	0.696
P5	2181080	191374	0.50	RW5	2181089	191985	0.696
P6	2181221	191369	0.50	RW6	2181224	191986	0.696
P7	2181361	191365	0.50	RW7	2181360	191986	0.696
P8	2181501	191360	0.50	RW8	2181495	191987	0.696
P9	2181642	191356	0.50	RW9	2181631	191988	0.696
P10	2181782	191352	0.75	RW10	2181766	191989	0.696
P11	2181923	191348	1.00	RW11	2181902	191990	0.696
P12	2182063	191344	1.00	RW12	2182037	191990	0.696
P13	2182203	191339	1.75	RW13	2182173	191992	0.696
				RW14	2182309	191992	0.696
Total			9.75	Total			9.75

	Table 15 Alternative NC-3C Simulation Results						
Pumping				Reci	harge		
	Loca	tion			Loca	tion	
Well No.	X-Coord (ft)	Y-Coord (ft)	Rate (gpm)	Well No.	X-Coord (ft)	Y-Coord (ft)	Rate (gpm)
P1	2180519	191392	1.084	RW1	2180546	191984	0.798
P2	2180659	191387	0.423	RW2	2180682	191984	0.798
Р3	2180800	191383	0.421	RW3	2180817	191984	0.798
P4	2180940	191378	0.521	RW4	2180953	191985	0.798
P5	2181080	191374	0.578	RW5	2181089	191985	0.798
P6	2181221	191369	0.378	RW6	2181224	191986	0.798
P7	2181361	191365	0.673	RW7	2181360	191986	0.798
P8	2181501	191360	0.106	RW8	2181495	191987	0.798
P9	2181642	191356	0.203	RW9	2181631	191988	0.798
P10	2181782	191352	0.877	RW10	2181766	191989	0.798
P11	2181923	191348	0.877	RW11	2181902	191990	0.798
P12	2182063	191344	1.061	RW12	2182037	191990	0.798
P13	2182203	191339	3.967	RW13	2182173	191992	0.798
				RW14	2182309	191992	0.798
Total			11.17	Total			11.17

Table 16 Alternative NC-3D Simulation Results					
		Location			
Well No.	X-Coord (ft)	Y-Coord (ft)	Pumping rate (gpm)		
P1	2183220	193365	22.479		
P2	2183377	193362	23.590		
P3	2182977	192904	7.343		
P4	2183130	192902	4.740		
P5	2182633	192448	4.189		
P6	2182759	192450	3.652		
P7	2181480	191746	2.192		
P8	2181361	191365	0.003		
P9	2181780	191152	0.371		
P10	2181264	190806	0.786		
P11	2181651	190765	1.287		
P12	2181177	190438	0.263		
P13	2181550	190187	1.800		
P14	2181029	189888	0.011		
P15	2181465	189808	0.413		
P16	2181197	189464	0.084		
Total			73.20		

Table 17 Simulation NC-3E Simulation Results **Pumping** Recharge Location Location Well X-Coord Y-Coord Well X-Coord Y-Coord Rate Rate (ft) No. No. (ft) (gpm) (ft) (ft) (gpm) P1 2180519 191392 1.322 RW1 2180546 191984 0.484 P2 2180659 191387 0.424 RW2 2180682 191984 0.484 **P3** 2180800 191383 0.407 RW3 2180817 191984 0.484 2180940 191378 0.516 RW4 2180953 191985 0.484 **P4 P5** 2181080 191374 0.579 RW5 2181089 191985 0.484 **P6** 2181221 191369 0.567 RW6 2181224 191986 0.484 Р7 2181361 191365 0.368 RW7 2181360 191986 0.484 **P8** 2181501 191360 0.043 RW8 2181495 191987 0.484 Р9 2181642 191356 0.391 RW9 2181631 191988 0.484 **RW10** 2181766 191989 0.484 P10 2181782 191352 0.911 2181902 191990 P11 2181923 191348 0.908 **RW11** 0.484 P12 2182063 191344 1.101 **RW12** 2182037 191990 0.484 P13 2182203 191339 4.570 **RW13** 2182173 191992 0.484 **RW14** 2182309 191992 0.484 **RW15** 2180767 187702 0.484 **RW16** 2180957 187715 0.484 187747 **RW17** 2181136 0.484 **RW18** 2181272 187748 0.484 **RW19** 2181407 187744 0.484 **RW20** 2181541 187737 0.484 **RW21** 2181673 187726 0.484 **RW22** 2181804 187710 0.484 **RW23** 2181934 187692 0.484 **RW24** 2183662 187669 0.484 **RW25** 2182188 187642 0.484

12.11

Total

Total

12.11

ł .	Table 18 Alternative NC-3F Simulation Results						
Pumping			Recharge				
	Location		Location	Ĺ	Location		
Well No.	X-Coord (ft)	Y-Coord (ft)	Rate (gpm)	Well No.	X-Coord (ft)	Y-Coord (ft)	Rate (gpm)
P1	2180519	191392	0.981	RW1	2180546	191984	0.415
P2	2180659	191387	0.340	RW2	2180682	191984	0.415
Р3	2180800	191383	0.167	RW3	2180817	191984	0.415
P4	2180940	191378	0.134	RW4	2180953	191985	0.415
P5	2181080	191374	0.371	RW5	2181089	191985	0.415
P6	2181221	191369	0.396	RW6	2181224	191986	0.415
P7	2181361	191365	0.031	RW7	2181360	191986	0.415
P8	2181501	191360	0.504	RW8	2181495	191987	0.415
P9	2181642	191356	0.275	RW9	2181631	191988	0.415
P10	2181782	191352	0.860	RW10	2181766	191989	0.415
P11	2181923	191348	0.006	RW11	2181902	191990	0.415
P12	2182063	191344	1.947	RW12	2182037	191990	0.415
P13	2182203	191339	4.763	RW13	2182173	191992	0.415
				RW14	2182309	191992	0.415
				RW15	2180766	187701	0.415
				RW16	2180957	187715	0.415
				RW17	2181135	187747	0.415
				RW18	2181272	187747	0.415
				RW19	2181407	187744	0.415
				RW20	2181540	187736	0.415
				RW21	2181673	187725	0.415
				RW22	2181804	187710	0.415
				RW23	2181933	187691	0.415
				RW24	2182061	187668	0.415
				RW25	2182188	187642	0.415
				RW26	2182314	187612	0.415
Total			10.78	Total			10.78

Table 19 Alternative NC-6A Simulation Results					
		Location			
Well No.	X-Coord (ft) Y-Coord (ft)		Pumping rate (gpm)		
23311	2181488	191226	4.367		

Table 20 Alternative NC-6B Simulation Results					
		Location			
Well No.	X-Coord (ft)	Y-Coord (ft)	Pumping rate (gpm)		
P1	2180519	191392	0.948		
P2	2180659	191387	0.157		
P3	2180800	191383	0.155		
P4	2180940	191378	0.195		
P5	2181080	191374	0.125		
P6	2181221	191369	0.013		
P7	2181361	191365	0.011		
P8	2181501	191360	0.019		
P9	2181642	191356	0.015		
P10	2181782	191352	0.020		
P11	2181923	191348	0.029		
P12	2182063	191344	0.038		
P13	2182203	191339	0.483		
Total			2.21		

## 8 Summary and Conclusions

A numerical model of the Basin F subregional groundwater flow at RMA has been constructed as an evaluation tool for comparison of the preliminary design of proposed remedial alternatives and the affect of remedial alternatives on future subregional groundwater flow conditions. The groundwater model simulates steady-state and transient, two-dimensional areal flow in the UFS that is comprised of shallow alluvium and upper weathered Denver Fm materials. The hydraulic conductivity of the alluvium ranged from 2 to 1,500 ft/day. The weathered upper Denver Fm hydraulic conductivity ranged from 0.1 to 14 ft/day. The storage coefficients used for saturated and unsaturated alluvium are 0.25 and 0.05, respectively. All parameter values were within the range of observed or published data.

Sources of water to the UFS include precipitation infiltration and recharge from Denver Fm subcropping sands. The boundary conditions of the study area were modeled as constant-head boundaries and prescribed fluxes. The model domain encompasses approximately 3.6 square miles. The study area's northern and western boundaries are aligned with the NBCTS and the NWBCS. Model calibration and simulation runs are made with CSU finite element code (GW Flow). Steady-state model calibration was based on summer 1990 water-table elevations of 74 observation wells. Transient model verification was based on six quarters of water-level elevations at 74 observation wells ending with the 2nd Quarter fiscal year 1992. There was a good comparison between model calculated and observed water levels over most of the modeled area. Model water budget (mass balance) components, however, were not directly comparable over the entire study area because of limited data, but there was good comparison at the NBCTS, NWBCS, and Basin A Neck System.

The response of the model to adjustments of input parameters was evaluated by sensitivity analysis. The model calibration results degenerate with moderate changes in hydraulic conductivity and recharge rates. Therefore, the model is sensitive to adjustments in these parameters. Significant modifications to these sensitive parameters would probably require a new calibration of the model.

After steady-state calibration and transient verification, the groundwater model was used to evaluate proposed remedial alternatives. Nine remedial alternatives were simulated in an effort to evaluate the ability of each alternative to control contaminated groundwater flow, and impact on future groundwater flow conditions. It should be emphasized that the ability of the calibrated model to replicate past ground water conditions does not necessarily verify its ability to predict future conditions. The simulation is subject to various uncertainties and

assumptions inherent in groundwater modeling process. The simulation results should be regarded as estimates based on currently available data. As new information and data are acquired or revisions in the assumed conceptual model are made, the model should be updated and, if necessary, recalibrated.

The following conclusions are made from the Basin F subregional ground-water flow modeling study.

- a. The upper Denver Fm is an important part of the UFS. In areas of totally unsaturated alluvium the upper weathered Denver Fm provides a mechanism for groundwater flow and contaminant transport through the UFS.
- b. The general direction of groundwater movement within the study area is southeast to northwest. The southeast to northwest flow direction has local variability and is affected by the operation of current containment systems.
- c. The overall effect and influence of recharge from Denver Fm subcropping sands to the UFS is small, but in some local areas the recharge from these sands can be critical to groundwater flow within the UFS.
- d. Steady-state calibration results indicate that the largest source of recharge and discharge to the UFS within the study area is boundary underflow which is the result of established regional groundwater movement through the study area. The North Boundary and Northwest Boundary containment systems combined represent the second largest discharge from the UFS from the study area.
- e. The uncertainty of input parameters (e.g, water-table elevation, bedrock surface elevation, UFS base elevation, hydraulic conductivity, boundary inflows, areal recharge, pumping rates) used for this modeling effort is typical of most modeling efforts. This modeling effort indicates the need for setting quality-control standards for all data. Uniform data standards will decrease the amount of data uncertainty.
- f. Simulations with the calibrated model produced approximate flows in the Basin F area that were different from values reported in previous studies. The difference in flow is primarily because previous studies did not model flow in the weathered Denver Fm in this area.
- g. The quantitative results provided are within a reasonable margin of error and can be used as part of the remedial alternative selection process. They should not be the sole basis for the design of any remedial systems.

## 9 Recommendations

Based on a review of the results of this modeling effort, the following recommendations are made.

- a. The RMA program manager should institute a system that standardizes and establishes quality controls for all data collected as part of the RMA contamination remediation effort, before it becomes part of the RMA official data base.
- b. A study should be undertaken to close all data gaps within the RMA boundary, specifically along major contamination pathways. All data parameters associated with groundwater flow along major pathways must be defined within a range of accuracy, if accurate groundwater flow and contaminant transport analyses are expected.
- c. The base of the UFS must be accurately defined in areas where new control systems are planned. The amount of weathering or fracturing to the Denver Fm is proportional to the quantities of groundwater flow through the UFS. The saturated thickness of the upper Denver Fm can differ by as much as 30 ft depending on how the base of the UFS is defined.
- d. The flow parameters of the weathered upper Denver Fm should be better defined, especially along major contamination transport pathways.
- e. The bedrock and base elevation of the UFS in the area of Basin F northward across 9th Avenue need to be accurately defined. The quantity of flow crossing 9th Avenue from the Basin F area is dependent on the bedrock and base elevations which define the saturated thickness of the UFS. Three different data sources give three different elevations for the same area which is a reflection of the data uncertainty.
- f. The conceptual model of the groundwater flow system at RMA must be accurately defined. The revised regional model does not simulate flow through the weathered Denver Fm except in areas where the alluvium is unsaturated. The Basin F Subregional Model simulates flow through the weathered Denver Fm in all the modeled area.
- g. The design of remedial alternatives should be based on the analysis of additional data collected at proposed remedial sites along with the results of this modeling effort. Additional data would close some data gaps, reduce data uncertainty, and possibly increase design accuracy.

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# Appendix A GWFLOW Computer Code

```
PROGRAM GWFLOW
C**** UPDATE MAY,6 92 CHANGE OUTPUT TO GALLONS & June,4 to Double
Precsision***
C**** UPDATE June,5 for updating constant head 2&3 at the 4th quarter********
С
      THIS MODEL SIMULATES 2-DIMENSIONAL GROUNDWATER FLOW.
С
С
      NUMERICAL SOLUTION BY THE GALERKIN FINITE ELEMENT METHOD
С
      USING TRIANGULAR ELEMENTS AND LINEAR SHAPE FUNCTIONS.
      WRITTEN AND PROGRAMMED BY JAMES WARNER, DEPARTMENT OF CIVIL *
С
С
      ENGINEERING, COLORADO STATE UNIVERSITY, FORT COLLINS, COLO. *
C
        UNIT 11 = INPUT DATA FILE (*.INP)
С
        UNIT 12 = OUTPUT ECHO OF INPUT DATA (*.ECH)
C
        UNIT 13 = OUTPUT FOR RESIDUAL HEADS (*.DAT)
С
        UNIT 7 = OUTPUT RESULTS FILE (*.RES)
С
        UNIT 8 = OUTPUT HEAD/DRAWDOWN SURFACE FILE (*.SRF)
С
        UNIT 9 = OUTPUT HEAD FILE FOR SURFER
С
    MODIFIED BY ABDEL-RAHMAN A. A. FOR THE CRAY Y-MP SUPER-COMPUTER
   PARAMETER (NNP = 3500, NEL = 7000, IB = 75, NBS = 200)
   IMPLICIT REAL*8(A-H,O-Z)
   COMMON /BLOCKA/ NUMNP,X(NNP),Y(NNP),NUMEL,NI(NEL),NJ(NEL),
   1NK(NEL),TITLE(20),IBAND,IFLAG(5),TOL,RELAX
   COMMON /BLOCKB/ NTIM,NPMP,PINT,TIMX,TINIT,TPDAY,SUMT,
   COMMON /BLOCKC/NCODNP, NODEID(NNP), TRANS(NNP), HYDK1(NNP), THCK(NNP),
   1REC(NNP),SC(NNP),S,HEAD(NNP),HDI(NNP)
   COMMON /BLOCKD/ NCODEL,IDELEM(NEL),RECH(NEL),VPRM(NEL),AREA(NEL),
              HDLEAK(NEL)
   COMMON /BLOCKE/ AF(NNP,IB),BF(NNP,IB),DF(NNP),CM(NNP,IB),RHS(NNP)
   COMMON /BLOCKF/QINRCH,QOUTRCH,QINREC,QOUTREC,QINCHN,QOUTCHN,
   1QINLEK,QOUTLEK,QSTOR,QINGHB,QOUTGHB,QINDR,QOUTDR
   COMMON /BLOCKG/ NUMBS, NGHB(NBS, 2), GHBCOND(NBS), GHBHEAD(NBS),
   1SLENGTH(NBS),QGHB(NBS),QBSNODE(NNP),QDR(NNP),DRCOND(NNP),
   2DRELEV(NNP)
   COMMON /BLOCKH/ PRINTIT
   COMMON /BLOCKO/ NOBSW(300), OBSH(300), NUMOB
   CHARACTER*1 PRINTIT
    COMMON /BLOCKT/GS(NNP),ZBED(NNP),ZBASE(NNP),HYDK2(NNP)
   INTEGER NOBSW, NUMOB
     REAL TARRAY(2)
C
C
    INCLUDE 'MSFGRPH'
```

```
С
C
   READ INPUT DATA
С
  CALL INPUT
C
   BEFORE = SECOND(TARRAY)
C
   START COMPUTATIONS
C
  NCALL = 1
C
Ċ
   CALCULATE LENGTH OF TIME STEP
  SUMT = 0.
  TPDAY = 0.
  DO 120 INT = 1,NPMP
   TIM = TINIT/86400.
  TPDAY = TPDAY + PINT
    DO 100 \text{ NT} = 1.\text{NTIM}
     TINT = TPDAY - SUMT + .0000001
     TEPS = ABS(TINT - TIM)
     IF (TEPS.LT..0001) TIM = TINT
     TDEL = AMIN1(TIM,TINT)
     IF (S.EQ.O.) TDEL = 1.0
     SUMT = SUMT + TDEL
     TIMY = SUMT/365.25
     TIM = TIM * TIMX
     CALL ELINTF (NCALL)
     IF (IFLAG(2).EQ.1) CALL MATFLOW
     IF (IFLAG(2).EQ.0) CALL MATSOL
     CALL WATBAL
     IF (S.EQ.O.) GO TO 110
     IF (SUMT.GE.TPDAY) GO TO 110
     NCALL = NCALL + 1
 100 CONTINUE
 110 CONTINUE
    IF(PRINTIT .EQ. 'Y') CALL FLOWOUT
   ICALL = INT + 1
   IF (ICALL .LE. NPMP) CALL UPDATE
 120 CONTINUE
>>>>>>>>
С
   AFTER = SECOND(TARRAY)
   CPUTIME = AFTER-BEFORE
   WRITE(7,2000)CPUTIME
C 2000 FORMAT(' CPU TIME IS: ',e15.7)
OPEN (9,FILE = "hout.dat",STATUS = "UNKNOWN")
  WRITE(9,1000)(X(NP),Y(NP),HEAD(NP),NP=1,NUMNP)
1000 FORMAT(3F12.3)
  WRITE(*,2000)
2000 FORMAT(//,
  +15X,' ***** look for hout.dat & hdiff.dat output files ****'/)
PRINT HEAD DIFF BETWEEN OBSERVED AND CALCULATED HEADS
OPEN (13,FILE = "hdiff.dat")
  WRITE (13,1800)
1800 FORMAT(' OBS WELL OBS HEAD CALC HEAD XCORD YCORD
  *HDIFF')
  DO 1810 I = 1, NUMOB
  DO 1805 J = 1, NUMNP
   IF(NOBSW(I) .EQ. NODEID(J))THEN
```

```
DIFF = OBSH(I)-HEAD(J)
   WRITE (13,1820) NOBSW(I), OBSH(I), HEAD(J), X(J), Y(J), DIFF
1820 FORMAT (I10,5F10,3)
   ENDIF
1805 CONTINUE
1810 CONTINUE
WRITE(*,200)
 200 FORMAT(////,
           ***** Normal program termination *****'///
   +15X.'
            CHECK YOUR DIRECTORY FOR OUTPUT FILES'///)
   +15X.
   WRITE(8,250)
 250 FORMAT(
   +' END OF FILE - NO ADDITIONAL SURFACES WRITTEN TO THIS FILE FOR '
   + 'CONTOURING')
С
   STOP
   END
C
C
   SUBROUTINE INPUT
    THIS SUBROUTINE INITIALIZES THE VARIABLES AND READS AND PRINTS ALL
С
С
    INPUT DATA. THESE DATA DEFINE THE MODEL GRID, THE BOUNDARY
    CONDITIONS, TIME-STEP FACTORS, AQUIFER PROPERTIES, INITIAL
С
    POTENTIOMETRC HEAD, HYDROLOGIC STRESSES ON THE GROUNDWATER SYSTEM.
С
С
    AND OTHER HYDROLOGIC PARAMETERS.
   PARAMETER (NNP = 3500, NEL = 7000, IB = 75, NBS = 200)
   IMPLICIT REAL*8(A-H,O-Z)
   COMMON /BLOCKA/ NUMNP,X(NNP),Y(NNP),NUMEL,NI(NEL),NJ(NEL),
   1NK(NEL), TITLE(20), IBAND, IFLAG(5), TOL, RELAX
   COMMON /BLOCKB/ NTIM,NPMP,PINT,TIMX,TINIT,TPDAY,SUMT,
   COMMON /BLOCKC/NCODNP, NODEID (NNP), TRANS (NNP), HYDK1 (NNP), THCK (NNP),
   1REC(NNP), SC(NNP), S, HEAD(NNP), HDI(NNP)
   COMMON /BLOCKD/ NCODEL,IDELEM(NEL),RECH(NEL),VPRM(NEL),AREA(NEL),
             HDLEAK(NEL)
   COMMON /BLOCKF/QINRCH,QOUTRCH,QINREC,QOUTREC,QINCHN,QOUTCHN,
   1QINLEK,QOUTLEK,QSTOR,QINGHB,QOUTGHB,QINDR,QOUTDR
   COMMON /BLOCKG/ NUMBS,NGHB(NBS,2),GHBCOND(NBS),GHBHEAD(NBS),
   1SLENGTH(NBS),QGHB(NBS),QBSNODE(NNP),QDR(NNP),DRCOND(NNP),
   2DRELEV(NNP)
   COMMON /BLOCKH/ PRINTIT
   COMMON /BLOCKO/ NOBSW(300), OBSH(300), NUMOB
   CHARACTER PRINTIT*1, STATE*3, EXTEN*4, FNAMEX*20
   COMMON /BLOCKT/GS(NNP), ZBED(NNP), ZBASE(NNP), HYDK2(NNP)
   INTEGER NOBSW, NUMOB
C
C
    .....ASSIGN FILE NAMES AND APPROVE DEFAULT FILE EXTENTIONS
  15 FORMAT (A)
   WRITE (*,20)
  20 FORMAT (////////
   + 12X.'
               ***** GWFLOW vers. 1.0 ******',/
   +12X,
                   (Turn CAPS LOCK on)',///
   +12X,
             --- Assign input and output file names ---
   +12X,' (default extentions are attached if left unspecified)',///
   +12X,'Name the INPut filename(.INP) (from mesh generator GWMESH)')
   EXTEN = '.INP'
   STATE = '1ST'
    CALL FILWRK(STATE, EXTEN, FNAMEX)
    OPEN(11, FILE = FNAMEX)
    REWIND 11
```

```
С
   WRITE (*,60)
  60 FORMAT (//,
   +12X'--- Name the output Echo filename(.ECH) (echo of input) ---')
   EXTEN = '.ECH'
   STATE = 'NEW'
   CALL FILWRK(STATE, EXTEN, FNAMEX)
   OPEN (12, FILE = FNAMEX)
C
   WRITE (*,70)
  70 FORMAT (//,
   +12X'
          --- Name the output Results filename(.RES) ---')
   EXTEN = '.RES'
   STATE = 'NEW'
   CALL FILWRK(STATE, EXTEN, FNAMEX)
   OPEN (7, FILE = FNAMEX)
С
   WRITE (*,80)
  80 FORMAT(//
   + 12X' --- Name the output Surface filename(.SRF) (head,etc.) ---')
   EXTEN = '.SRF'
   STATE = 'NEW'
   CALL FILWRK(STATE, EXTEN, FNAMEX)
   OPEN (8,FILE = FNAMEX)
C
   WRITE (*,90)NNP,NEL,IB,NBS
  90 FORMAT(//' PROGRAM GWFLOW HAS THE FOLLOWING MAXIMUM DIMENSIONS:'//
   1'
          NUMBER OF NODAL POINTS = ',15,/
          NUMBER OF ELEMENTS = ',15,/
   2'
   3'
          BANDWIDTH
                                = '.15./
   4'
          NUMBER OF BOUNDARY SEGMENTS = ',15,/)
С
   AREATOT = 0.
   IBAND = 0
   QINRCH = 0.
   QOUTRCH = 0.
   QINREC = 0.
   QOUTREC = 0.
   QINCHN = 0.
   QOUTCHN = 0.
   QINLEK = 0.
   QOUTLEK = 0.
   QINGHB = 0.
   QOUTGHB = 0.
   QINDR = 0.
   QOUTDR = 0.
С
    .....PRINT HEADING
   WRITE (12,100)
 100 FORMAT (///' **********
   1***********************//
   2' *
   3
   4' * THIS MODEL SIMULATES 2-DIMENSIONAL GROUNDWATER FLOW. NUMERIC
   5AL SOLUTION *',/,
   6' * BY THE GALERKIN FINITE ELEMENT METHOD USING TRIANGULAR ELEMEN
   7TS AND
   8' * LINEAR SHAPE FUNCTIONS. WRITTEN AND PROGRAMMED BY JAMES WARN
   9ER, DEPT OF *',/,
   1' * CIVIL ENGINEERING, COLORADO STATE UNIVERSITY, FORT COLLINS, C
   20LORADO.
   3' *
   4
```

```
6************
С
    .....READ TITLE CARD
   READ (11,110) TITLE
 110 FORMAT (20A4)
   WRITE (12,120) TITLE
 120 FORMAT (//1H ,20A4//)
   WRITE (8,110) TITLE
   WRITE (12,130)
 130 FORMAT (1H0,45X,21HI N P U T D A T A/1H ,44X,23H------
С
С
    ....READ TIME TIME PARAMETERS
C
       NTIM = MAXIMUM NUMBER OF TIME STEPS
С
       NPMP = NUMBER OF PUMPING PERIODS
C
       PINT = FIRST PUMPING PERIOD IN DAYS
C
       PRINTIT = PRINT OPTION FOR THE CURRENT PUMPING PERIOD
C
       TIMX = TIME INCREMENT MULTIPLIER
C
       TINIT = INITIAL TIME STEP IN SECONDS
   READ (11,110) TITLE
   READ (11,160) NTIM, NPMP, PINT, PRINTIT, TIMX, TINIT
 160 FORMAT (215,F10.0,4X,A1,2F10.0)
   WRITE (12,170) NTIM, NPMP, PINT, PRINTIT, TIMX, TINIT
 170 FORMAT (///.23X,16HTIME PARAMETERS//
   113X,48HNTIM (MAXIMUM NUMBER OF TIME STEPS)
                                                         = .2X.14/
   213X,48HNPMP (NUMBER OF PUMPING PERIODS)
                                                       = .2X.14/
   313X.48HPINT (FIRST PUMPING PERIOD IN DAYS)
                                                      =,2X,F7.2/
   313X,48HPRINTIT (PRINT OPTION FOR FIRST PERIOD)
                                                       = .5X.A1 /
   413X,48HTIMX (TIME INCREMENT MULTIPLIER)
                                                     =.2X,F7.2/
   513X,48HTINIT (INITIAL TIME STEP IN SECONDS)
                                                     =,2X,F5.0
C
    .....READ SIMULATION OPTIONS
C
С
       IFLAG1 = 0 (CONFINED AQUIFER
С
       IFLAG1 = 1 (UNCONFINED AQUIFER)
C*
       IFLAG1 = 2 (LEAKY AQUIFER)
       IFLAG1 = 3 (MODIFIED ONE LAYER MODEL)
C*
С
       IFLAG2 = 0 (SOLUTION BY GAUSS ELIMINATION)
       IFLAG2 = 1 (SOLUTION BY POINT ITER. SUCCESSIVE OVER RELAXATIO
С
С
       IFLAG3 = 0 (GWFLOW DATA SET -- MUST BE 0 FOR THIS PROGRAM)
C
       TOL = ERROR TOLERANCE IN PISOR
С
       RELAX = RELAXATION FACTOR IN PISOR
    READ (11,110) TITLE
    READ (11,180) IFLAG(1)
    READ (11,110) TITLE
    READ (11,180) IFLAG(2),TOL,RELAX
    READ (11,110) TITLE
    READ (11,180) IFLAG(3)
 180 FORMAT (I1,2F10.0)
    WRITE (12,190)
  190 FORMAT (///,23X,19HSIMULATION OPTIONS/)
    IF (IFLAG(1).EQ.0) WRITE (12,200)
 200 FORMAT (18X,16HCONFINED AQUIFER)
    IF (IFLAG(1),EQ.1) WRITE (12,210)
 210 FORMAT (18X,18HUNCONFINED AQUIFER)
    IF (IFLAG(2).EQ.0) WRITE (12,220)
 220 FORMAT (18X,29HSOLUTION BY GAUSS ELIMINATION)
    IF (IFLAG(2).EQ.1) WRITE (12,230) TOL, RELAX
 230 FORMAT (18X.38HSOLUTION BY POINT ITERATIVE SUCCESSIVE/
   123X,25HOVER RELAXATION - (PISOR)/
   223X,38HTOL (ERROR TOLERANCE)
                                            =,2X,F11.6/
   323X,38HRELAX (RELAXATION FACTOR)
                                              =,2X,F7.2)
С
    .....READ ELEMENT DESCRIPTORS
C
       NUMNP = NUMBER OF NODAL POINTS
```

```
С
       NUMEL = NUMBER OF ELEMENTS
C
   READ (11,110) TITLE
   READ (11,140) NUMNP, NUMEL
 140 FORMAT (215)
   IF (NUMNP .GT. NNP .OR. NUMEL .GT. NEL) THEN
     WRITE (*,145)
 145 FORMAT(///,20X,'***** E R R O R -- # INP1 ******//)
     STOP
     RETURN
   END IF
   WRITE (12,150) NUMNP, NUMEL
 150 FORMAT (///1H ,22X, 'ELEMENT DISCRIPTORS'//
   113X,48HNUMNP (NUMBER OF NODAL POINTS)
                                                        = .2X.14/
   213X,48HNUMEL (NUMBER OF ELEMENTS)
                                                      = ,2X,14)
С
    .....READ NODAL COORDINATES
   READ (11,110) TITLE
   READ (11,260) FCTR
 260 FORMAT (F10.0)
   READ (11,270) (NP,X(NP),Y(NP),I = 1,NUMNP)
 270 FORMAT (3(15,2F10.0))
C
   DO 280 NP = 1,NUMNP
     X(NP) = X(NP) * FCTR
     Y(NP) = Y(NP) * FCTR
 280 CONTINUE
С
   WRITE (12,290)
 290 FORMAT (1H1,45X,21HI N P U T D A T A/1H ,44X,23H------
   1-----////1H0,5X,16HNODE COORDINATES/1H,4X,18H-----
   2--/1H0,7X,2(4HNODE,5X,5HX LOC,7X,5HY LOC,13X)/)
   WRITE (12,300) (NP,X(NP),Y(NP),NP = 1,NUMNP)
 300 FORMAT (/( 8X,2(I5,F12.2,F12.2,12X)))
С
С
    .....READ ELEMENT VERTICES
   READ (11,110) TITLE
   READ (11,310) (NE,NI(NE),NJ(NE),NK(NE),I = 1,NUMEL)
 310 FORMAT (4(415))
С
    .....CALCULATE BANDWIDTH
   DO 320 I = 1, NUMEL
     IJ = IABS(NI(I) - NJ(I)) + 1
     IK = IABS(NI(I) - NK(I)) + 1
     JK = IABS(NJ(I) - NK(I)) + 1
 320 IBAND = MAXO(IBAND,IJ,IK,JK)
   WRITE (12,330)
 330 FORMAT (1H1,45X,21HI N P U T D A T A/1H ,44X,23H------
  1------1///1H0,5X,16HELEMENT VERTICES/1H ,4X,18H------
   2--/1H0, 7X,2(7HELEMENT,3X,6HNODE I,2X,6HNODE J,2X,6HNODE K,7X)/)
   WRITE (12,340) (NE,NI(NE),NJ(NE),NK(NE),NE = 1,NUMEL)
 340 FORMAT (/( 7X,2(I5,5X,I5,3X,I5,3X,I5,8X)))
   WRITE (12,350) IBAND
 350 FORMAT (///,1H ,10X,11HBANDWIDTH =,15)
С
   IF (IBAND .GT. IB) THEN
     WRITE (*,352)
 352 FORMAT(///,20X,'***** E R R O R -- # INP2 ******//)
     STOP
     RETURN
   END IF
    .....CALCULATE ELEMENT AREAS
   DO 390 I = 1, NUMEL
     AREA(I) = ABS((X(NJ(I)) * Y(NK(I)) - X(NK(I)) * Y(NJ(I))
```

```
+ X(NK(I)) * Y(NI(I)) - X(NI(I)) * Y(NK(I))
             + X(NI(I)) * Y(NJ(I)) - X(NJ(I)) * Y(NI(I))))*.5
  2
 390 AREATOT = AREATOT + AREA(I)
   .....READ IDELEM ARRAY
С
С
       RECH = DISTRIBUTED RECHARGE OR DISCHARGE IN FT**3/DAY/FT**2
        "+" IS DISCHARGE(PUMPAGE), "-" IS RECHARGE(INJECTION)
С
С
       RECH = ECTR1
       VPRM = VERT.HYDRAULIC CONDUCTIVITY/THICKNESS OF CONFINING LAYE
C
C
       VPRM = FCTR2
       HDLEAK = CONSTANT HEAD LEVEL OVERLYING THE CONFINING LAYER
С
С
       HDLEAK = FCTR3
С
       NCODEL = NUMBER OF ELEMENT ID CODES TO BE DEFINED
C
       SPECIFY OTHER CODES TO FIT YOUR NEEDS
       *****NOTE: IF NCODEL < 0, THE FILE IS INCOMPLETE
   READ (11,110) TITLE
   READ (11,400) NCODEL
 400 FORMAT (12)
   IF (NCODEL .LT. 0) THEN
     WRITE (*,405)
     WRITE (12,405)
     WRITE (7,405)
 405 FORMAT(///,20X,'***** E R R O R -- # INP3 *****'///)
     STOP
     RETURN
   END IF
   DO 410 NE = 1, NUMEL
     RECH(NE) = 0.
     VPRM(NE) = 0.
     IDELEM(NE) = 0
     HDLEAK(NE) = 0.
 410 CONTINUE
   IF (NCODEL.EQ.0) GO TO 510
   READ (11,420) (NE,IDELEM(NE),I = 1,NUMEL)
 420 FORMAT (8(215))
   WRITE (12,430)
 430 FORMAT (1H1,45X,21HI N P U T D A T A/1H ,44X,23H------
   1-----////1H0,5X,22HELEMENT IDENTIFICATION/1H ,4X,23H------
   2-----/1H0,21X,9HNUMBER OF,/1H ,9X,7HELEM ID,5X,10HOCCURENC
   3ES,10X,5HRECH,10X,4HVPRM,10X,'HDLEAK')
   READ (11,110) TITLE
   DO 470 NID = 1,NCODEL
     KOUNT = 0
     READ (11,440) ICODE,FCTR1,FCTR2,FCTR3,FCTR4,FCTR5
 440 FORMAT (15,5F10.0)
     DO 450 | = 1, NUMEL
       IF (IDELEM(I).NE.ICODE) GO TO 450
       KOUNT = KOUNT + 1
       RECH(I) = FCTR1
       VPRM(I) = FCTR2
       HDLEAK(I) = FCTR3
 450 CONTINUE
     WRITE (12,460) ICODE, KOUNT, FCTR1, FCTR2, FCTR3
 460 FORMAT ((10X,I5,8X,I5,8X,3(F10.7,5X)))
 470 CONTINUE
    .....PRINT ELEMENT DATA FOR AREA AND ELEMENT ID
    WRITE (12,480)
 480 FORMAT (1H1,45X,21HI N P U T D A T A/1H ,44X,23H------
   1-----////1H0,5X,12HELEMENT DATA/1H ,4X,14H-----/1H0,2
   2(7X,7HELEMENT,7X,4HAREA,5X,7HELEM ID,4X))
    WRITE (12,490) (NE,AREA(NE),IDELEM(NE),NE = 1,NUMEL)
  490 FORMAT (2( 8X,15,F14.1,4X,15,5X))
    WRITE (12,500) AREATOT
  500 FORMAT (///,1H ,10X,18HMODEL AREA(FT**2) = ,F20.2)
```

```
510 CONTINUE
С
С
    READ GROUND SURFACE ELEVATION (GS ARRAY) IN (FT)
С
   READ (11,110) TITLE
   READ (11,520) INP,SFCT
 520 FORMAT (I2,F10.0)
   IF (INP.EQ.1) READ (11,525) (NP,GS(NP),I = 1,NUMNP)
 525 FORMAT (5(15,F10.0))
   DO 530 I = 1,NUMNP
     IF (INP.EQ.1) THEN
       GS(I) = GS(I) * SFCT
     ELSEIF(INP .EQ. 0)THEN
       GS(I) = SFCT
     ENDIF
 530 CONTINUE
С
   WRITE (12,531)
 531 FORMAT (1H1,////,24X,' I N P U T D A T A ')
   WRITE (12,532)
 532 FORMAT (24X,'-----',//)
   WRITE (12,533)
 533 FORMAT (4X,' GROUND SURFACE ELEVATION ')
   WRITE (12,534)
 534 FORMAT (4X.'--
   WRITE (12,535)
 535 FORMAT (4X,3(' NODE GS ELEV
                                        '))
   WRITE (12,536)
 536 FORMAT (4X,3('-----
   WRITE (12,537)(I,GS(I),I=1,NUMNP)
 537 FORMAT (3(I8,F14.1,4X))
C
С
    READ BEDROCK ELEVATION (ZBED ARRAY) IN (FT)
С
   READ (11,110) TITLE
   READ (11,920) INP,SFCT
 920 FORMAT (I2,F10.0)
   IF (INP.EQ.1) READ (11,925) (NP,ZBED(NP),I = 1,NUMNP)
 925 FORMAT (5(15,F10.0))
   DO 930 I = 1,NUMNP
     IF (INP.EQ.1) THEN
       ZBED(I) = ZBED(I) * SFCT
     ELSEIF(INP .EQ. 0)THEN
       ZBED(I) = SFCT
     ENDIF
 930 CONTINUE
С
   WRITE (12,931)
 931 FORMAT (1H1,////,24X,' I N P U T D A T A ')
   WRITE (12,932)
 932 FORMAT (24X,'-----',//)
   WRITE (12,933)
 933 FORMAT (4X,' BEDROCK ELEVATION ')
   WRITE (12,934)
 934 FORMAT (4X,'-----')
   WRITE (12,938)
                         BEDROCK
 938 FORMAT (4X,3('
                                       '))
   WRITE (12,935)
 935 FORMAT (4X,3(' NODE ELEVATION
                                          '))
   WRITE (12,936)
 936 FORMAT (4X,3('-----
   WRITE (12,937)(I,ZBED(I),I = 1,NUMNP)
 937 FORMAT (3(18,F14.1,4X))
С
С
    READ BASE OF AQUIFER ELEVATION (ZBASE ARRAY) IN (FT)
```

```
C
   READ (11,110) TITLE
   READ (11,940) INP,SFCT
 940 FORMAT (I2,F10.0)
   IF (INP.EQ.1) READ (11,945) (NP,ZBASE(NP),I = 1,NUMNP)
 945 FORMAT (5(15,F10.0))
   DO 950 I = 1, NUMNP
     IF (INP.EQ.1) THEN
       ZBASE(I) = ZBASE(I) * SFCT
     ELSEIF(INP .EQ. 0)THEN
       ZBASE(I) = SFCT
     ENDIF
 950 CONTINUE
C
   WRITE (12,951)
 951 FORMAT (1H1,////,24X,' INPUT DATA')
   WRITE (12,952)
 952 FORMAT (24X,'-----',//)
   WRITE (12,953)
 953 FORMAT (4X,' BASE OF AQUIFER ')
   WRITE (12,954)
 954 FORMAT (4X,'---
   WRITE (12,958)
 958 FORMAT (4X,3('
                       AQUIFER BASE
                                         '))
   WRITE (12,955)
 955 FORMAT (4X,3(' NODE ELEVATION
                                          '))
   WRITE (12,956)
 956 FORMAT (4X,3('-----
   WRITE (12,957)(I,ZBASE(I),I=1,NUMNP)
 957 FORMAT (3(I8,F14.1,4X))
    READ HYDRAULIC CONDUCTIVITY FOR AQUIFER 1 ARRAY IN (FT/DAY)
С
C
    READ (11,110) TITLE
    READ (11,560) INP,SFCT
 560 FORMAT (12,F10.0)
    IF (INP.EQ.1) READ (11,570) (NP,HYDK1(NP),I = 1,NUMNP)
 570 FORMAT (5(15,F10.0))
    DO 590 I = 1, NUMNP
     IF (INP.NE.1) GO TO 580
     HYDK1(I) = HYDK1(I) * SFCT
     GO TO 590
 580 HYDK1(I) = SFCT
 590 CONTINUE
    WRITE (12,601)
 601 FORMAT (1H1,////,24X,' I N P U T D A T A ')
    WRITE (12,602)
  602 FORMAT (24X,'-----',//)
    WRITE (12,603)
 603 FORMAT (4X,' HYDRAULIC CONDUCTIVITY AQUIFER 1 - FT/DAY')
    WRITE (12,604)
  604 FORMAT (4X,'-
    WRITE (12,605)
  605 FORMAT (4X,3(' NODE HYDK1
                                        '))
    WRITE (12,606)
  606 FORMAT (4X,3('-----
    WRITE (12,607)(I,HYDK1(I),I=1,NUMNP)
  607 FORMAT (3(18,F12.1,4X))
С
    READ HYDRAULIC CONDUCTIVITY FOR AQUIFER 2 ARRAY IN (FT/DAY)
С
    READ (11,110) TITLE
    READ (11,1060) INP,SFCT
 1060 FORMAT (I2,F10.0)
    IF (INP.EQ.1) READ (11,1070) (NP,HYDK2(NP),I = 1,NUMNP)
```

```
1070 FORMAT (5(15,F10.0))
   DO 1090 I = 1, NUMNP
     IF (INP.NE.1) GO TO 1080
     HYDK2(I) = HYDK2(I) * SFCT
     GO TO 1090
1080 HYDK2(I) = SFCT
1090 CONTINUE
   WRITE (12,1091)
1091 FORMAT (1H1,////,24X,' I N P U T D A T A ')
   WRITE (12,1092)
1092 FORMAT (24X,'-----',//)
   WRITE (12,1093)
1093 FORMAT (4X,' HYDRAULIC CONDUCTIVITY AQUIFER 2 - FT/DAY')
   WRITE (12,1094)
1094 FORMAT (4X,'--
   WRITE (12,1095)
1095 FORMAT (4X,3(' NODE HYDK2
                                        '))
   WRITE (12,1096)
1096 FORMAT (4X,3('-----
   WRITE (12,1097)(I,HYDK2(I),I=1,NUMNP)
1097 FORMAT (3(18,F12.1,4X))
С
С
    .....READ STORAGE COEFFICIENT ARRAY IN (DIMENSIONLESS)
   READ (11,110) TITLE
   READ (11,610) INP,SFCT
 610 FORMAT (I2,F10.0)
   S = SFCT
   IF (INP.EQ.1) READ (11,620) (NP,SC(NP),I = 1,NUMNP)
 620 FORMAT (5(15,F10.0))
   DO 640 I = 1, NUMNP
     IF (INP.NE.1) GO TO 630
     SC(I) = SC(I) * SFCT
     GO TO 640
 630 SC(I) = SFCT
 640 CONTINUE
   WRITE (12,641)
 641 FORMAT (1H1,////,24X,'INPUT DATA')
   WRITE (12,642)
 642 FORMAT (24X,'-----',//)
   WRITE (12,643)
 643 FORMAT (4X,' STORAGE COEFFICIENT ')
   WRITE (12,644)
 644 FORMAT (4X,'---
   WRITE (12,648)
 648 FORMAT (4X,3('
                         STOR
                                   '))
   WRITE (12,645)
 645 FORMAT (4X,3(' NODE COEFF
                                      '))
   WRITE (12,646)
 646 FORMAT (4X,3('-----
   WRITE (12,647)(I,SC(I),I=1,NUMNP)
 647 FORMAT (3(18,F10.6,5X))
С
   .....READ INITIAL HEAD ARRAY IN (FT)
C
   READ (11,110) TITLE
   READ (11,650) INP,SFCT
 650 FORMAT (I2,F10.0)
   IF (INP.EQ.1) READ (11,660) (NP,HEAD(NP),I = 1,NUMNP)
 660 FORMAT (5(I5,F10.0))
   DO 680 I = 1,NUMNP
     IF (INP.NE.1) GO TO 670
     HEAD(I) = HEAD(I) * SFCT
     GO TO 680
 670 HEAD(I) = SFCT
```

```
680 CONTINUE
С
    .....SET INITIAL HEAD VALUE
   DO 690 I = 1, NUMNP
 690 \text{ HDI(I)} = \text{HEAD(I)}
   WRITE (12,691)
 691 FORMAT (1H1,////,24X,' I N P U T D A T A ')
   WRITE (12,692)
 692 FORMAT (24X,'-----',//)
   WRITE (12,693)
 693 FORMAT (4X,' INITIAL HEAD - FEET ')
   WRITE (12,694)
 694 FORMAT (4X,'-
   WRITE (12,695)
 695 FORMAT (4X,3(' NODE
                                        '))
                             HEAD
   WRITE (12,696)
 696 FORMAT (4X,3('-----
   WRITE (12,697)(I,HEAD(I),I = 1,NUMNP)
 697 FORMAT (3(18,F13.1,5X))
С
С
    CALCULATE TRANSMISSIVITY ARRAY IN (FT*2/DAY)
C
   IFLAG(1) = 3
   CALL TRANADJ
C
   WRITE (12,1201)
1201 FORMAT (1H1,/////,24X,' | N P U T D A T A ')
   WRITE (12,1202)
 1202 FORMAT (24X,'-----',//)
   WRITE (12,1203)
 1203 FORMAT (4X,' TRANSMISSIVITY - FT**2/DAY')
   WRITE (12,1204)
 1204 FORMAT (4X,'--
   WRITE (12,1205)
 1205 FORMAT (4X,3(' NODE
                                        '))
                           TRANS
    WRITE (12,1206)
 1206 FORMAT (4X,3('-----
    WRITE (12,1207)(I,TRANS(I),I=1,NUMNP)
 1207 FORMAT (3(18,F12.1,4X))
С
    .....READ NODEID ARRAY
C
       NODE ID CODES FOR 1 - 10 ARE RESERVED FOR CONSTANT HEAD NODES
С
С
       REC = POINT RECHARGE OR DISCHARGE IN GPM
         "+" IS DISCHARGE(PUMPAGE), "-" IS RECHARGE(INJECTION)
С
C
       REC = FCTR1
       DRCOND = RIVER/DRAIN CONDUCTANCE (- IS RIVER)
C
С
       DRELEV = RIVER/DRAIN HEAD
С
       NCODNP = NUMBER OF NODE ID CODES TO BE DEFINED
       SPECIFY OTHER CODES TO FIT YOUR NEEDS
С
    READ (11,110) TITLE
    READ (11,700) NCODNP
 700 FORMAT (I2)
    DO 710 NP = 1, NUMNP
     REC(NP) = 0.
     NODEID(NP) = 0
     QBSNODE(NP) = 0.
     DRELEV(NP) = 0.
     DRCOND(NP) = 0.
  710 CONTINUE
    DO 715 NS = 1,NBS
     QGHB(NS) = 0.
 715 CONTINUE
    IF (NCODNP.LE.O) GO TO 780
```

```
READ (11,720) (NP,NODEID(NP),I = 1,NUMNP)
 720 FORMAT (8(215))
   WRITE (12,730)
 730 FORMAT (1H1,45X,21HI N P U T D A T A/1H ,44X,23H------
   1------1///1H0,5X,19HNODE IDENTIFICATION/1H ,4X,21H------
   2-----/1H0,21X,9HNUMBER OF,/1H ,9X,7HNODE ID,5X,10HOCCURENCES,11
   3X,3HREC,9X,6HDRCOND,6X,6HDRELEV)
   READ (11.110) TITLE
   DO 770 NID = 1,NCODNP
     KOUNT = 0
     READ (11,740) ICODE,FCTR1,FCTR2,FCTR3,FCTR4,FCTR5
 740 FORMAT (15,5F10.0)
     DO 750 I = 1, NUMNP
      IF (NODEID(I).NE.ICODE) GO TO 750
       KOUNT = KOUNT + 1
       REC(I) = FCTR1
      DRCOND(I) = FCTR2
      DRELEV(I) = FCTR3
 750 CONTINUE
     WRITE (12,760) ICODE, KOUNT, FCTR1, FCTR2, FCTR3
 760 FORMAT ((10X,I5,8X,I5,8X,1(F10,2,5X),2(F10,2,2X)))
 770 CONTINUE
   WRITE (12,771)
771 FORMAT (1H1,////,24X,'INPUT DATA')
   WRITE (12,772)
 772 FORMAT (24X.'-----'.//)
   WRITE (12,773)
 773 FORMAT (4X,' NODEID ARRAY ')
   WRITE (12,774)
 774 FORMAT (4X,'----')
   WRITE (12,775)
 775 FORMAT (4X,3(' NODE NODEID
   WRITE (12,776)
776 FORMAT (4X,3('-----
   WRITE (12,777)(I,NODEID(I),I=1,NUMNP)
777 FORMAT (3(18,110,5X))
С
С
   .....CONVERT REC FROM GPM TO FT**3/DAY
780 DO 790 NP = 1,NUMNP
     REC(NP) = REC(NP)/7.48052 * 60 * 24
790 CONTINUE
С
    .... INPUT THE GHB DATA
С
   READ(11,110) TITLE
   READ(11,800) NUMBS
800 FORMAT (I5)
   IF (NUMBS .LE. 0) GO TO 890
   IF (NUMBS .GT. NBS) THEN
    WRITE (*,805)
805 FORMAT(///,20X,'***** E R R O R -- # INP4 ******//)
     STOP
     RETURN
   END IF
   READ(11,110) TITLE
   DO 810 NS = 1, NUMBS
     GHBCOND(NS) = 0.
     GHBHEAD(NS) = 0.
    SLENGTH(NS) = 0.
     QGHB(NS) = 0.
810 CONTINUE
   DO 820 NS = 1, NUMBS
    READ(11,830) ISEGMENT, NGHB(NS, 1), NGHB(NS, 2),
             GHBCOND(NS), GHBHEAD(NS)
```

```
830 FORMAT(3|5,F10,7,F10,1)
    IF (NGHB(NS,2) .LT. NGHB(NS,1)) THEN
      N1 = NGHB(NS, 1)
      N2 = NGHB(NS, 2)
      NGHB(NS,1) = N2
      NGHB(NS,2) = N1
    END IF
    SLENGTH(NS) = SQRT( ((X(NGHB(NS,1))-X(NGHB(NS,2)))**2) +
              ( (Y(NGHB(NS,1))-Y(NGHB(NS,2)))**2 ) )
 820 CONTINUE
С
С
   WRITE(12,771)
   WRITE(12,772)
   WRITE(12,851)
 851 FORMAT(5X, 'GENERAL HEAD BOUNDARY SEGMENTS')
   WRITE(12,850)
                                      COND
                                              HEAD
                                                     LENGTH')
 850 FORMAT(/5X' SEGMENT NODE1 NODE2
   WRITE(12,852)
 852 FORMAT(5X,' --
   DO 860 NS = 1, NUMBS
    WRITE(12,865)NS, (NGHB(NS,J),J=1,2), GHBCOND(NS), GHBHEAD(NS),
          SLENGTH(NS)
 865 FORMAT (5X,I5,3X,2(I5,1X),2X,F10.7,F10.1,F10.1)
 860 CONTINUE
   GO TO 900
C
 890 WRITE(12,771)
   WRITE(12,772)
   WRITE(12,892)
 892 FORMAT (//,15X,'NO HEAD-DEPENDENT FLUX (GHB) SEGMENTS'///)
 900 CONTINUE
++++++++++++++++++
     READ OBSERVED HEAD DATA
+++++++++++++++++++
   READ (11,110)TITLE
   READ (11,1840) NUMOB
 1840 FORMAT (I5)
   DO 1860 I = 1, NUMOB
   READ (11,1850) NOBSW(I),OBSH(I)
 1850 FORMAT (I10,F10.0)
1860 CONTINUE
 999 RETURN
   END
   SUBROUTINE FILWRK(STATE, EXTEN, FNAMEX)
     THIS SUBROUTINE PROMPTS THE USER FOR A FILE NAME FOR INPUT OR
    OUTPUT AND APPENDS A DEFAULT EXTENTION IF THE USER CHOOSES
С
     STATE = 1ST/OLD/NEW = CHARACTER VAR. WHICH INDICATES IF THIS
С
         THE FIRST TIME ANY FILE CALLED, OR IF IT IS AN OLD
C
C
         (EXISTING) FILE OR NEW (TO BE CREATED) FILE.
С
C
   CHARACTER STATE*3, EXTEN*4, FNAMEX*20, ANSWER*1
   LOGICAL EXISTS
C
   ANSWER = 'Y'
  10 FORMAT (A)
C
```

```
.....PROMPT FOR THE FILE NAME, WITH OR WITHOUT THE EXTENTION
         IF THE FIRST PROMPT FOR A NAME, PROMPT FOR BASE FILE NAME
    IF(STATE .NE. '1ST') GO TO 199
  99 WRITE(*,100)
 100 FORMAT(20X,
                              (D:FNAME?): = > ')
    READ(*,10) FNAMEX
   I = INDEX(FNAMEX,' ')
   IF(I.EQ.1) GOTO 99
C
    .....FIND THE LENGTH OF THE BASE FILE NAME (FNAME)
C
C
        IF JJ IS LESS THAN II, AN EXTENTION IS ALREADY IN THE NAME
 199 I = INDEX(FNAMEX,' ')
    J = INDEX(FNAMEX,'.')
   IF(J.EQ.0) J=1
   || = || -1|
    JJ = J-1
    LEN = MIN(II,JJ)
    .....IF NO EXTEN GIVEN, SUGGEST THE DEFAULT INITIALLY
C
         NOTE: STATE = 1ST NOW CHANGED TO = OLD
    IF (STATE .EQ. '1ST') THEN
      IF (JJ.GE.II) FNAMEX = FNAMEX(1:LEN)//EXTEN
      STATE = 'OLD'
    ELSE IF (STATE.NE.'1ST' .AND. ANSWER.EQ.'Y') THEN
      FNAMEX = FNAMEX(1:LEN)//EXTEN
С
    .....ASK FOR APPROVAL FOR THE FILE NAME "FNAMEX"
 299 CONTINUE
   IF(ANSWER .EQ. 'Y') WRITE(*,300) FNAMEX
 300 FORMAT(20X, 'For this file, the default name is: ',A,/
                Is this ACCEPTable (Y/N?) := > '
         20X,'
   IF(ANSWER .EQ. 'N') WRITE(*,310) FNAMEX
 310 FORMAT(20X,'For this file, the NEW name is: ',A,/
                 Is this ACCEPTable (Y/N?) := > '
         20X,1
 320 READ(*,10) ANSWER
   IF (ANSWER .NE. 'Y' .AND. ANSWER .NE. 'N') THEN
     WRITE (*,330)
 330 FORMAT(20X,1
                     Is this ACCEPTable (Y/N?) := > ')
     GO TO 320
   END IF
   IF (ANSWER .EQ. 'N') GO TO 99
 399 WRITE(*,400) FNAMEX
 400 FORMAT(20X,' Using file named = ',A)
    ..... DETERMINE THE STATUS OF THE FILE "FNAMEX" AND COMPARE THIS
C
         TO THE EXPECTED STATUS "STATE"
   INQUIRE(FILE = FNAMEX, EXIST = EXISTS)
   IF (.NOT.EXISTS .AND. STATE.EQ.'OLD') THEN
     WRITE(*,500) FNAMEX
 500 FORMAT(20X,'***** ERROR -- cannot find file:',A,/
           40X,
                 ' -- TRY AGAIN'//)
     GO TO 99
   ELSE IF (EXISTS .AND. STATE.EQ.'NEW') THEN
 510 WRITE(*,520) FNAMEX
 520 FORMAT(20X,'***** WARNING -- file:',A,/
          20X,1
                  already exists -- OK TO OVERWRITE (Y/N?): = >')
     READ(*,10)ANSWER
     IF (ANSWER.NE.'Y' .AND. ANSWER.NE.'N') GO TO 510
     IF (ANSWER.EQ.'N') GO TO 99
   END IF
C
 999 RETURN
   END
```

```
SUBROUTINE UPDATE
C
С
    THIS SUBROUTINE IS USED TO SELECTIVELY UPDATE SOME OR ANY OF THE
C
    MODEL INPUT DATA AT THE END OF EACH PUMPING PERIOD.
C
    PARAMETER (NNP = 3500, NEL = 7000, IB = 75, NBS = 200)
C**** IMPLICIT REAL*8(A-H,O-Z)
   COMMON /BLOCKA/ NUMNP,X(NNP),Y(NNP),NUMEL,NI(NEL),NJ(NEL),
   1NK(NEL), TITLE(20), IBAND, IFLAG(5), TOL, RELAX
    COMMON /BLOCKB/ NTIM,NPMP,PINT,TIMX,TINIT,TPDAY,SUMT,
   1TDEL, TIMY
   COMMON /BLOCKC/NCODNP,NODEID(NNP),TRANS(NNP),HYDK1(NNP),THCK(NNP),
   1REC(NNP), SC(NNP), S, HEAD(NNP), HDI(NNP)
   COMMON /BLOCKD/ NCODEL,IDELEM(NEL),RECH(NEL),VPRM(NEL),AREA(NEL),
              HDLEAK(NEL)
   COMMON /BLOCKF/QINRCH,QOUTRCH,QINREC,QOUTREC,QINCHN,QOUTCHN,
   1QINLEK,QOUTLEK,QSTOR,QINGHB,QOUTGHB,QINDR,QOUTDR
   COMMON /BLOCKG/ NUMBS, NGHB(NBS, 2), GHBCOND(NBS), GHBHEAD(NBS),
   1SLENGTH(NBS),QGHB(NBS),QBSNODE(NNP),QDR(NNP),DRCOND(NNP).
   2DRELEV(NNP)
   COMMON /BLOCKH/ PRINTIT
   CHARACTER PRINTIT*1, CHANGEM*4
C
C
С
С
     UPDATE CONSTANT HEAD FOR NODEID 2&3
C
C
     IF(SUMT.GE.270.AND.SUMT.LE.360)THEN
C
     DO 2000 I = 1.NUMNP
С
       IF(NODEID(I).NE.10)GOTO 2000
С
         HEAD(I) = HEAD(I) + 1.5
С
         HDI(I) = HDI(I) + 1.5
         WRITE(6,*)I,HEAD(I)
C2000 CONTINUE
C
    ENDIF
    .....UPDATE PUMPING PERIOD DATA
 100 WRITE (12,110)
 110 FORMAT (1H1,45X,23HU P D A T E D A T A/1H .44X,25H-----
   1----///)
   READ (11,120) TITLE
   WRITE (12,130) TITLE
 120 FORMAT (20A4)
 130 FORMAT (//1H ,20A4/,'-----',/)
    .....UPDATE TIME PARAMETERS
   READ (11,120) TITLE
   READ (11,140) PINT, PRINTIT, CHANGEM
 140 FORMAT (F10.0,4X,A1,1X,A4)
   WRITE (12,150) PINT, PRINTIT, CHANGEM
 150 FORMAT (
         /6X, 'PINT (PUMPING PERIOD IN DAYS)
   +
                                                  =1.2X.F7.2.
   +
         /6X,'PRINTIT (PRINT SOLUTION FOR THIS PERIOD) = ',2X,A1,
         /6X,'CHANGEM (UPDATE OPTION FOR THIS PERIOD) = ',2X,A4)
C
   IF (CHANGEM .EQ. 'NONE') GO TO 1000
   IF (CHANGEM .EQ. 'LMNT') GO TO 300
    .....UPDATE NODE ID CODES
   IF (NCODNP .LE. 0) GO TO 300
   DO 160 \text{ NP} = 1, \text{NUMNP}
 160 \text{ REC(NP)} = 0.
   WRITE (12,180)
 180 FORMAT (//1H0,5X,'NODE IDENTIFICATION'/5X,'-----',
   1'-----'/1H0,21X,'NUMBER OF'/10X,'NODE ID'5X'OCCURENCES',11X
```

```
2, 'REC', 9X, 6HDRCOND, 6X, 6HDRELEV)
   READ (11,120) TITLE
   DO 220 NID = 1,NCODNP
    KOUNT = 0
    READ (11,190) ICODE,FCTR1,FCTR2,FCTR3
190 FORMAT (I5,3F10.0)
    DO 200 I = 1, NUMNP
      IF (NODEID(I).NE.ICODE) GO TO 200
      KOUNT = KOUNT + 1
      REC(I) = FCTR1
      DRCOND(I) = FCTR2
      DRELEV(I) = FCTR3
200 CONTINUE
    WRITE (12,210) ICODE, KOUNT, FCTR1, FCTR2, FCTR3
210 FORMAT ((10X,I5,8X,I5,8X,1(F10.2,5X),2(F10.2,2X)))
220 CONTINUE
С
   .....CONVERT REC FROM GPM TO FT**3/DAY
   DO 230 NP = 1, NUMNP
     REC(NP) = REC(NP)/7.48052 * 60 * 24
 230 CONTINUE
C
   IF (CHANGEM .EQ. 'NODE') GO TO 1000
C
   .....UPDATE ELEMENT ID CODES
С
 300 IF (NCODEL.EQ.0) GO TO 1000
   DO 410 NE = 1, NUMEL
     RECH(NE) = 0.
     VPRM(NE) = 0.
     HDLEAK(NE) = 0.
 410 CONTINUE
   WRITE (12,430)
 430 FORMAT (1H1,45X,21H
                                     /1H ,44X,23H
         ////1H0,5X,22HELEMENT IDENTIFICATION/1H ,4X,23H------
         ----/1H0,21X,9HNUMBER OF,/1H ,9X,7HELEM ID,5X,10HOCCURENC
   3ES,10X,5HRECH ,10X,4HVPRM,10X,'HDLEAK')
   READ (11,120) TITLE
   DO 470 NID = 1,NCODEL
     KOUNT = 0
     READ (11,440) ICODE,FCTR1,FCTR2,FCTR3,FCTR4,FCTR5
 440 FORMAT (15,5F10.0)
     DO 450 I = 1, NUMEL
       IF (IDELEM(I).NE.ICODE) GO TO 450
       KOUNT = KOUNT + 1
       RECH(I) = FCTR1
       VPRM(I) = FCTR2
       HDLEAK(I) = FCTR3
 450 CONTINUE
     WRITE (12,460) ICODE, KOUNT, FCTR1, FCTR2, FCTR3
 460 FORMAT ((10X,I5,8X,I5,8X,3(F10.7,5X)))
 470 CONTINUE
 1000 CONTINUE
 999 RETURN
   END
    SUBROUTINE ELINTF(NCALL)
    THIS SUBROUTINE PERFORMS THE INTEGRATIONS REQUIRED FOR THE FLOW
С
    EQUATION. THESE INTEGRATIONS ARE CARRIED OUT IN A PIECEWISE
    MANNER ON AN ELEMENT BASIS. GLOBAL MATRICES ARE THEN FORMED BY
    SUMMING FOR A GIVEN NODE THE CONTRIBUTION TO THAT NODE FROM EACH
С
    ELEMENT. THESE GLOBAL MATRICES FOR THE FLOW EQUATION ARE BANDED
С
С
    AND SYMMETRIC.
```

```
PARAMETER (NNP = 3500, NEL = 7000, IB = 75.NBS = 200)
C**** IMPLICIT REAL*8(A-H,O-Z)
    COMMON /BLOCKA/ NUMNP,X(NNP),Y(NNP),NUMEL,NI(NEL),NJ(NEL),
   1NK(NEL), TITLE(20), IBAND, IFLAG(5), TOL, RELAX
    COMMON /BLOCKC/NCODNP,NODEID(NNP),TRANS(NNP),HYDK1(NNP),THCK(NNP),
   1REC(NNP),SC(NNP),S,HEAD(NNP),HDI(NNP)
    COMMON /BLOCKD/ NCODEL,IDELEM(NEL),RECH(NEL),VPRM(NEL),AREA(NEL),
                HDLEAK(NEL)
    COMMON /BLOCKE/ AF(NNP.IB), BF(NNP.IB), DF(NNP), CM(NNP,IB), RHS(NNP)
    COMMON /BLOCKG/ NUMBS,NGHB(NBS,2),GHBCOND(NBS),GHBHEAD(NBS),
   1SLENGTH(NBS),QGHB(NBS),QBSNODE(NNP),QDR(NNP),DRCOND(NNP),
   2DRELEV(NNP)
    COMMON /BLOCKT/GS(NNP), ZBED(NNP), ZBASE(NNP), HYDK2(NNP)
C
    IF (IFLAG(1), EQ.O, AND, NCALL, GT.1) GO TO 170
    IF (IFLAG(1),EQ.2.AND.NCALL.GT.1) GO TO 170
    IF (IFLAG(1).EQ.1 .OR. IFLAG(1) .EQ. 3)CALL TRANADJ
С
С
    PERFORM ELEMENT INTEGRATIONS (A MATRIX - FLOW)
 110 DO 120 I = 1, NUMNP
    DO 120 J = 1,IBAND
 120 AF(I,J) = 0.
    DO 130 I = 1, NUMEL
      TA4 = (TRANS(NI(I)) + TRANS(NJ(I)) + TRANS(NK(I)))/(AREA(I)*12.)
      E1 = ((Y(NJ(I)) - Y(NK(I))) * (Y(NJ(I)) - Y(NK(I)))
          +(X(NK(I)) - X(NJ(I))) * (X(NK(I)) - X(NJ(I)))) * TA4
      E2 = ((Y(NK(I)) - Y(NI(I))) * (Y(NJ(I)) - Y(NK(I)))
          +(X(NI(I)) - X(NK(I))) * (X(NK(I)) - X(NJ(I)))) * TA4
      E3 = ((Y(NI(I)) - Y(NJ(I))) * (Y(NJ(I)) - Y(NK(I)))
          +(X(NJ(I)) - X(NI(I))) * (X(NK(I)) - X(NJ(I)))) * TA4
      E4 = ((Y(NK(I)) - Y(NI(I))) * (Y(NK(I)) - Y(NI(I)))
          +(X(NI(I)) - X(NK(I))) * (X(NI(I)) - X(NK(I)))) * TA4
      E5 = ((Y(NI(I)) - Y(NJ(I))) * (Y(NK(I)) - Y(NI(I)))
          +(X(NJ(I)) - X(NI(I))) * (X(NI(I)) - X(NK(I)))) * TA4
      E6 = ((Y(NI(I)) - Y(NJ(I))) * (Y(NI(I)) - Y(NJ(I)))
          +(X(NJ(I)) - X(NI(I))) * (X(NJ(I)) - X(NI(I)))) * TA4
     .....LOCATE IN BANDED GLOBAL MATRIX (SYMMETRIC)
      IJ = IABS(NI(I) - NJ(I)) + 1
      IK = IABS(NI(I) - NK(I)) + 1
      JK = IABS(NJ(I) - NK(I)) + 1
      AF(NI(I),1) = AF(NI(I),1) + E1
      IF (NI(I).LT.NJ(I)) AF(NI(I),IJ) = AF(NI(I),IJ) + E2
      IF (NJ(I),LT,NI(I)) AF(NJ(I),IJ) = AF(NJ(I),IJ) + E2
      IF (NI(I),LT,NK(I)) AF(NI(I),IK) = AF(NI(I),IK) + E3
      IF (NK(I),LT,NI(I)) AF(NK(I),IK) = AF(NK(I),IK) + E3
      AF(NJ(I),1) = AF(NJ(I),1) + E4
      IF (NJ(I).LT.NK(I)) AF(NJ(I),JK) = AF(NJ(I),JK) + E5
      IF (NK(I).LT.NJ(I)) AF(NK(I),JK) = AF(NK(I),JK) + E5
      AF(NK(I),1) = AF(NK(I),1) + E6
С
       .....ADJUST COEFF. MATRIX FOR LEAKAGE TERMS
      IF(IDELEM(I).NE.O ,AND. VPRM(I).NE.O.O) THEN
        AF(NI(I),1) = AF(NI(I),1) - 2.*VPRM(I)*AREA(I)/12.
        IF(NI(I),LT,NJ(I)) AF(NI(I),IJ) = AF(NI(I),IJ)
                                  - VPRM(I)*AREA(I)/12.
        IF (NJ(I).LT.NI(I)) AF(NJ(I),IJ) = AF(NJ(I),IJ)
                                  - VPRM(I)*AREA(I)/12.
        IF(NI(I),LT,NK(I)) AF(NI(I),IK) = AF(NI(I),IK)
                                  - VPRM(I)*AREA(I)/12.
        IF (NK(I),LT,NI(I)) AF(NK(I),IK) = AF(NK(I),IK)
                                  - VPRM(I)*AREA(I)/12.
        AF(NJ(I),1) = AF(NJ(I),1) - 2.*VPRM(I)*AREA(I)/12.
        IF (NJ(I).LT.NK(I)) AF(NJ(I),JK) = AF(NJ(I),JK)
```

```
- VPRM(I)*AREA(I)/12.
        IF (NK(I).LT.NJ(I)) AF(NK(I),JK) = AF(NK(I),JK)
                                - VPRM(I)*AREA(I)/12.
        AF(NK(I),1) = AF(NK(I),1) - 2.*VPRM(I)*AREA(I)/12.
      FND IF
 130 CONTINUE
C
С
     .....ADJUST COEFF. FOR HEAD-DEPENDANT NODES (DRAINS/RIVERS)
    DO 135 \text{ NP} = 1, NUMNP
      IF(NODEID(NP).GE.1 .AND. NODEID(NP).LE.10) GO TO 135
      AF(NP,1) = AF(NP,1) + ABS(DRCOND(NP))
 135 CONTINUE
C
C
    .....ADJUST COEFF. FOR GHB CONTRIBUTION FOR BOUNDARY SEGMENT NODES
    IF (NUMBS .GT. 0) THEN
      DO 140 NS = 1, NUMBS
        AF(NGHB(NS,1),1) = AF(NGHB(NS,1),1) +
                     ((1/2.)* SLENGTH(NS)*GHBCOND(NS))
        AF(NGHB(NS,2),1) = AF(NGHB(NS,2),1) +
                     ((1/2.)* SLENGTH(NS)*GHBCOND(NS))
 140 CONTINUE
    END IF
    IF (NCALL.GT.1) GO TO 170
C
С
С
    .....PERFORM ELEMENT INTEGRATIONS ( B MATRIX - FLOW)
    DO 145 I = 1, NUMNP
    DO 145 J = 1,IBAND
 145 BF(I,J) = 0.
    DO 160 I = 1, NUMEL
      E1 = (3*SC(NI(I)) + SC(NJ(I)) + SC(NK(I))) * AREA(I)/30.
      E2 = (2*SC(NI(I)) + 2*SC(NJ(I)) + SC(NK(I))) * AREA(I)/60.
     E3 = (2*SC(NI(I)) + SC(NJ(I)) + 2*SC(NK(I))) * AREA(I)/60.
      E4 = (SC(NI(I)) + 3*SC(NJ(I)) + SC(NK(I))) * AREA(I)/30.
      E5 = (SC(NI(I)) + 2*SC(NJ(I)) + 2*SC(NK(I))) * AREA(I)/60.
      E6 = (SC(NI(I)) + SC(NJ(I)) + 3*SC(NK(I))) * AREA(I)/30.
C
    .....MASS LUMPING
     E1 = E1 + E2 + E3
     E4 = E2 + E4 + E5
     E6 = E3 + E5 + E6
     E2 = 0.
      E3 = 0.
      F5 = 0
C
    .....LOCATE IN BANDED GLOBAL MATRIX (SYMMETRIC)
 150 IJ = IABS(NI(I) - NJ(I)) + 1
     IK = IABS(NI(I) - NK(I)) + 1
      JK = IABS(NJ(I) - NK(I)) + 1
      BF(NI(I),1) = BF(NI(I),1) + E1
     IF (NI(I),LT,NJ(I)) BF(NI(I),IJ) = BF(NI(I),IJ) + E2
      IF (NJ(I).LT.NI(I)) BF(NJ(I),IJ) = BF(NJ(I),IJ) + E2
      IF (NI(I).LT.NK(I)) BF(NI(I),IK) = BF(NI(I),IK) + E3
      IF (NK(I).LT.NI(I)) BF(NK(I),IK) = BF(NK(I),IK) + E3
      BF(NJ(I),1) = BF(NJ(I),1) + E4
     IF (NJ(I).LT.NK(I)) BF(NJ(I),JK) = BF(NJ(I),JK) + E5
      IF (NK(I),LT,NJ(I)) BF(NK(I),JK) = BF(NK(I),JK) + E5
      BF(NK(I),1) = BF(NK(I),1) + E6
 160 CONTINUE
С
C
    .....PERFORM ELEMENT INTEGRATION ( MATRICES D,E&F - FLOW)
       LOCATE IN GLOBAL MATRIX
 170 DO 180 NP = 1, NUMNP
```

```
180 DF(NP) = 0.
C
   DO 200 NE = 1, NUMEL
     QLEK = 0.
     QRECH = 0.
     IF (VPRM(NE) .NE. O.O) THEN
       QLEK = - VPRM(NE) * AREA(NE) * HDLEAK(NE) / 3.
     END IF
     QRECH = RECH(NE) * AREA(NE)/3.
     DF(NI(NE)) = DF(NI(NE)) + QRECH + QLEK
     DF(NJ(NE)) = DF(NJ(NE)) + QRECH + QLEK
     DF(NK(NE)) = DF(NK(NE)) + QRECH + QLEK
 200 CONTINUE
C
C
    .....ADD HEAD-DEPENDANT NODES (DRAINS AND RIVERS) AND POINT SOURCE
        (WELLS) TO SOURCE VECTOR, EXCLUDING CONSTANT HEAD FLOWS
С
С
                                  DRCOND = -, RIVER
         DRCOND = +, DRAIN
   DO 220 NP = 1.NUMNP
     IF (NODEID(NP).GE.1 .AND. NODEID(NP).LE.10) THEN
       REC(NP) = 0.0
       DRCOND(NP) = 0.0
     END IF
     IF (HEAD(NP).GT.DRELEV(NP) .AND. DRCOND(NP).GT.0.0) THEN
       DF(NP) = DF(NP) - DRCOND(NP)*DRELEV(NP)
     ELSEIF (HEAD(NP).LE.DRELEV(NP) .AND. DRCOND(NP).LT.0.0) THEN
       DF(NP) = DF(NP) - (ABS(DRCOND(NP)))*DRELEV(NP)
       DF(NP) = DF(NP) + REC(NP)
     END IF
 220 CONTINUE
    .....ADD GHB CONTRIBUTIONS TO POINT SOURCE VECTOR
C
    IF (NUMBS .GT. 0) THEN
     DO 235 NS = 1, NUMBS
       DO 230 NP = 1, NUMNP
         IF (NP .EQ. NGHB(NS,1)) THEN
           DF(NP) = DF(NP)-0.5*SLENGTH(NS)*GHBCOND(NS)*GHBHEAD(NS)
         ELSE IF (NP .EQ. NGHB(NS,2)) THEN
           DF(NP) = DF(NP)-0.5*SLENGTH(NS)*GHBCOND(NS)*GHBHEAD(NS)
         END IF
 230
         CONTINUE
 235 CONTINUE
    END IF
 999 RETURN
    END
    SUBROUTINE MATSOL
    PARAMETER (NNP = 3500, NEL = 7000, IB = 75, NBS = 200)
   ****IMPLICIT REAL*8(A-H,O-Z)
    COMMON /BLOCKA/ NUMNP, X(NNP), Y(NNP), NUMEL, NI(NEL), NJ(NEL),
   1NK(NEL),TITLE(20),IBAND,IFLAG(5),TOL,RELAX
    COMMON /BLOCKB/ NTIM, NPMP, PINT, TIMX, TINIT, TPDAY, SUMT,
   1TDEL,TIMY
    COMMON /BLOCKC/NCODNP,NODEID(NNP),TRANS(NNP),HYDK1(NNP),THCK(NNP),
   1REC(NNP), SC(NNP), S, HEAD(NNP), HDI(NNP)
    COMMON /BLOCKE/ AF(NNP,IB),BF(NNP,IB),DF(NNP),CM(NNP,IB),RHS(NNP)
    COMMON /BLOCKG/ NUMBS, NGHB(NBS, 2), GHBCOND(NBS), GHBHEAD(NBS),
   1SLENGTH(NBS),QGHB(NBS),QBSNODE(NNP),QDR(NNP),DRCOND(NNP),
   2DRELEV(NNP)
    DIMENSION TMP(NNP)
    COMMON /BLOCKH/ PRINTIT
    CHARACTER*1 PRINTIT
    THIS SUBROUTINE ASSEMBLES AND SOLVES THE FLOW EQUATION
```

```
(MATRIX(AF) + (MATRIX(BF)/TDEL)) = LHS COEFFICIENT MATRIX(CM)
    (((MATRIX(BF)/TDEL) * VECTOR(HEAD)) - VECTOR(DF)) = KNOWN RHS VECTOR
С
    SOLUTION IS BY BANDED GAUSSIAN ELIMINATION
С
С
    .....COEFFICIENT MATRIX
   DO 100 I = 1, NUMNP
     DO 100 J = 1,IBAND
       CM(I,J) = AF(I,J) + BF(I,J)/TDEL
 100 CONTINUE
C
C
    .....RHS VECTOR
   CALL MULT (NUMNP, IBAND, BF, HEAD, RHS)
   DO 110 I = 1, NUMNP
 110 \text{ RHS(I)} = \text{RHS(I)/TDEL} - \text{DF(I)}
C
    .....BLAST CONSTANT HEAD NODES
С
   DO 115I = 1, NUMNP
     TMP(I) = RHS(I)
 115 CONTINUE
   DO 1201 = 1, NUMNP
     IF ((NODEID(I) .EQ. 0) .OR. (NODEID(I) .GT. 10)) GO TO 120
     RHS(I) = RHS(I) - CM(I,1) + HEAD(I)
     CM(I,1) = 1.0E + 10
     RHS(I) = RHS(I) + CM(I,1) * HEAD(I)
 120 CONTINUE
C
    .....SOLVE MATRIX EQUATION BY GAUSS ELIMINATION
   CALL UDU(NUMNP, IBAND, CM, RHS)
C
   WRITE (7,155) SUMT
   WRITE (*,155) SUMT
 155 FORMAT (/,5X,28HMATSOL-UDU GAUSS ELIMINATION,10X,5HTIME = ,F12.7)
   DO 160 I = 1, NUMNP
 160 \text{ HEAD(I)} = \text{RHS(I)}
С
    .....CALCULATE FLOW FROM CONSTANT HEAD NODES
   DO 170I = 1, NUMNP
     DO 165 J = 1,IBAND
       CM(I,J) = AF(I,J) + BF(I,J)/TDEL
165
       CONTINUE
     RHS(I) = TMP(I)
170 CONTINUE
   CALL MULT (NUMNP, IBAND, CM, HEAD, DF)
C
   DO 175 I = 1, NUMNP
     IF ((NODEID(I) .EQ. 0) .OR. (NODEID(I) .GT. 10)) GO TO 175
     REC(I) = RHS(I) - DF(I)
 175 CONTINUE
C
1000 RETURN
   END
   SUBROUTINE UDU(NUMNP, IBAND, A, B)
   PARAMETER (NNP = 3500, NEL = 7000, IB = 75, NBS = 200)
C**** IMPLICIT REAL*8(A-H,O-Z)
   DIMENSION A(NNP,IB),B(NNP)
C
C
C
    THIS SUBROUTINE SOLVES THE MATRIX EQUATION AX=B BY GAUSSIAN
    ELIMINATION. THE MATRIX (A) IS A BANDED SYMMETRIC MATRIX AND (X)
    AND (B) ARE COLUMN VECTORS. THE RESULT IS RETURNED IN VECTOR (B).
C
    NUMNP = NUMBER OF EQUATIONS AND IBAND = BANDWIDTH
C
```

```
С
   NEM1 = NUMNP - 1
С
   DO 120 I = 1,NEM1
     JEND = NUMNP - I + 1
     IF (JEND.GT.IBAND) JEND = IBAND
С
     DO 110 J = 2, JEND
       J1 = I + J - 1
C
       FAC = A(I,J)/A(I,1)
C
       K1 = 0
       DO 100 K = J, JEND
С
         K1 = K1 + 1
         A(J1,K1) = A(J1,K1) - A(I,K) * FAC
 100
        CONTINUE
       A(I,J) = FAC
C
       B(J1) = B(J1) - B(I) * A(I,J)
 110 CONTINUE
 120 CONTINUE
С
С
    BACK SUBSTITUTION
C
    B(NUMNP) = B(NUMNP)/A(NUMNP,1)
С
    DO 140 I = 1,NEM1
     I1 = NUMNP - I
     B(11) = B(11)/A(11,1)
     JEND = NUMNP - I1 + 1
     IF (JEND.GT.IBAND) JEND = IBAND
     DO 130 J = 2, JEND
       J1 = I1 + J - 1
       B(11) = B(11) - A(11,J) * B(J1)
 130 CONTINUE
 140 CONTINUE
 999 RETURN
    END
    SUBROUTINE MULT(NUMNP,IBAND,A,X,Y)
    PARAMETER (NNP = 3500, NEL = 7000, IB = 75, NBS = 200)
C****IMPLICIT REAL*8(A-H,O-Z)
    DIMENSION A(NNP,IB),X(NNP),Y(NNP)
С
С
С
    THIS SUBROUTINE MULTIPLIES A BANDED SYMMETRIC MATRIX TIMES A
     VECTOR. THE PRODUCT OF MATRIX(A) AND VECTOR(X) IS VECTOR(Y).
С
C
С
С
С
     IBAND MUST BE .LE. (NUMNP/2)
С
     CHECK LIMITS ON IBAND
    IBT2 = IBAND * 2
    IF (IBT2 .GT. NUMNP) THEN
      WRITE (7,100)
      WRITE (*,100)
  100 FORMAT (///,9X,'*** E R R O R *** # MULT1 ',/
        ' IBAND MUST BE LESS OR EQUAL TO (NUMNP/2)',//)
      STOP
```

```
END IF
С
С
С
   (1) ROW
 110 Y(1) = 0.
   DO 120 J = 1,IBAND
 120 Y(1) = A(1,J) * X(J) + Y(1)
C
    (2) TO (IBAND) ROW
   DO 150 I = 2,IBAND
     Y(I) = 0.
     IR = I - 1
     DO 130 J = 1,IBAND
       IR = IR + 1
 130 Y(I) = A(I,J) * X(IR) + Y(I)
     JC = 1
     IR = I
     DO 140 K = 2,I
       JC = JC + 1
       IR = IR - 1
 140 Y(I) = A(IR,JC) * X(IR) + Y(I)
 150 CONTINUE
C
    (IBAND+1) TO (NUMNP-(IBAND-1)) ROW
   KR = NUMNP - IBAND + 1
   IBP1 = IBAND + 1
   DO 180 I = IBP1,KR
     Y(1) = 0.
     IR = 1 - 1
     DO 160 J = 1,IBAND
      IR = IR + 1
 160 Y(I) = A(I,J) * X(IR) + Y(I)
     JC = 1
     IR = I
     DO 170 K = 2,IBAND
       JC = JC + 1
       IR = IR - 1
 170 Y(I) = A(IR,JC) * X(IR) + Y(I)
 180 CONTINUE
С
С
    (NUMNP-IBAND + 2) TO (NUMNP) ROW
   KR = NUMNP - IBAND + 2
   KC = IBAND - 1
   DO 210 I = KR, NUMNP
     Y(I) = 0.
     IR = I - 1
     DO 190 J = 1,KC
       IR = IR + 1
 190 Y(I) = A(I,J) * X(IR) + Y(I)
     JC = 1
     IR = I
     DO 200 K = 2,IBAND
       JC = JC + 1
       IR = IR - 1
 200 Y(I) = A(IR,JC) * X(IR) + Y(I)
     KC = KC - 1
 210 CONTINUE
С
 999 RETURN
   END
   SUBROUTINE MATFLOW
   THIS SUBROUTINE ASSEMBLES AND SOLVES THE FLOW EQUATION
    (MATRIX(AF) + (MATRIX(BF)/TDEL)) = LHS COEFFICIENT MATRIX
```

```
(((MATRIX(BF)/TDEL) * VECTOR(HEAD)) - VECTOR(DF)) = KNOWN RHS VECTOR
C
    SOLUTION IS BY THE POINT SUCCESIVE OVERRELAXATION ITERATIVE METHOD
С
   PARAMETER (NNP = 3500, NEL = 7000, IB = 75, NBS = 200)
C*****IMPLICIT REAL*8(A-H,O-Z)
   COMMON /BLOCKA/ NUMNP,X(NNP),Y(NNP),NUMEL,NI(NEL),NJ(NEL),
   1NK(NEL), TITLE(20), IBAND, IFLAG(5), TOL, RELAX
   COMMON /BLOCKB/ NTIM, NPMP, PINT, TIMX, TINIT, TPDAY, SUMT,
   +TDEL,TIMY
   COMMON /BLOCKC/NCODNP, NODEID(NNP), TRANS(NNP), HYDK1(NNP), THCK(NNP),
   1REC(NNP),SC(NNP),S,HEAD(NNP),HDI(NNP)
   COMMON /BLOCKE/ AF(NNP.IB), BF(NNP.IB), DF(NNP), CM(NNP,IB), RHS(NNP)
   COMMON /BLOCKH/ PRINTIT
   CHARACTER*1 PRINTIT
C
C
    ....ABSOLUTE CONVERGENCE TEST
C
    .....(1) ROW
   SUM = 0.
   DO 100 J = 2.IBAND
 100 \text{ SUM} = (AF(1,J) + BF(1,J)/TDEL) + SUM
   IF (SUM.GT.(AF(1,1) + BF(1,1)/TDEL)) GO TO 170
    ....(2) TO (IBAND) ROW
   DO 130 I = 2,IBAND
     SUM = 0.
     DO 110 J = 2,IBAND
 110 SUM = (AF(I,J) + BF(I,J)/TDEL) + SUM
     JC = 1
     IR = I
     DO 120 K = 2,I
       JC = JC + 1
       IR = IR - 1
 120 SUM = (AF(IR,JC) + BF(IR,JC)/TDEL) + SUM
     IF (SUM.GT.(AF(I,1) + BF(I,1)/TDEL)) GO TO 170
 130 CONTINUE
C
    .....(IBAND+1) TO (NUMNP) ROW
    IBP1 = IBAND + 1
   DO 160 I = IBP1,NUMNP
     SUM = 0.
     DO 140 J = 2,IBAND
 140 SUM = (AF(I,J) + BF(I,J)/TDEL) + SUM
     JC = 1
     IR = I
     DO 150 \text{ K} = 2.\text{IBAND}
       JC = JC + 1
       IR = IR - 1
 150 SUM = (AF(IR,JC) + BF(IR,JC)/TDEL) + SUM
     IF (SUM.GT.(AF(I,1) + BF(I,1)/TDEL)) GO TO 170
  160 CONTINUE
    GO TO 190
  170 WRITE (7,180)
    WRITE (*,180)
  180 FORMAT (//,1H0,
                  ***** ERROR -- #PISOR1 ***WARNING***'/
   +10X,
                 ABSOLUTE CONVERGENCE TEST FAILED IN MATFLOW'///)
    +10X,
 190 CONTINUE
С
     .....CHECK ON TOL VS. AQUIFER THICKNESS
    DO 195 IPNT = 1,NUMNP
     IF (TRANS(IPNT) .LE. 0.1) GO TO 195
     TOLCHK = TOL / ( TRANS(IPNT)/HYDK1(IPNT) )
     IF (TOLCHK .GE. 0.01) THEN
       WRITE (*,194) IPNT
       WRITE (7,194) IPNT
```

```
FORMAT(//,
 194
                 ***** E R R O R -- PISOR2 *** WARNING ***'/
       10X,'AT NODE ',I4,' THE TOLERANCE (TOL) IS WITHIN 1 PERCENT O
      F THE THICKNESS'.//)
      GO TO 198
    END IF
 195 CONTINUE
 198 CONTINUE
С
    .....RHS VECTOR
   CALL MULT (NUMNP, IBAND, BF, HEAD, RHS)
   DO 200 I = 1,NUMNP
 200 \text{ RHS(I)} = \text{RHS(I)/TDEL} - \text{DF(I)}
   ITMAX = 200
C
   DO 390 IT = 1,ITMAX
     ERROR = 0.0
C
    .....(1) ROW
     SUM = 0.
     DO 210 J = 2.IBAND
 210 SUM = (AF(1,J) + BF(1,J)/TDEL) * HEAD(J) + SUM
     IF (NODEID(1).EQ.O.OR.NODEID(1).GT.10) GO TO 220
     REC(1) = RHS(1) - SUM - ((AF(1,1) + BF(1,1)/TDEL) * HEAD(1))
     GO TO 230
 220 HNEW = (RHS(1) - SUM)/(AF(1,1) + BF(1,1)/TDEL)
     RESID = HNEW - HEAD(1)
     HEAD(1) = HEAD(1) + RELAX * RESID
     RESID = ABS(RESID)
     ERROR = AMAX1(ERROR, RESID)
 230 CONTINUE
С
    .....(2) TO (IBAND) ROW
     DO 270 I = 2,IBAND
       SUM = 0.
       IR = I
       DO 240 J = 2,IBAND
        IR = IR + 1
 240
        SUM = (AF(I,J) + BF(I,J)/TDEL) * HEAD(IR) + SUM
       JC = 1
       IR = I
       DO 250 K = 2.1
         JC = JC + 1
        IR = IR - 1
        SUM = (AF(IR,JC) + BF(IR,JC)/TDEL) * HEAD(IR) + SUM
 250
       IF (NODEID(I).EQ.O.OR.NODEID(I).GT.10) GO TO 260
       REC(I) = RHS(I) - SUM - ((AF(I,1) + BF(I,1)/TDEL) * HEAD(I))
       GO TO 270
        HNEW = (RHS(I) - SUM)/(AF(I,1) + BF(I,1)/TDEL)
 260
       RESID = HNEW - HEAD(I)
       HEAD(I) = HEAD(I) + RELAX * RESID
       RESID = ABS(RESID)
       ERROR = AMAX1(ERROR, RESID)
 270 CONTINUE
С
    .....(IBAND+1) TO (NUMNP-(IBAND-1)) ROW
     KR = NUMNP - IBAND + 1
     IBP1 = IBAND + 1
     DO 310 I = IBP1,KR
       SUM = 0.
       IR = I
       DO 280 J = 2,IBAND
        IR = IR + 1
 280
        SUM = (AF(I,J) + BF(I,J)/TDEL) * HEAD(IR) + SUM
```

```
JC = 1
       IR = I
       DO 290 K = 2,IBAND
        JC = JC + 1
        IR = IR - 1
 290
        SUM = (AF(IR,JC) + BF(IR,JC)/TDEL) * HEAD(IR) + SUM
       IF (NODEID(I),EQ.O,OR.NODEID(I),GT.10) GO TO 300
       REC(I) = RHS(I) - SUM - ((AF(I,1) + BF(I,1)/TDEL) * HEAD(I))
       GO TO 310
        HNEW = (RHS(I) - SUM)/(AF(I,1) + BF(I,1)/TDEL)
 300
       RESID = HNEW - HEAD(I)
       HEAD(I) = HEAD(I) + RELAX * RESID
       RESID = ABS(RESID)
       ERROR = AMAX1(ERROR, RESID)
 310 CONTINUE
С
    .....(NUMNP-IBAND+2) TO (NUMNP-1) ROW
С
     NUMNP1 = NUMNP - 1
     KR = NUMNP - IBAND + 2
     KC = IBAND - 1
     DO 350 I = KR, NUMNP1
       SUM = 0.
       IR = I
       DO 320 J = 2,KC
         IR = IR + 1
        SUM = (AF(I,J) + BF(I,J)/TDEL) * HEAD(IR) + SUM
 320
       JC = 1
       IR = I
       DO 330 K = 2,IBAND
         JC = JC + 1
         IR = IR - 1
        SUM = (AF(IR,JC) + BF(IR,JC)/TDEL) * HEAD(IR) + SUM
 330
       IF (NODEID(I).EQ.O.OR.NODEID(I).GT.10) GO TO 340
       REC(I) = RHS(I) - SUM - ((AF(I,1) + BF(I,1)/TDEL) * HEAD(I))
       GO TO 350
        HNEW = (RHS(I) - SUM)/(AF(I,1) + BF(I,1)/TDEL)
 340
       RESID = HNEW - HEAD(I)
       HEAD(I) = HEAD(I) + RELAX * RESID
       RESID = ABS(RESID)
       ERROR = AMAX1(ERROR, RESID)
       KC = KC - 1
 350
       CONTINUE
С
С
    ....(NUMNP) ROW
     SUM = 0.
     JC = 1
      IR = NUMNP
     DO 360 K = 2,IBAND
       JC = JC + 1
       IR = IR - 1
 360 SUM = (AF(IR,JC) + BF(IR,JC)/TDEL) * HEAD(IR) + SUM
      IF (NODEID(NUMNP).EQ.O.OR.NODEID(NUMNP).GT.10) GO TO 370
      REC(NUMNP) = RHS(NUMNP) - SUM - ((AF(NUMNP,1) + BF(NUMNP,1)/TDE)
   1 L) * HEAD(NUMNP))
      GO TO 380
 370 HNEW = (RHS(NUMNP) - SUM)/(AF(NUMNP,1) + BF(NUMNP,1)/TDEL)
      RESID = HNEW - HEAD(NUMNP)
      HEAD(NUMNP) = HEAD(NUMNP) + RELAX * RESID
      RESID = ABS(RESID)
      ERROR = AMAX1(ERROR, RESID)
 380 IF (ERROR.LE.TOL) GO TO 410
 390 CONTINUE
С
    WRITE (7,400)
    WRITE (*,400)
  400 FORMAT (////,1H1,
```

```
+10X.1
             ***** ERROR -- #PISOR3 ******',/
   + 10X,'STOP--MAXIMUM ALLOWABLE NUMBER OF ITERATIONS HAS BEEN',/
   +10X, 'REACHED IN SUBROUTINE MATFLOW (NO SOLUTION REACHED)'///
   STOP
C
 410 WRITE (7,420) IT, SUMT
   WRITE (*,420) IT, SUMT
 420 FORMAT (/,5X'MATFLOW ITERATIONS = 'I5,10X'TIME = 'F12.7)
С
 440 RETURN
   END
   SUBROUTINE WATBAL
C
C
    THIS SUBROUTINE CALCULATES A WATER BALANCE
C
   PARAMETER (NNP = 3500, NEL = 7000, IB = 75, NBS = 200)
C*****IMPLICIT REAL*8(A-H,O-Z)
   COMMON /BLOCKA/ NUMNP,X(NNP),Y(NNP),NUMEL,NI(NEL),NJ(NEL),
   1NK(NEL), TITLE(20), IBAND, IFLAG(5), TOL, RELAX
   COMMON /BLOCKB/ NTIM, NPMP, PINT, TIMX, TINIT, TPDAY, SUMT,
   1TDEL.TIMY
   COMMON /BLOCKC/NCODNP, NODEID (NNP), TRANS (NNP), HYDK1 (NNP), THCK (NNP),
   1REC(NNP),SC(NNP),S,HEAD(NNP),HDI(NNP)
   COMMON /BLOCKD/ NCODEL,IDELEM(NEL),RECH(NEL),VPRM(NEL),AREA(NEL),
              HDI FAK(NFL)
   COMMON /BLOCKF/QINRCH,QOUTRCH,QINREC,QOUTREC,QINCHN,QOUTCHN,
   1QINLEK,QOUTLEK,QSTOR,QINGHB,QOUTGHB,QINDR,QOUTDR
   COMMON /BLOCKG/ NUMBS,NGHB(NBS,2),GHBCOND(NBS),GHBHEAD(NBS),
  1SLENGTH(NBS),QGHB(NBS),QBSNODE(NNP),QDR(NNP),DRCOND(NNP),
  2DRELEV(NNP)
   COMMON /BLOCKH/ PRINTIT
   CHARACTER*1 PRINTIT
C
C
    .....CALCULATE FLUX FROM DISTRIBUTED RECHARGE AND DISCHARGE SOURCE
C
   DO 110 NE = 1, NUMEL
     IF (RECH(NE).GT.0.0) GO TO 100
     QINRCH = RECH(NE) * AREA(NE) * TDEL + QINRCH
     GO TO 110
 100 QOUTRCH = RECH(NE) * AREA(NE) * TDEL + QOUTRCH
 110 CONTINUE
С
    .....CALCULATE FLUX FROM POINT RECHARGE AND DISCHARGE SOURCES
С
       (EXCLUDING CONSTANT HEAD NODES)
   DO 130 NP = 1, NUMNP
     IF (NODEID(NP).GE.1.AND.NODEID(NP).LE.10) GO TO 130
     IF (REC(NP).GT.O.O) GO TO 120
     QINREC = REC(NP) * TDEL + QINREC
     GO TO 130
 120 QOUTREC = REC(NP) * TDEL + QOUTREC
 130 CONTINUE
C
    .....CALCULATE FLUX FROM POINT RECHARGE AND DISCHARGE SOURCES
C
      (AT CONSTANT HEAD NODES ONLY)
   DO 150 \text{ NP} = 1,\text{NUMNP}
     IF (NODEID(NP).EQ.O.OR.NODEID(NP).GT.10) GO TO 150
     IF (REC(NP).GT.O.O) GO TO 140
     QINCHN = REC(NP) * TDEL + QINCHN
     GO TO 150
 140 QOUTCHN = REC(NP) * TDEL + QOUTCHN
 150 CONTINUE
С
    .....CALCULATE FLUX FROM VERTICAL LEAKAGE
   DO 170 NE = 1, NUMEL
     IF (VPRM(NE).EQ.0.0) GO TO 170
```

```
HEADBAR = (HEAD(NI(NE)) + HEAD(NJ(NE)) + HEAD(NK(NE)))/3.
     VLEK = VPRM(NE) * (HEADBAR - HDLEAK(NE)) * AREA(NE)
     IF (VLEK.GT.0.0) GO TO 160
     QINLEK = VLEK * TDEL + QINLEK
     GO TO 170
 160 QOUTLEK = VLEK * TDEL + QOUTLEK
 170 CONTINUE
    .....CALCULATE FLUX FROM HEAD-DEPENDANT NODES (DRAINS AND RIVERS)
С
                                 DRCOND = -, RIVER
С
        DRCOND = +, DRAIN
   DO 180 NP=1,NUMNP
     IF (NODEID(NP).GE.1 ,AND, NODEID(NP).LE.10) GO TO 180
     IF (DRCOND(NP) .EQ. 0.0) THEN
       GO TO 180
     ELSEIF (HEAD(NP).LE.DRELEV(NP) .AND. DRCOND(NP).GT.O.O) THEN
       GO TO 180
     ELSEIF (HEAD(NP).LE.DRELEV(NP) .AND. DRCOND(NP).LT.O.0) THEN
       QDR(NP) = (ABS(DRCOND(NP))) * (HEAD(NP)-DRELEV(NP))
       QINDR = QINDR + QDR(NP)*TDEL
       QDR(NP) = DRCOND(NP) * (HEAD(NP)-DRELEV(NP))
       QOUTDR = QOUTDR + QDR(NP)*TDEL
     END IF
 180 CONTINUE
С
    .....CALCULATE GHB FLOW IN OR OUT OF THE DOMAIN
С
С
   IF (NUMBS .GT. 0) THEN
     DO 200 NS = 1,NUMBS
       QBSNODE(NGHB(NS,1)) = (SLENGTH(NS)*GHBCOND(NS))*
        (HEAD(NGHB(NS,1))/3. + HEAD(NGHB(NS,2))/6.-GHBHEAD(NS)/2.)
       QBSNODE(NGHB(NS,2)) = (SLENGTH(NS)*GHBCOND(NS))*
        (HEAD(NGHB(NS,2))/3. + HEAD(NGHB(NS,1))/6.-GHBHEAD(NS)/2.)
       QGHB(NS) = QBSNODE(NGHB(NS,1)) + QBSNODE(NGHB(NS,2))
       IF (QGHB(NS) .GT. 0.) GO TO 190
         QINGHB = QINGHB + QGHB(NS)*TDEL
       GO TO 200
 190
          QOUTGHB = QOUTGHB + QGHB(NS) *TDEL
 200
      CONTINUE
   END IF
С
    .....CALCULATE CHANGE IN STORAGE IN THE AQUIFER
   DO 260 NE = 1, NUMEL
     HEADBAR = (HEAD(NI(NE)) + HEAD(NJ(NE)) + HEAD(NK(NE)))/3.
     HDIBAR = (HDI(NI(NE)) + HDI(NJ(NE)) + HDI(NK(NE)))/3.
     SA = (SC(NI(NE)) + SC(NJ(NE)) + SC(NK(NE)))/3.
 260 QSTOR = SA * (HDIBAR - HEADBAR) * AREA(NE) + QSTOR
С
 999 RETURN
   END
    SUBROUTINE FLOWOUT
    PARAMETER (NNP = 3500, NEL = 7000, IB = 75, NBS = 200)
C**** IMPLICIT REAL*8(A-H,O-Z)
    COMMON /BLOCKA/ NUMNP,X(NNP),Y(NNP),NUMEL,NI(NEL),NJ(NEL),
   1NK(NEL), TITLE(20), IBAND, IFLAG(5), TOL, RELAX
    COMMON /BLOCKB/ NTIM,NPMP,PINT,TIMX,TINIT,TPDAY,SUMT,
   1TDEL.TIMY
    COMMON /BLOCKC/NCODNP, NODEID(NNP), TRANS(NNP), HYDK1 (NNP), THCK(NNP),
   1REC(NNP),SC(NNP),S,HEAD(NNP),HDI(NNP)
    COMMON /BLOCKF/QINRCH,QOUTRCH,QINREC,QOUTREC,QINCHN,QOUTCHN,
   1QINLEK,QOUTLEK,QSTOR,QINGHB,QOUTGHB,QINDR,QOUTDR
    COMMON /BLOCKG/ NUMBS,NGHB(NBS,2),GHBCOND(NBS),GHBHEAD(NBS),
   1SLENGTH(NBS),QGHB(NBS),QBSNODE(NNP),QDR(NNP),DRCOND(NNP),
```

```
2DRELEV(NNP)
   COMMON /BLOCKH/ PRINTIT
   DIMENSION ND(5), DRWDN(5)
   CHARACTER*1 PRINTIT
С
С
    THIS SUBROUTINE PRINTS THE MAJOR OUTPUT FROM THE MODEL.
    IT PRINTS A HEAD MAP, DRAWDOWN MAP, CUMULATIVE MASS BALANCE,
C
    FLOW BY NODE ID AND FLOW FROM CONSTANT HEAD NODES.
С
C
С
    .....PRINT HEAD VALUES -- FT
   WRITE (7,100)
 100 FORMAT (1H1,4X,23HHEAD DISTRIBUTION -- FT/5X,23H------
   1----)
   IF (S.EQ.O.) GO TO 130
   WRITE (7,110) SUMT
 110 FORMAT (1H0,4X,13HTIME(DAYS) = ,F10.3)
   WRITE (7,120) TIMY
 120 FORMAT (5X,13HTIME(YEARS) = ,F10.5)
   GO TO 150
 130 WRITE (7,140)
 140 FORMAT (1H0,4X,21HSTEADY STATE SOLUTION)
 150 WRITE (7,160)
 160 FORMAT (///1H ,9X,4HNODE,10X,4HHEAD,12X,4HNODE,10X,4HHEAD
   1 )
   WRITE (7.170) (NP, HEAD(NP), NP = 1, NUMNP)
 170 FORMAT (2(10X,15,5X,F12.3))
С
С
    .....PRINT DRAWDOWN VALUES -- FT
   WRITE (7,180)
 180 FORMAT (1H1,4X,27HDRAWDOWN DISTRIBUTION -- FT/5X,27H-----
   IF (S.EQ.0.) GO TO 190
   WRITE (7,110) SUMT
   WRITE (7,120) TIMY
   GO TO 200
 190 WRITE (7,140)
 200 WRITE (7,210)
 210 FORMAT (///1H ,9X,4HNODE,9X,8HDRAWDOWN,9X,4HNODE,9X,8HDRAWDOWN
  1)
   IR = 0
   KR = 1
   KC = 2
 220 DO 230 NP = KR,KC
     IR = IR + 1
     ND(IR) = NP
 230 DRWDN(IR) = HDI(NP) - HEAD(NP)
   WRITE (7,240) (ND(I),DRWDN(I),I = 1,IR)
 240 FORMAT (2(10X,15,5X,F12.3))
   IF (KC.EQ.NUMNP) GO TO 250
   IR = 0
   KR = KC + 1
   KC = KC + 2
   IF (KC.GT.NUMNP) KC = NUMNP
   GO TO 220
С
   .....PRINT CUMULATIVE WATER BALANCE -- GALLONS
 250 WRITE (7,260)
 260 FORMAT (///1H1,4X,36HCUMULATIVE WATER BALANCE -- GALLONS/5X,31H--
   WRITE (7,110) SUMT
   WRITE (7,120) TIMY
cccccccccccccccccccccccccccccccccc
    QINRCH = QINRCH*7.48048
    QOUTRCH = QOUTRCH*7.48048
```

```
QINREC = QINREC*7.48048
   OOUTREC = QOUTREC*7,48048
   QINDR = QINDR*7.48048
   QOUTDR = QOUTDR*7.48048
   QINGHB = QINGHB*7.48048
   QOUTGHB = QOUTGHB*7.48048
   QINLEK = QINLEK * 7.48048
   QOUTLEK = QOUTLEK * 7.48048
   QINCHN = QINCHN*7.48048
   QOUTCHN = QOUTCHN*7.48048
WRITE (7,270) QINRCH, QOUTRCH
270 FORMAT (//,15X,38HQINRCH (RECHARGE-DISTRIBUTED)
                                                       = F15.3,/,1
  15X.38HQOUTRCH (DISCHARGE-DISTRIBUTED)
   WRITE (7,280) QINREC, QOUTREC
 280 FORMAT (/,15X,38HQINREC (RECHARGE-POINT)
                                                    =,F15.3,/,15
  1X,38HQOUTREC (DISCHARGE-POINT)
                                        = ,F15.3)
   WRITE (7,285) QINDR,QOUTDR
 285 FORMAT (/,15X,38HQINDR (RECHARGE-RIVER)
                                                   =,F15.3,/,15
  1X,38HQOUTDR (DISCHARGE-DRAIN/RIVER)
                                           = ,F15.3)
   WRITE (7,287) QINGHB, QOUTGHB
                                                     =,F15.3,/,15
 287 FORMAT (/,15X,38HQINGHB (HEAD-DEP. INFLOW)
  1X,38HQOUTGHB (HEAD-DEP. OUTFLOW)
                                           = .F15.3)
   WRITE (7,290) QINLEK, QOUTLEK
 290 FORMAT (/,15X,38HQINLEK (RECHARGE-LEAKAGE)
                                                     =,F15.3,/,15
   1X,38HQOUTLEK (DISCHARGE-LEAKAGE)
                                          = .F15.3
   WRITE (7,310) QINCHN, QOUTCHN
 310 FORMAT (/,15X,38HQINCHN (RECHARGE-CONST HEAD NODES) =,F15.3,/,15
   1X.38HQOUTCHN (DISCHARGE-CONST HEAD NODES) = ,F15.3)
   QIN = QINRCH + QINREC + QINLEK + QINCHN + QINGHB + QINDR
   QOUT = QOUTRCH + QOUTREC + QOUTLEK + QOUTCHN + QOUTGHB + QOUTDR
   WRITE (7,320) QIN,QOUT
 320 FORMAT (56X,12H--
                       -----/,40X,13HTOTAL QIN = ,F15.3/,40X,13HTO
   1TAL\ QOUT = F15.3
   QSTOR=QSTOR*7.48048
   WRITE (7,330) QSTOR
 330 FORMAT (/,15X,38HQSTOR (WATER RELEASED FROM STORAGE) = ,F15.3)
    .....CALCULATE & PRINT MASS BALANCE RESIDUAL & ERROR AS A PER CENT
   QRESID = QIN + QOUT - QSTOR
   QRESID = ABS(QRESID)
   WRITE (7,340) QRESID
 340 FORMAT (//,25X,28HMASS BALANCE RESIDUAL
                                                = .F15.3)
   QERRIN = 0.
   IF (QIN.NE.O.O) QERRIN = ABS(QRESID)/( - QIN) * 100.
   QERROUT = 0.
   IF (QOUT.NE.0.0) QERROUT = ABS(QRESID)/QOUT * 100.
   QERRSTR = 0.
   IF (QSTOR.NE.0.0) QERRSTR = ABS(QRESID)/ABS(QSTOR) * 100.
   WRITE (7,350) QERRIN, QERROUT, QERRSTR
 350 FORMAT (25X,28HERROR AS PERCENT OF QIN =,F15.3/,25X,28HERROR AS
   1 PERCENT OF QOUT =,F15.3/,25X,28HERROR AS PERCENT OF QSTOR =,F1
   25.3)
2222222222222222222222222222222222
    QINRCH = QINRCH/7.48048
    QOUTRCH = QOUTRCH/7.48048
    QINREC = QINREC/7.48048
    QOUTREC = QOUTREC/7.48048
    QINDR = QINDR/7.48048
    QOUTDR = QOUTDR/7.48048
    QINGHB = QINGHB/7.48048
    QOUTGHB = QOUTGHB/7.48048
    QINLEK = QINLEK/7.48048
    QOUTLEK = QOUTLEK/7.48048
    QINCHN = QINCHN/7.48048
```

```
QOUTCHN = QOUTCHN/7.48048
   QSTOR = QSTOR/7.48048
С
   .....PRINT FLOW BY NODE ID -- GPM
   WRITE (7,360)
 360 FORMAT (///1H0,4X,23HFLOW BY NODE ID -- GPM/3X,28H-----
   DO 400 NC = 1,NCODNP
    QINNID = 0.
     QOUTNID = 0.
    DO 380 NP = 1, NUMNP
      IF (NODEID(NP).NE.NC) GO TO 380
      IF (REC(NP).LE.O.) GO TO 370
      QOUTNID = QOUTNID + REC(NP) / 86400.
      GO TO 380
 370
       QINNID = QINNID + REC(NP) / 86400.
 380
     CONTINUE
    IF (QINNID.EQ.O.O.AND.QOUTNID.EQ.O.O) GO TO 400
222222222222222222222222222222222222
    QINNID = QINNID * 448.8288
    QOUTNID = QOUTNID*448.8288
2222222222222222222222222222222222
    WRITE (7,390) NC,QINNID,NC,QOUTNID
 390 FORMAT (\frac{5}{5},5HQIN (\frac{5}{5},5HQIN (\frac{5}{5},5H,25) = \frac{5}{5}X,5HQOUT(\frac{5}{5},2H) = \frac{5}{5}X,F12.5)
222222222222222222222222222222222222
    QINNID = QINNID/448.8288
    QOUTNID = QOUTNID/448.8288
2222222222222222222222222222222222222
 400 CONTINUE
С
C
   .....PRINT FLOW BY NODE ID FOR DRAINS AND RIVERS
   DO 420 NC = 11,NCODNP
    QINNID = 0.
    QOUTNID = 0.
    DO 410 NP = 1, NUMNP
      IF (NODEID(NP).NE.NC) GO TO 410
      IF (DRCOND(NP).EQ.0) GO TO 410
      IF (QDR(NP).LE.O.) GO TO 405
      QOUTNID = QOUTNID + QDR(NP) / 86400.
      GO TO 410
 405
       QINNID = QINNID + QDR(NP) / 86400.
     CONTINUE
    IF (QINNID.EQ.0.0.AND.QOUTNID.EQ.0.0) GO TO 420
22222222222222222222222222222222222222
    QINNID = QINNID * 448.8288
    QOUTNID = QOUTNID * 448.8288
WRITE (7,415) NC,QINNID,NC,QOUTNID
 415 FORMAT (/5X,5HQIN (,15,2H) = ,5X,F12.5,' (RIVER NODE)'/
  +5X,5HQOUT(,15,2H) = ,5X,F12.5,' (RIVER/DRAIN NODE)')
QINNID = QINNID/448.8288
    QOUTNID = QOUTNID/448.8288
420 CONTINUE
C
   .....PRINT FLOW BY BOUNDARY SEGMENTS
   IF (NUMBS .GT. 0) THEN
    WRITE(7,430)
 430 FORMAT(//1H0,4X,'FLOW FROM GHB SEGMENTS -- GPM'/,5X,
  1 'POSITIVE IS OUTFLOW, NEGATIVE IS INFLOW')
    DO 440 NS = 1, NUMBS
     QGHB(NS) = QGHB(NS)/86400.
```

```
QGHB(NS) = QGHB(NS)*448.8288
222222222222222222222222222222222222
     WRITE(7.435)NS,QGHB(NS)
      FORMAT(5X, 5HSIDE(,15,2H) = ,5X,F12.5)
QGHB(NS) = QGHB(NS)/448.8288
QGHB(NS) = QGHB(NS)*86400.
440 CONTINUE
445 END IF
   .....PRINT FLOW FROM CONSTANT HEAD NODES -- GPM
C
   WRITE (7,450)
 450 FORMAT (///1H0,4X,42HFLOW FROM CONSTANT HEAD NODES -- GPM /,5
  1X,31HPOSITIVE IS DISCHARGE (PUMPAGE)/,5X,32HNEGATIVE IS RECHARGE (
  2INJECTION))
   DO 460 \text{ NP} = 1,\text{NUMNP}
    IF (NODEID(NP).EQ.O.OR.NODEID(NP).GT.10) GO TO 460
    REC(NP) = REC(NP) / 86400.
REC(NP) = REC(NP) * 448.8288
WRITE (7,455) NP,REC(NP).
REC(NP) = REC(NP)/448.8288
REC(NP) = REC(NP) * 86400.
 455 FORMAT (5X,5HNODE(,15,2H) = ,5X,F12.5)
 460 CONTINUE
   .....WRITE HEADS FOR PLOTTING
   WRITE(8,480)SUMT
 480 FORMAT (' HEAD SOLUTION -- TIME = ',F10.5,' DAYS.')
   WRITE (8.485)(NP, HEAD(NP), NP = 1, NUMNP)
 485 FORMAT (5(15,F10.2))
С
   .....WRITE DRAWDOWNS FOR PLOTTING
 500 WRITE (8,510) SUMT
 510 FORMAT (' DRAWDOWNS -- TIME = ',F10.5,' DAYS.')
   IR = 0
   KR = 1
   KC = 5
 520 DO 530 NP = KR,KC
    IR = IR + 1
    ND(IR) = NP
 530 DRWDN(IR) = HDI(NP) - HEAD(NP)
   WRITE (8,540) (ND(I),DRWDN(I),I = 1,IR)
 540 FORMAT (5(15,F10.2))
   IF (KC.EQ.NUMNP) GO TO 1000
   IR = 0
   KR = KC + 1
   KC = KC + 5
   IF (KC.GT.NUMNP) KC = NUMNP
   GO TO 520
 1000 CONTINUE
   CALL LAYER
 999 RETURN
   FND
   SUBROUTINE TRANADJ
    THIS SUBROUTINE ADJUSTS THE TRANSMISSIVITY FOR THE MODIFIED
    ONE LAYER MODEL AT THE ROCKY MOUNTAIN ARSENAL.
С
   PARAMETER (NNP = 3500, NEL = 7000, IB = 75, NBS = 200)
C*****IMPLICIT REAL*8(A-H,O-Z)
```

```
COMMON /BLOCKA/ NUMNP,X(NNP),Y(NNP),NUMEL,NI(NEL),NJ(NEL),
   1NK(NEL), TITLE(20), IBAND, IFLAG(5), TOL, RELAX
    COMMON /BLOCKC/NCODNP, NODEID(NNP), TRANS(NNP), HYDK1(NNP), THCK(NNP),
   1REC(NNP), SC(NNP), S, HEAD(NNP), HDI(NNP)
    COMMON /BLOCKD/ NCODEL, IDELEM(NEL), RECH(NEL), VPRM(NEL), AREA(NEL),
               HDLEAK(NEL)
    COMMON /BLOCKT/GS(NNP), ZBED(NNP), ZBASE(NNP), HYDK2(NNP)
C
С
С
    ADJUST TRANSMISSIVITY FOR MODIFIED ONE LAYER MODEL
    IF(IFLAG(1) .EQ. 3)THEN
    DO 100 I = 1, NUMNP
   IF(HEAD(I) .GT. GS(I))THEN
      TRANS(I) = HYDK1(I)* (GS(I)-ZBED(I)) + HYDK2(I)*(ZBED(I)-ZBASE(I))
   ELSEIF(HEAD(I) .LE. GS(I) .AND. HEAD(I) .GT. ZBED(I))THEN
      TRANS(I) = HYDK1(I)*(HEAD(I)-ZBED(I)) + HYDK2(I)*(ZBED(I)-ZBASE(I))
    ELSEIF(HEAD(I) .LE. ZBED(I) .AND. HEAD(I) .GT. ZBASE(I))THEN
      TRANS(I) = HYDK2(I)*(HEAD(I)-ZBASE(I))
    ELSE
      TRANS(I) = 0.
    ENDIF
 100 CONTINUE
C
C
    SET MINIMUM TRANSMISSIVITY
C
   DO 150 I = 1, NUMNP
     TMIN = HYDK2(I) * 1.
     IF(TRANS(I) .LT. TMIN)TRANS(I) = TMIN
 150 CONTINUE
   ENDIF
C
    ADJUST TRANSMISSIVITY FOR UNCONFINED AQUIFER
С
С
   IF(IFLAG(1) .EQ. 1)THEN
   DO 200 I = 1, NUMNP
   IF(HEAD(I) .GT. GS(I))THEN
     TRANS(I) = HYDK1(I)*(GS(I)-ZBED(I))
   ELSEIF(HEAD(I) .LE. GS(I) .AND. HEAD(I) .GT. ZBED(I))THEN
     TRANS(I) = HYDK1(I)*(HEAD(I)-ZBED(I))
   ELSE
      TRANS(I) = 0.
   ENDIF
 200 CONTINUE
С
С
    SET MINIMUM TRANSMISSIVITY
С
   DO 250 I = 1, NUMNP
     TMIN = HYDK1(I)*1.
     IF(TRANS(I) .LT. TMIN)TRANS(I) = TMIN
 250 CONTINUE
   ENDIF
 999 RETURN
   END
   SUBROUTINE LAYER
C
    THIS SUBROUTINE IDENTIFIES WHICH AQUIFER THE WATER LEVEL AT NODE I
С
    IS IN (BEDROCK OR ALLUVIUM).
   PARAMETER (NNP = 3500, NEL = 7000, IB = 75, NBS = 200)
C**** IMPLICIT REAL*8(A-H,O-Z)
   COMMON /BLOCKA/ NUMNP,X(NNP),Y(NNP),NUMEL,NI(NEL),NJ(NEL),
   1NK(NEL),TITLE(20),IBAND,IFLAG(5),TOL,RELAX
   COMMON /BLOCKC/NCODNP, NODEID(NNP), TRANS(NNP), HYDK1(NNP), THCK(NNP),
   1REC(NNP), SC(NNP), S, HEAD(NNP), HDI(NNP)
```

```
COMMON /BLOCKD/ NCODEL,IDELEM(NEL),RECH(NEL),VPRM(NEL),AREA(NEL),
          HDLEAK(NEL)
  COMMON /BLOCKT/GS(NNP), ZBED(NNP), ZBASE(NNP), HYDK2(NNP)
C
С
С
   IDENTIFY LAYER
С
  WRITE(7,30)
 30 FORMAT(//)
OPEN (10,FiLE = "hwhere.dat",STATUS = "NEW")
DO 100 I = 1, NUMNP
  IF(HEAD(I) .GT. GS(I))THEN
    WRITE(7,10)I
 10 FORMAT(' THE WATER LEVEL AT NODE ',15,' IS ABOVE GROUND SURFACE.')
  ELSEIF(HEAD(I) .LE. GS(I) .AND. HEAD(I) .GT. ZBED(I))THEN
C 15 FORMAT(' THE WATER LEVEL AT NODE ',15,' IS IN THE ALLUVIUM.')
  ELSEIF(HEAD(I) .LE. ZBED(I) .AND. HEAD(I) .GT. ZBASE(I))THEN
    WRITE(7,20)1
 20 FORMAT(' THE WATER LEVEL AT NODE ',15,' IS IN THE BEDROCK.')
    WRITE(7,25)1
 25 FORMAT(' NODE ',15,' IS DRY.')
  ENDIF
 100 CONTINUE
 999 RETURN
  END
```

## Appendix B Steady-State Calibration Input File

```
WES MESH
NTIM, NPMP, PINT, PRINTIT, TIMX, TINIT (215,F10.0,4X,A1,2F10.0)
50050 1 50000.00 Y 1.500 3600.000
SIMULATION OPTION IFLAG1(I1)-(0=CONFINED,1=UNCONFINED&3=M ODIFIED ONE LAYER MODEL)
SIMULATION OPTION IFLAG2, TOL, RELAX (11,2F10.0) - (0=GAUSS & 1=PISOR)
SIMULATION OPTION IFLAG3 (I1) - (0=GWFLOW DATA & 1=GWTRAN DATA)
NUMNP, NUMEL, IBAND (315)
3359 6466 69
NODAL COORDINATES: FCTR (F10.0); NODE, X,Y (3(15,2F10.0))
 400.000
     0.000
            17.540 2
                        0.432
                               17.169 3
                                          0.800
     0.861
            16.801
                        1.239
                               18.038
                                           1.550
     1.287
             16.435
                        1.676
                               17.666 9
                                           1.991
                                                 18.875
      2.250
             20.056
                         1.709
                                16.071 12
                                            1.700
                                                  16.737
      2.432
             18.500 14
                         2.689
                                19.681 15
                                            2.900
                                                   20.830
      3.333
             20.455
                    17
                         2.129
                                15.710
                                       18
                                            2.546
                                                   16.924
      2.874
             18.124 20
                         3.130
                                19.303 21
                                            3.769
                                                   20.076
 19
      3.385
             21.360
                    23
                         3.831
                                20.961
                                            2.545
                                                   15.351
      2.979
             16.556
                         3.315
                                17.749
                                            3.648
                                                   18.770
      4.209
             19.695
                    29
                         4.278
                                20.560
                                            3.841
                                                   21.860
      4.299
             21.437 32
                         2.958
                                14.995 33
                                            3.410
                                                   16.188
      3.757
             17.373
                    35
                         4.018
                                18.544
                                            4.653
                                                   19.311
 37
      4.729
             20.157 38
                         4.759
                                21.014 39
                                            4.267
                                                   22.330
      4.739
             21.885
                    41
                         3.367
                                14.641
                                       42
                                            3.840
                                                   15.821
      4.199
             16.997
                         4.464
                                18.163 45
                                            5.100
                                                   18.924
      5.181
             19.752
                    47
                         5.220
                                20.591 48
                                            5.212
                                                   21.441
 49
      4.663
             22.771
                    50
                         5.150
                                22.304 51
                                            3.774
                                                   14.290
 52
      4.268
             15.455
                    53
                         4.485
                                16.708 54
                                            4.913
                                                   17,779
      5.551
             18.535 56
                         5.637
                                19.346 57
                                            5.683
                                                   20.166
 58
      5.684
             20.997
                    59
                         5.636
                                21.839 60
                                            5.030
                                                   23.182
      5.253
             22.980 62
                         4.177
                                13.941 63
                                            4.695
                                                   15.091
      5.084
             16.244 65
                         5.364
                                17.395
                                            6.006
                                                   18.142
      6.094
             18.938 68
                         6.147
                                19.741 69
                                            6.157
                                                   20.552
      5.963
             21.392
                    71
                         6.031
                                22,208
                                            5.367
                                                   23.563
  73
      5.884
             23.054
                          4.577
                                13.594 75
                                            5.120
                                                   14.727
      5.527
             15.868
                          5.816
                                17.008
                                             6.464
                                                   17.747
      6.555
             18.528 80
                          6.612
                                19.315 81
                                             6.630
                                                   20.109
      6.604
             20.911
                    83
                          6.528
                                21.724
                                             6.398
                                                   22.549
      5.674
             23.915 86
                          6.208
                                23.386 87
                                             4.974
                                                   13.250
      5.544
             14.365
                          5.970
                                15.491
                                        90
                                             6.271
                                                   16.620
             17.349
      6.926
                          7.017
                                18.116 93
                                            7.305
                                                   19.052
       7.103
             19.665
                          7.086
                                20.450
                                        96
                                             7.023
                                                   21.243
             22.046 98
                          6.736
                                22.861 99
                                             5.952
                                                   24.237
 100
       6.502
              23.689 101
                          5.368
                                  12.908 102
                                                     14.004
                                  16.231 105
                                              6.200
                                                    24.530
 103
       6.413
              15.114 104
                           6.727
                                 24.824 108
                                                     24.970
 106
       6.335
              24.677 107
                           6.468
                                 25.259 111
                                              6.993
                                                     25.403
 109
       6.733
              25.115 110
                           6.864
                           7.251
                                  25.689 114
                                              7.378
                                                     25.831
 112
       7.122
              25.546 113
                                 26.112 117
                                                     26.252
       7.504
              25.972 116
                           7.629
 115
       7.877
              26.391 119
                           8.000
                                 26.530 120
                                              8.122
 118
                                 26.942 123
              26.805 122
                           8.362
       8.242
```

124 8.599 27.213 125 27.347 126 8.716 8.833 27,481 127 8.948 27,747 129 27.614 128 9.062 27 879 9.176 130 9.288 28.010 131 9.400 28.141 132 9.510 28.271 133 9 620 28 400 134 10 123 28 982 135 10.618 29.553 136 11.104 30.112 137 11.583 30.660 138 12.055 31.197 139 12 518 31 722 140 12.973 32 236 141 13.420 32,739 142 13.860 33 230 143 7.391 16 948 144 7.482 17.702 145 7.545 18 460 146 7.575 19.222 147 7.567 19 989 148 7.515 20.764 149 7.415 21.547 150 7.260 22,341 151 7.046 23,145 152 6.767 23.962 153 5.758 12.569 154 6.387 13.644 155 6.857 14.736 156 7.186 15.840 157 6.548 24.520 158 7.008 24.296 159 7.127 24.461 160 6.855 24.945 161 7.363 24.789 162 7.479 24.951 163 7.265 25.413 164 7.710 25.273 165 7.825 25,432 166 7.678 25.883 167 8.051 25.748 168 25.905 8.162 169 8.273 26.060 170 8.090 26.373 171 8.493 26.369 172 8.602 26.521 173 8.443 26.870 174 8.816 26.824 175 8.923 26.973 176 9.028 27.122 177 27.270 9.132 178 9.236 27.417 179 9.203 27.718 180 9.441 27,707 181 9.543 27.851 182 9.643 27.994 183 9.743 28.136 184 28.277 185 9.842 10.336 28 872 186 10.822 29 456 187 11.300 30.029 188 30.590 189 11.770 12 233 31.141 190 12.688 31.680 191 13.135 32,208 192 13.574 32,724 193 14.006 33,230 194 7.861 16.544 195 7.950 17,287 196 8.014 18.031 197 8.048 18.778 198 8.047 19.530 199 8.006 20.287 200 7.918 21.051 201 7.779 21.824 202 7.584 22.607 203 7.327 23,400 204 7.435 23.587 205 6.146 12.232 206 13.285 207 6.806 7.300 14.359 208 15.448 209 7.646 7.541 23.773 210 7.647 23.958 211 7.752 24.141 212 7.856 24.323 213 7.960 24.504 214 8.063 24.683 215 8.165 24.861 216 8.267 25.038 217 8.368 25.214 218 25.388 219 25 561 8.468 8.567 220 8.666 25,732 221 8.764 25.903 222 8.862 26.072 223 26 240 224 8.958 9.054 26 406 225 9 150 26 572 226 26.898 228 9.244 26,736 227 9.338 27.060 9.431 229 9.524 27,220 230 9.616 27,379 231 9.707 27.536 232 9.797 27 693 233 9.887 27 847 234 9 976 28 001 235 10.064 28.154 236 10.549 28.762 237 11.027 29 359 238 11 497 29 945 239 11.958 30.520 240 12.413 31.084 241 12.859 31.637 242 13.298 32.179 243 13.729 32,710 14.152 244 33 230 245 8 334 16.137 246 8.420 16 869 247 8.484 17.602 248 8 521 18 335 249 8.526 19.072 250 8.494 19.813 251 8.418 20.559 252 8 294 21 312 253 8.117 22,074 254 7.881 22 845 255 7.974 23.052 256 7.945 23,494 257 6.530 11.897 258 7.224 12.927 259 8.115 14.355 260 8.108 15.054 261 8.160 23,460 262 8.253 23.662 263 8.344 23.863 264 8.435 24.061 265 8.526 24.258 266 8.615 24.454 267 8.705 24.648 268 8.793 24.840 269 8.881 25.031 270 8.969 25.220 271 9.055 25,408 272 9.142 25 594 273 9 227 25.778 274 9.313 25.961 275 9.397 26.142 276 9.481 26.322 277 9.564 26,500 278 9.647 26.676 279 9.729 26.851 280 9.811 27.024 281 9.892 27,196 282 9.972 27.366 283 10.052 27.534 284 10.131 27.701 285 10.210 27.866 286 10.490 28,442 287 10.764 28.651 288 11.233 29.261 289 11.694 29.861 290 12.147 30.450 291 12.593 31.027 292 13.031 31.594 293 13.462 32.150 294 13.884 32.696 295 14.300 33.230 296 8.810 15.728 297 8.892 16.450 298 8.955 17.171 299 8.994 17.892 300 9.004 18.615 301 8.979 19.340 302 8.914 20.070 303 8.804 20.804 304 8.643 21.546 305 8.426 22.296 306 8.507 22.522 307 8.588 22,746 308 8.668 22,968 309 6.911 11.565 310 7.641 12.570 311 8.189 13.603 312 8.572 14.658 313 8.747 23.189 314 8 826 23,407 315 8 905 23.624 316 8.983 23.838 317 9.061 24.051 318 9.138 24.262 319 9.214 24.471 320 9.291 24.678 321 9.366 24.883 322 9.442 25.086 323 9.516 25.288 324 9.591 25.487 325 9.664 25.685 326 9.738 25.880 327 9.811 26.074 328 9.883 26.266 329 9.955 26.455 330 10.026 26.643 331 10.097 26.830 332 10.168 27.014 333 10.238 27.196 334 10.307 27.376 335 10.376 27.555 336 10.445 27,731 337 10.513 27.906 338 10.980 28.540 339 11.440 29.164 340 11.893 29.777 341 12.337 30.379 342 12.775 30.971 343 13.204 31.551 344 13.626 32.122 345 14.041 32.681 14.448 33.230 347 9.290 15.316 348 9.367 16.029 349 9.428 16.740 350 9.468 17.450 351 9.342 18.400 352 9.462 18.870 353 9.407 19.583 354 9.309 20.301 355 9.164 21.024 356 8.965 21.753 357 9.034 21.998 358 22.241 359 22.482 360 9.101 9.169 9.236 22.721 361 7.288 11.235 362 8.056 12.214 363 13,225 8.633 9.039 14.261 365 22.957 366 364 9.303 9.369 23.191 9.435 23.423 368 9.501 23.653 369 23.880 9.567

```
9.696 24.329 372
                                                9.760 24.549
370
     9.631
            24.106 371
                           9.888
                                  24.984 375
                                                9.951
                                                       25.199
373
      9.824
             24.768 374
     10.014
              25,411 377
                           10.076
                                   25.620 378
                                                10.138
                                                        25.828
376
              26.033 380
                           10.257
                                   26.267 381
                                                 10.322
                                                         26,437
     10.200
379
382
     10,383
              26,636 383
                           10.443
                                   26.833 384
                                                10.503
                                                        27.027
              27.219 386
                           10.622
                                   27.409 387
                                                 10.680
                                                         27.596
385
     10.562
     10.739
                                   28.429 390
                                                11.649
                                                         29.066
388
              27,782 389
                           11.197
                           12.528
                                   30.308 393
                                                12.957
                                                         30.914
391
              29,692, 392
      12.092
                                   32.093 396
                                                14.198
                                                        32.667
394
     13.378
              31,508 395
                           13,792
                                   14,900 399
                                                9.752
                                                        15.802
397
      14.597
              33 230 398
                           9.774
400
                                  17.007 402
                                                9.956
                                                       17.705
      9.902
              16.308 401
                           9.941
      9.943
                           9 896
                                  19.101 405
                                                9.809
                                                       19.802
403
              18 402 404
                                                9.553
                                                       21.481
406
             20 506 407
                           9.497
                                  21.217 408
      9.678
             21,742,410
                           9 664
                                  22 001 411
                                                9.719
                                                       22.258
400
      9.609
                                                       11.860
                           7.663
                                  10 908 414
                                                8.469
412
      9.774
             22.512 413
415
      9.078
              12.847 416
                           9.507
                                  13.863 417
                                                9.828
                                                       22,763
418
      9.883
             23.012 419
                           9.937
                                  23,259 420
                                                9 991
                                                       23.503
                                   23,983 423
421
      10.044
              23.744 422
                           10.098
                                                10.151
                                                        24.219
424
      10.204
              24.453 425
                           10.256
                                   24.684 426
                                                 10.309
                                                         24 913
427
      10.361
              25.139 428
                           10.412
                                   25.363 429
                                                 10.464
                                                         25.584
430
      10.515
              25,803 431
                           10.566
                                   26.019 432
                                                 10.617
                                                         26 233
433
      10.668
              26.444 434
                           10.718
                                   26.652 435
                                                 10.768
                                                         26.858
436
      10.818
              27.062 437
                           10.867
                                   27.263 438
                                                 10.917
                                                         27.461
439
      10.966
              27.657 440
                           11.415
                                   28.318 441
                                                 11.858
                                                         28.968
442
      12.293
              29.608 443
                           12.720
                                    30.237 444
                                                 13.141
                                                         30.857
445
      13.553
              31.465 446
                           13.959
                                    32.064 447
                                                 14.357
                                                         32,652
448
      14.747
              33.230 449
                           10.262
                                    14.482 450
                                                 10.324
                                                         15.182
451
      10.377
              15.876 452
                           10.414
                                    16.565 453
                                                 10.431
                                                         17.252
454
      10.422
              17.936 455
                           10.381
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628	11.688	23.225 629	11.700	23.514 630	11.712	23.798
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640	11.841	26.437 641	11.855	26.680 642	11.869	26.919
643	11.884	27.155 644	12.298	27.869 645	12.705	28.573
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664		19.335 665	12.045		12.044	20.024
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817 820 823 826 829 832 835 838 841 844 847	13.581 13.430 13.337 13.251 13.170 10.544 13.322 12.972 12.982 12.922 12.867 12.818	16.560 815 17.960 818 19.135 821 20.266 824 21.351 827 8.377 830 10.619 833 23.157 836 24.024 839 25.818 845 26.648 848	13.494 13.398 13.308 13.223 13.144 11.723 13.094 13.025 12.961 12.903 12.850 13.197	17.152 816 18.357 819 19.517 822 20.632 825 21.702 828 9.063 831 22.391 834 23.386 837 24.336 840 25.240 843 26.100 846 27.415 849	13.462 13.367 13.279 13.196 13.119 12.643 13.071 13.003 12.941 12.885 12.834 13.568	17.558 18.749 19.894 20.994 22.049 9.812 22.727 23.707 24.642 25.532 26.376 28.174
817 820 823 826 829 832 835 838 841 844 847	13.581 13.430 13.337 13.251 13.170 10.544 13.322 12.972 12.982 12.922 12.867 12.818 13.933	16.560 815 17.960 818 19.135 821 20.266 824 21.351 827 8.377 830 10.619 833 23.157 836 24.924 839 24.944 842 25.818 845 26.648 848 28.923 851	13.494 13.398 13.308 13.223 13.144 11.723 13.094 13.025 12.961 12.903 12.850 13.197 14.291	17.152 816 18.357 819 19.517 822 20.632 825 21.702 828 9.063 831 22.391 834 23.386 837 24.336 840 25.240 843 26.100 846 27.415 849 29.663 852	13.462 13.367 13.279 13.196 13.119 12.643 13.071 13.003 12.941 12.885 12.834 13.568 14.643	17.558 18.749 19.894 20.994 22.049 9.812 22.727 23.707 24.642 25.532 26.376 28.174 30.395
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1612	18.454	33.230 1613	20.577	8.489 1614	20.978	8.087
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	22.864	6.625 1622		6.322 1623	23.736	6.000
1624	20.618	9.296 1625	20.476	9.853 1626	20.823	9.480
1627	19.969	10.878 1628	19.817	11.515 1629	19.668	12.142
1630	19.522	12.759 1631 14.549 1634	19.377	13.365 1632	19.236	13.962
1633 1636	19.096 18.692	16.250 1637	18.959	15.126 1635 16.796 1638	18.825	15.693
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1642	18.080	19.295 1643	17.835	19.868 1644	18.068	18.884
1645	17.611	20.813 1646	17.503	21.270 1647	17.722	20.345
1648	17.294	22.154 1649	17.193	22.581 1650	17.397 17.094	21.717 22.998
1651	16.998	23.406 1652	16.905	23.803 1653	16.813	24.190
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1657	17.406	27.511 1658	17.623	28.480 1659	17.183	29.443
1660	18.040	30.399 1661	18.241	31.349 1662	18.436	32.293
1663	18.626	33.230 1664	20.783	8.708 1665	21.161	8.320
1666	21.534	7.936 1667	21.887	7.696 1668	22.250	7.448
1669	22.627	7.189 1670	20.978	8.916 1671	20.317	10.512
1672	23.023	6.917 1673	23.440	6.630 1674	23.883	6.325
1675	24.356	6.000 1676	21.162	9.114 1677	20.659	10.152
1678	20.994	9.799 1679	21.322	9.451 1680	20.161	11.162
1681	20.007	11.801 1682	19.856	12.430 1683	19.707	13.048
1684	19.560	13.656 1685	19.417	14.254 1686	19.275	14.842
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1696	18.001	20,153 1697	17.887	20.627 1698	17.776	21.091
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1732	21.890	8.526 1733	21.725	9.218 1734	21.958	8.648
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1756	17.936 17.619	21.375 1754 22.693 1757	17.828 17.518	21.825 1755 23.111 1758	17.722 17.420	20.915 22.264 23.518
1759	17.936 17.619 17.324	21.375 1754 22.693 1757 23.915 1760	17.828 17.518 17.232	21.825 1755 23.111 1758 24.301 1761	17.722 17.420 17.327	20.915 22.264 23.518 25.140
1759 1762	17.936 17.619 17.324 17.655	21.375 1754 22.693 1757 23.915 1760 26.327 1763	17.828 17.518 17.232 17.859	21.825 1755 23.111 1758 24.301 1761 27.331 1764	17.722 17.420 17.327 18.057	20.915 22.264 23.518 25.140 28.329
1759 1762 1765	17.936 17.619 17.324 17.655 18.251	21.375 1754 22.693 1757 23.915 1760 26.327 1763 29.321 1766	17.828 17.518 17.232 17.859 18.439	21.825 1755 23.111 1758 24.301 1761 27.331 1764 30.307 1767	17.722 17.420 17.327 18.057 18.622	20.915 22.264 23.518 25.140 28.329 31.287
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1759 1762 1765 1768 1771 1774 1777 1780 1783	17.936 17.619 17.324 17.655 18.251 18.800 22.181 23.319 24.161 25.626 21.563	21.375 1754 22.693 1757 23.915 1760 26.327 1763 29.321 1766 32.262 1769 8.176 1772 7.464 1775 6.932 1778 6.000 1781 9.899 1784	17.828 17.518 17.232 17.859 18.439 18.973 22.549 23.729 24.618 20.986 21.805	21.825 1755 23.111 1758 24.301 1761 27.331 1764 30.307 1767 33.230 1770 7.947 1773 7.205 1776 6.641 1779 10.812 1782 9.322 1785	17.722 17.420 17.327 18.057 18.622 21.820 22.927 20.666 25.105 21.300 22.026	20.915 22.264 23.518 25.140 28.329 31.287 8.400 7.710 11.136 6.331 10.493 8.767
1759 1762 1765 1768 1771 1774 1777 1780 1783 1786 1789 1792	17.936 17.619 17.324 17.655 18.251 18.800 22.181 23.319 24.161 25.626 21.563 26.276	21.375 1754 22.693 1757 23.915 1760 26.327 1763 29.321 1766 32.262 1769 8.176 1772 7.464 1775 6.932 1778 6.930 1781 9.899 1784 6.000 1787	17.828 17.518 17.232 17.859 18.439 18.973 22.549 23.729 24.618 20.986 21.805 26.935	21.825 1755 23.111 1758 24.301 1761 27.331 1764 27.331 1764 30.307 1767 33.230 1770 7.947 1773 7.205 1776 6.641 1779 10.812 1782 9.322 1785 6.000 1788	17.722 17.420 17.327 18.057 18.622 21.820 22.927 20.666 25.105 21.300 22.026 27.604	20.915 22.264 23.518 25.140 28.329 31.287 8.400 7.710 11.136 6.331 10.493 8.767 6.000
1759 1762 1765 1768 1771 1774 1777 1780 1783 1786 1789 1792 1795	17.936 17.619 17.324 17.655 18.251 18.800 22.181 23.319 24.161 25.626 21.563 26.276 28.283 21.820 20.194	21.375 1754 22.693 1757 23.915 1760 26.327 1763 29.321 1766 32.262 1769 8.176 1772 7.464 1775 6.932 1778 6.000 1781 9.899 1784 6.000 1787 6.000 1787	17.828 17.518 17.232 17.859 18.439 18.973 22.549 23.729 24.618 20.986 21.805 26.935 28.972	21.825 1755 23.111 1758 24.301 1761 27.331 1764 30.307 1767 33.230 1770 7.947 1773 7.205 1776 6.641 1779 10.812 1782 9.322 1785 6.000 1788 6.000 1791	17.722 17.420 17.327 18.057 18.622 21.820 22.927 20.666 25.105 21.300 22.026 27.604 29.670	20.915 22.264 23.518 25.140 28.329 31.287 8.400 7.710 11.136 6.331 10.493 8.767 6.000 6.000
1759 1762 1765 1768 1771 1774 1777 1780 1783 1786 1789 1792 1795 1798	17.936 17.619 17.324 17.655 18.251 18.800 22.181 23.319 24.161 25.626 21.563 26.276 28.283 21.820 20.194 19.747	21.375 1754 22.693 1757 23.915 1760 26.327 1763 29.321 1766 32.262 1769 8.176 1772 7.464 1775 6.092 1778 6.000 1781 9.899 1784 6.000 1787 6.000 1790 3.400 1793 13.060 1796 14.885 1799	17.828 17.518 17.232 17.859 18.439 18.973 22.549 23.729 24.618 20.986 21.805 26.935 26.935 20.506 20.042 19.603	21.825 1755 23.111 1758 24.301 1761 27.331 1764 30.307 1767 7.947 1773 7.205 1776 6.641 1779 10.812 1782 9.322 1785 6.000 1791 11.788 1794 13.679 1797 15.472 1800	17.722 17.420 17.327 18.057 18.622 21.820 22.927 20.666 25.105 21.300 22.026 27.604 29.670 20.349	20.915 22.264 23.518 25.140 28.329 31.287 8.400 7.710 11.136 6.331 10.493 8.767 6.000 6.000 12.429
1759 1762 1765 1768 1771 1774 1777 1780 1783 1786 1789 1792 1795 1798 1801	17.936 17.619 17.324 17.655 18.251 18.800 22.181 23.319 24.161 25.626 21.563 26.276 28.283 21.820 20.194 19.747 19.324	21.375 1754 22.693 1757 23.915 1760 26.327 1763 29.321 1766 32.262 1769 8.176 1772 7.464 1775 6.932 1778 6.000 1781 6.000 1787 6.000 1790 8.400 1793 13.060 1796 14.885 1799 16.613 1802	17.828 17.518 17.232 17.859 18.439 18.973 22.549 23.729 24.618 20.986 21.805 26.935 28.972 20.506 20.042 19.603 19.189	21.825 1755 23.111 1758 24.301 1761 27.331 1764 30.307 1767 33.230 1770 7.947 1773 7.205 1776 6.641 1779 10.812 1782 9.322 1785 6.000 1788 6.000 1791 11.788 1794 13.679 1797 15.472 1800 17.167 1803	17.722 17.420 17.327 18.057 18.622 21.820 22.927 20.666 25.105 22.026 27.604 29.670 20.349 19.893 19.462 19.056	20.915 22.264 23.518 25.140 28.329 31.287 8.400 7.710 11.136 6.331 10.493 8.600 6.000 12.429 14.288 16.048 17.710
1759 1762 1765 1768 1771 1774 1777 1780 1783 1786 1789 1792 1795 1798 1801 1804	17.936 17.619 17.324 17.655 18.251 18.800 22.181 23.319 24.161 25.626 21.563 26.276 28.283 21.820 20.194 19.747 19.324 18.926	21.375 1754 22.693 1757 23.915 1760 26.327 1763 29.321 1766 32.262 1769 8.176 1772 7.464 1775 6.932 1778 6.000 1781 9.899 1784 6.000 1787 6.000 1790 8.400 1793 13.060 1796 14.885 1799 16.613 1802 18.242 1805	17.828 17.518 17.232 17.859 18.439 23.729 24.618 20.986 20.986 20.042 19.603 19.603 19.603 19.189 18.799	21.825 1755 23.111 1758 24.301 1761 27.331 1764 30.307 1767 33.230 1770 7.947 1773 7.205 1776 6.641 1779 10.812 1782 9.322 1785 6.000 1788 6.000 1788 6.000 1791 11.788 1794 13.679 1797 15.472 1800 17.167 1803 18.763 1806	17.722 17.420 17.327 18.652 21.820 22.927 20.666 25.105 21.300 22.026 27.604 29.670 20.349 19.893 19.462 19.056 18.675	20.915 22.264 23.518 25.140 28.329 31.287 8.400 7.710 6.331 10.493 8.767 6.000 6.000 12.429 14.288 16.048 16.048 17.710 19.274
1759 1762 1765 1768 1771 1774 1777 1780 1783 1786 1789 1792 1795 1798 1801 1804 1807	17.936 17.619 17.324 17.655 18.251 18.800 22.181 23.319 24.161 25.626 21.563 26.276 28.283 21.820 20.194 19.747 19.324 18.926 18.553	21.375 1754 22.693 1757 23.915 1760 26.327 1763 29.321 1766 32.262 1769 8.176 1772 7.464 1775 6.932 1778 6.000 1781 9.899 1784 6.000 1787 6.000 1790 8.400 1793 13.060 1796 14.885 1799 16.613 1802 18.242 1805 19.773 1808	17.828 17.518 17.232 17.859 18.439 18.973 22.549 23.729 24.618 20.986 21.805 26.935 26.935 20.506 20.042 19.603 19.189 18.799 18.434	21.825 1755 23.111 1758 24.301 1761 27.331 1764 30.307 1767 33.230 1770 7.947 1773 7.205 1776 6.641 1779 10.812 1782 9.322 1785 6.000 1788 6.000 1791 11.788 1794 13.679 1797 15.472 1800 17.167 1803 18.763 1806 20.262 1809	17.722 17.420 17.327 18.057 18.622 21.820 22.927 20.666 20.666 21.300 22.026 27.604 29.670 20.349 19.893 19.462 19.056 18.675 18.318	20.915 22.264 23.514 25.5140 28.329 31.287 8.400 7.710 6.331 10.493 8.767 6.000 12.429 14.288 16.048 17.710 19.274 20.739
1759 1762 1765 1768 1771 1774 1777 1780 1783 1786 1789 1792 1795 1798 1801 1804 1807 1810	17.936 17.619 17.324 17.655 18.251 18.800 22.181 23.319 24.161 25.626 21.563 26.276 28.283 21.820 20.194 19.747 19.324 18.953 18.553 18.504	21.375 1754 22.693 1757 23.915 1760 26.327 1763 29.321 1766 32.262 1769 8.176 1772 7.464 1775 6.093 1778 6.000 1781 9.899 1784 6.000 1780 6.000 1790 14.885 1799 16.613 1802 18.242 1805 19.773 1808 21.206 1811	17.828 17.518 17.232 17.859 18.439 18.973 22.549 23.729 24.618 20.986 21.805 26.935 28.972 20.506 20.042 19.603 19.189 18.799 18.434 18.063	21.825 1755 23.111 1758 24.301 1761 27.331 1764 30.307 1767 33.230 1770 7.947 1773 7.205 1776 6.641 1779 10.812 1782 9.322 1785 6.000 1781 11.788 1794 13.679 1797 15.472 1800 17.167 1803 18.763 1806 20.262 1809 21.675 1812	17.722 17.420 17.327 18.057 18.622 21.820 22.927 20.666 27.604 29.670 20.349 19.893 19.462 19.056 18.675 18.318 17.986	20.915 22.264 23.518 25.140 28.329 31.287 8.400 7.710 11.136 6.331 10.493 8.767 6.000 12.429 14.288 16.048 17.710 19.274 20.739 22.107
1759 1762 1765 1768 1771 1774 1777 1780 1783 1786 1789 1792 1795 1798 1801 1804 1807 1810	17.936 17.619 17.324 17.655 18.251 18.800 22.181 23.319 24.161 25.626 21.563 26.276 28.283 21.820 20.194 19.747 19.324 18.926 18.553 18.204 17.880	21.375 1754 22.693 1757 23.915 1760 26.327 1763 29.321 1766 32.262 1769 8.176 1772 7.464 1775 6.092 1778 6.000 1781 9.899 1784 6.000 1787 6.000 1790 13.060 1790 14.885 1799 16.613 1802 18.242 1805 19.773 1808 21.206 1811 22.541 1814	17.828 17.518 17.232 17.859 18.439 18.973 22.549 23.729 24.618 20.986 21.805 26.935 28.972 20.506 20.042 19.603 19.189 18.799 18.434 18.063 17.778	21.825 1755 23.111 1758 24.301 1761 27.331 1764 30.307 1767 33.230 1770 7.947 1773 7.205 1776 6.641 1779 10.812 1782 9.322 1785 6.000 1781 11.788 1794 13.679 1797 15.472 1800 17.167 1803 18.763 1806 20.262 1809 21.675 1812 22.964 1815	17.722 17.420 17.327 18.057 18.622 21.820 22.927 20.666 25.105 21.300 22.026 27.604 29.670 20.349 19.893 19.462 19.056 18.675 18.318 17.986 17.678	20.915 22.264 23.518 25.140 28.329 31.287 8.400 7.710 11.136 6.331 10.493 8.767 6.000 6.000 12.429 14.288 16.048 17.710 19.274 20.739 22.107 23.376
1759 1762 1765 1768 1771 1774 1777 1780 1783 1786 1792 1795 1798 1801 1804 1807 1810 1813	17.936 17.619 17.324 17.655 18.251 18.800 22.181 23.319 24.161 25.626 21.563 26.276 28.283 21.820 20.194 19.747 19.324 18.926 18.553 18.204 17.880 17.581	21.375 1754 22.693 1757 23.915 1760 23.915 1760 32.262 1769 8.176 1772 7.464 1775 6.932 1778 6.000 1781 9.899 1784 6.000 1787 6.000 1790 8.400 1793 13.060 1796 14.885 1799 16.613 1802 18.242 1805 19.773 1808 21.206 1811 22.541 1814 23.778 1817	17.828 17.518 17.232 17.859 18.439 18.973 22.549 23.729 24.618 20.986 21.805 26.935 28.972 20.506 20.042 19.603 19.189 18.799 18.434 18.063 17.778 17.487	21.825 1755 23.111 1758 24.301 1761 27.331 1764 30.307 1767 33.230 1770 7.947 1773 7.205 1776 6.641 1779 10.812 1782 9.322 1785 6.000 1788 6.000 1791 11.788 1794 13.679 1797 15.472 1800 17.167 1803 18.763 1806 20.262 1809 21.675 1812 22.964 1815 24.168 1818	17.722 17.420 17.327 18.057 18.622 21.820 22.927 20.666 25.105 21.300 22.026 27.604 29.670 20.349 19.893 19.462 19.056 18.675 18.318 17.986 17.678 17.678	20.915 22.264 23.518 25.140 28.329 31.287 8.400 7.710 11.136 6.331 10.493 8.767 6.000 6.000 12.429 14.288 17.710 19.274 20.739 22.107 23.376 25.198
1759 1762 1765 1768 1771 1774 1777 1780 1783 1786 1789 1792 1795 1798 1801 1804 1804 1807 1810 1813	17.936 17.619 17.324 17.655 18.251 18.800 22.181 23.319 24.161 25.626 21.563 26.276 28.283 21.820 20.194 19.324 19.324 17.880 17.880 17.581 17.891	21.375 1754 22.693 1757 23.915 1760 26.327 1763 29.321 1766 32.262 1769 8.176 1772 7.464 1775 6.092 1778 6.000 1781 9.899 1784 6.000 1787 6.000 1790 8.400 1793 13.060 1796 14.885 1799 14.885 1799 14.885 1799 14.895 1814 22.541 1814 23.778 1817 26.222 1820	17.828 17.518 17.232 17.859 18.439 18.973 22.549 23.729 24.618 20.986 21.805 26.935 26.935 20.506 20.042 19.603 19.189 18.799 18.434 18.063 17.778 17.487 18.086	21.825 1755 23.111 1758 24.301 1761 27.331 1764 30.307 1767 33.230 1770 7.947 1773 7.205 1776 6.641 1779 10.812 1782 9.322 1785 6.000 1788 6.000 1789 11.788 1794 13.679 1797 15.472 1800 20.262 1809 21.675 1812 22.964 1815 22.964 1815 22.946 1818	17.722 17.420 17.327 18.057 18.622 21.820 22.927 20.666 25.105 21.300 22.026 27.604 29.670 20.349 19.893 19.462 19.056 18.675 18.318 17.986 17.678 17.678	20.915 22.264 23.518 25.140 28.329 31.287 8.400 7.710 6.331 10.493 8.767 6.000 6.000 12.429 14.288 16.048 16.048 17.710 19.274 20.739 22.107 23.376 25.198 28.253
1759 1762 1765 1768 1771 1774 1777 1780 1783 1786 1789 1792 1795 1798 1801 1804 1807 1810 1813 1816 1819	17.936 17.619 17.324 17.655 18.251 18.800 22.181 23.319 24.161 25.626 21.563 26.276 28.283 21.820 20.194 19.747 19.324 18.926 18.553 18.204 17.581 17.581 17.691	21.375 1754 22.693 1757 23.915 1760 26.327 1763 29.321 1766 32.262 1769 8.176 1772 7.464 1775 6.932 1778 6.000 1781 9.899 1784 6.000 1780 6.000 1790 8.400 1793 13.060 1796 14.885 1799 16.613 1802 18.242 1805 19.773 1808 21.206 1811 22.541 1814 22.541 1814 26.222 1820 29.260 1823	17.828 17.518 17.232 17.859 18.439 18.973 22.549 23.729 24.618 20.986 21.805 26.935 26.935 20.506 20.042 19.603 19.189 18.799 18.434 18.063 17.778 17.487 18.086 18.640	21.825 1755 23.111 1758 24.301 1761 27.331 1764 30.307 1767 33.230 1770 7.947 1773 7.205 1776 6.641 1779 10.812 1782 9.322 1785 6.000 1781 6.000 1791 11.788 1794 13.679 1797 15.472 1800 17.167 1803 18.763 1806 20.262 1809 21.675 1812 22.964 1815 24.168 1818 24.168 1818 27.241 1821 30.261 1824	17.722 17.420 17.327 18.057 18.622 21.820 22.927 20.666 25.105 21.300 22.026 27.604 19.893 19.462 19.056 18.675 18.318 17.986 17.678 17.692 18.276 18.276	20.915 22.264 23.518 25.140 28.329 31.287 8.400 7.710 6.331 10.493 8.767 6.000 12.429 14.288 16.048 17.710 19.274 20.739 22.107 23.376 25.198 28.253 31.257
1759 1762 1765 1768 1771 1771 1774 1777 1780 1783 1795 1795 1795 1801 1801 1804 1810 1813 1816 1818 1819 1819 1822 1825	17.936 17.619 17.324 17.655 18.251 18.800 22.181 23.319 24.161 25.626 21.563 26.276 28.283 20.194 19.747 19.324 18.553 18.204 17.880 17.581 17.891 18.460 18.983	21.375 1754 22.693 1757 23.915 1760 26.327 1763 29.321 1766 32.262 1769 8.176 1772 7.464 1775 6.092 1778 6.000 1781 9.899 1784 6.000 1787 6.000 1790 14.885 1799 16.613 1802 1.206 1811 22.541 1814 23.778 1817 26.222 1820 29.260 1823 32.246 1826	17.828 17.518 17.232 17.859 18.439 18.973 22.549 23.729 24.618 20.986 21.805 26.935 26.935 20.506 20.042 19.603 19.189 18.799 18.434 18.063 17.778 17.487 18.086 19.148	21.825 1755 23.111 1758 24.301 1761 27.331 1764 30.307 1767 33.230 1770 7.947 1773 7.205 1776 6.641 1779 10.812 1782 9.322 1785 6.000 1781 11.788 1794 13.679 1797 15.472 1800 17.167 1803 18.763 1806 20.262 1809 21.675 1812 22.964 1815 24.168 1818 24.168 1818 27.241 1821 30.261 1824 33.230 1827	17.722 17.420 17.327 18.057 18.622 21.820 22.927 20.666 27.604 29.670 20.349 19.893 19.462 19.056 18.675 18.318 17.986 17.678 17.692 18.276	20.915 22.264 23.518 25.140 28.329 31.287 8.400 7.710 11.136 6.331 10.493 8.767 6.000 6.000 12.429 14.288 17.710 19.274 20.739 20.739 22.107 23.376 25.198 28.253 31.257 8.400
1759 1762 1765 1768 1771 1774 1777 1780 1783 1786 1795 1795 1801 1807 1801 1813 1816 1819 1812 1812 1822 1825	17.936 17.619 17.324 17.655 18.251 18.800 22.181 23.319 24.161 25.626 21.563 26.276 28.283 21.820 20.194 19.747 19.324 18.926 18.553 18.204 17.581 17.891 18.460 17.581 17.891 18.983 22.685	21.375 1754 22.693 1757 23.915 1760 26.327 1763 29.321 1766 32.262 1769 8.176 1772 6.000 1781 9.899 1784 6.000 1787 6.000 1790 8.400 1793 13.060 1796 14.885 1799 16.613 1802 18.242 1805 19.773 1808 21.206 1811 22.541 1814 23.778 1817 26.222 1820 29.260 1823 32.246 1826 8.179 1829	17.828 17.518 17.232 17.859 18.439 18.973 22.549 23.729 24.618 20.986 21.805 26.935 28.972 20.506 20.042 19.603 19.189 18.799 18.434 18.063 17.778 17.487 18.086 18.640 19.148 23.065	21.825 1755 23.111 1758 24.301 1761 27.331 1764 30.307 1767 33.230 1770 7.947 1773 7.205 1776 6.641 1779 10.812 1782 9.322 1785 6.000 1788 6.000 1791 11.788 1794 13.679 1797 15.472 1800 17.167 1803 18.763 1806 20.262 1809 21.675 1812 22.964 1815 24.168 1818 27.241 1821 30.261 1824 30.261 1824 30.261 1824 30.261 1824	17.722 17.420 17.327 18.057 18.622 21.820 22.927 20.666 25.105 21.300 22.026 27.604 29.670 20.349 19.893 19.462 19.056 18.675 18.318 17.986 17.678 17.692 18.276 18.814 22.315 23.456	20.915 22.264 23.518 25.140 28.329 31.287 8.400 7.710 11.136 6.331 10.493 6.000 6.000 12.429 14.288 16.048 17.710 19.274 20.739 22.107 23.376 25.198 28.253 31.257 8.400 7.717
1759 1762 1765 1768 1771 1774 1777 1780 1783 1786 1795 1795 1804 1807 1813 1816 1819 1822 1828 1828	17.936 17.619 17.324 17.655 18.251 18.800 22.181 23.319 24.161 25.626 21.563 26.276 28.283 21.820 20.194 19.747 19.324 18.926 18.553 18.204 17.880 17.881 17.891 18.460 18.983 22.685 23.863	21.375 1754 22.693 1757 23.915 1760 26.327 1763 29.321 1766 32.262 1769 8.176 1772 6.092 1778 6.000 1781 9.899 1784 6.000 1787 6.000 1790 8.400 1793 13.060 1796 14.885 1799 16.613 1802 18.242 1805 19.773 1808 21.206 1811 22.541 1814 23.778 1817 26.222 1820 29.260 1823 32.246 1826 31.79 1829 7.472 1832	17.828 17.518 17.232 17.859 18.439 18.973 22.549 23.729 24.618 20.986 21.805 26.935 26.935 20.506 20.042 19.603 19.189 18.799 18.434 18.063 17.778 17.487 18.086 18.640 19.148 23.065 24.290	21.825 1755 23.111 1758 24.301 1761 27.331 1764 30.307 1767 33.230 1770 7.947 1773 7.205 1776 6.641 1779 10.812 1782 9.322 1785 6.000 1788 6.000 1788 6.000 1791 11.788 1794 13.679 1797 15.472 1800 20.262 1809 21.675 1812 24.168 1818 27.241 1821 30.261 1824 33.230 1827 7.952 1830 7.213 1833	17.722 17.420 17.327 18.057 18.622 21.820 22.927 20.666 25.105 21.300 22.026 27.604 29.670 20.349 19.462 19.056 18.675 18.318 17.986 17.692 18.276 18.276 18.814 22.315 23.456 20.822	20.915 22.264 23.518 25.140 28.329 31.287 8.400 7.710 6.331 10.493 8.767 6.000 6.000 12.429 14.288 16.048 17.710 19.274 20.739 22.107 25.198 28.253 31.257 8.400 7.717 11.475
1759 1762 1765 1768 1771 1774 1777 1780 1780 1789 1792 1795 1798 1801 1813 1816 1819 1822 1825 1828 1828	17.936 17.619 17.324 17.655 18.251 18.800 22.181 23.319 24.161 25.626 21.563 26.276 28.283 21.820 20.194 19.324 17.880 17.880 17.881 17.891 18.460 18.983 22.685 23.863 24.741	21.375 1754 22.693 1757 23.915 1760 26.327 1763 29.321 1766 32.262 1769 8.176 1772 7.464 1775 6.092 1778 6.000 1781 9.899 1784 6.000 1787 6.000 1790 8.400 1793 13.060 1796 14.885 1799 14.885 1799 14.885 1799 21.206 1811 22.541 1814 22.541 1814 22.542 1805 19.773 1808 21.206 1811 22.541 1814 22.542 1826 8.179 1829 7.472 1832 6.939 1835	17.828 17.518 17.232 17.859 18.439 18.973 22.549 23.729 24.618 20.986 21.805 26.935 26.935 26.935 20.042 19.603 19.189 18.799 18.434 18.063 17.778 18.086 18.640 19.148 23.065 24.290 25.220	21.825 1755 23.111 1758 24.301 1761 30.307 1767 33.230 1770 7.947 1773 7.205 1776 6.641 1779 10.812 1782 9.322 1785 6.000 1788 6.000 1781 11.788 1794 13.679 1797 15.472 1800 20.262 1809 21.675 1812 22.964 1815 22.964 1815 22.964 1815 27.241 1821 30.261 1824 33.230 1827 7.213 1833 6.647 1836	17.722 17.420 17.327 18.057 18.622 21.820 22.927 20.666 25.105 21.300 22.026 27.604 29.670 20.349 19.893 19.462 19.056 18.675 18.318 17.678 17.678 17.678 17.678 18.276 18.276 18.276 20.822 25.730	20.915 22.264 23.518 25.140 28.329 31.287 8.400 7.710 6.331 10.493 8.767 6.000 6.000 12.429 14.288 16.048 17.710 19.274 20.739 22.107 23.376 25.198 28.253 31.257 8.400 7.717 8.400 7.717 8.400 7.717 8.400 7.717 8.400
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 6 5127.8363 7 5146.9969 8 5129.4176 9 5128.1809 10 5126.1001
 11 5149.0465 12 5146.0134 13 5129.8582 14 5128.0755 15 5127.7593
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521 5154.5604 522 5151.4257 523 5148.2899 524 5149.9499 525 5150.9305 526 5151.8019 527 5151.7840 528 5152.8394 529 5151.4909 530 5151.2760 531 5150.6725 532 5151.3036 533 5151.8858 534 5154.6417 535 5155.1713 536 5157.4458 537 5157.9574 538 5159.5185 539 5159.3765 540 5160.4612 541 5161.1287 542 5158.8509 543 5156.8675 544 5151.1262 545 5146.9312 546 5145.0518 547 5144.8280 548 5142.2557 549 5142.1546 550 5141.4252 551 5163.2964 552 5165.8674 553 5161.6766 554 5160.8456 555 5157.3456 556 5157.7517 557 5162.3461 558 5156.8113 559 5152.0888 560 5150.6446 561 5150.5056 562 5152.0755 563 5153.5937 564 5155.5448 565 5160.0378 566 5161.3862 567 5157.8357 568 5156.6686 569 5170.9631 570 5169.5058 571 5171.2778 572 5167.0851 573 5151.9277 574 5152.0411 575 5152.3624 576 5153.7896 577 5155.3421 578 5155.6345 579 5154.0703 580 5153.8706 581 5153.5582 582 5153.2986 583 5153.2692 584 5153.5780 585 5155.2870 586 5156.5196 587 5158.2894 588 5159.5062 589 5160.7046 590 5161.7168 591 5162.7985 592 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7832 664 5161 9071 665 5160 0159 666 5159.9451 667 5159.6931 668 5161.6586 669 5162.6890 670 5161.7295 671 5160.5016 672 5157.8286 673 5177.9343 674 5177.6645 675 5176.8842 676 5178.5058 677 5157.2120 678 5156.8726 679 5157.8009 680 5158.9589 681 5159.9110 682 5160.3478 683 5159.9507 684 5159.9029 685 5159.6290 686 5159.4185 687 5159.0497 688 5159.9123 689 5161.0420 690 5162.1668 691 5162.8087 692 5163.6396 693 5164.1678 694 5164.4105 695 5163.0058 696 5160.7170 697 5155.6054 698 5152.2507 699 5149.7092 700 5147.9200 701 5144.5275 702 5146.3018 703 5143.7431 704 5179.4565 705 5173.7385 706 5172.5075 707 5169.5661 708 5168.2008 709 5168.6473 710 5170.1796 711 5169.0094 712 5171.2117 713 5173.7564 714 5168.3241 715 5169.7825 716 5166.3985 717 5166.0967 718 5164.8350 719 5163.3368 720 5165.4667 721 5166.3451 722 5165.6015 723 5164.2891 724 5162.1300 725 5181.9609 726 5181.0224 727 5175.8816 728 5186.4725 729 5160.2127 730 5159.8271 731 5160.5128 732 5161.1481 733 5162.5174 734 5163.2306 735 5163.4776 736 5163.3604 737 5162.9979 738 5163.0623 739 5162.5051 740 5163.2162 741 5164.1120 742 5164.4428 743 5164.9609 744 5164.9943 745 5165.4012 746 5164.0078 747 5162.2166 748 5157.0280 749 5155.0849 750 5152.1724 751 5147,9996 752 5147,0013 753 5146,7197 754 5144,4825 755 5182,8489 756 5178.2962 757 5174.0608 758 5172.1499 759 5170.4761 760 5171.4760 761 5173.8486 762 5174.8771 763 5172.1207 764 5175.2560 765 5176.0110 766 5175.2520 767 5172.6787 768 5170.7080 769 5166.6791 770 5165.4038 771 5166.3869 772 5169.5583 773 5168.9753 774 5169.1340 775 5168.4927 776 5165.6891 777 5188.3167 778 5182.7207 779 5178.1534 780 5182.8738 781 5164.5568 782 5164.9776 783 5165.9995 784 5165.9547 785 5166.2281 786 5167.0775 787 5166.4882 788 5166.6110 789 5166.3419 790 5166.9645 791 5165.9531 792 5166.1435 793 5166.0615 794 5166.5448 795 5166.1238 796 5166.3553 797 5165.9042 798 5163.8982 799 5159.2315 800 5157.8078 801 5153.7833 802 5149.8057 803 5147.6986 804 5147.6584 805 5145.3736 806 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3356 5216.6667 3357 5224.9144 3358 5211.7149 3359 5218.3934
ZBED ARRAY: INP,SFCT (I2,F10.0); NODE, BEDROCK ELEVATION (5(I5,F10.0))
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5109.1080 479 5108.9113 480 5108.9008 481 5109.2517 482 5109.4824 483 5111.0573 484 5111.9566 485 5113.4489 486 5114.7766 487 5116.5878 488 5117.9197 489 5119.2861 490 5119.9940 491 5119.7009 492 5119.4646 493 5121.7466 494 5125.2326 495 5125.0203 496 5121.3819 497 5119.1925 498 5119.5380 499 5121.1915 500 5125.2314 501 5122.8792 502 5122.7222 503 5126.1240 504 5128.2836 505 5127.5235 506 5126.7033 507 5125.5901 508 5125.0545 509 5121.6923 510 5121.4037 511 5122.4366 512 5124.7564 513 5127.0963 514 5128.6538 515 5129.8339 516 5128.1703 517 5119.8870 518 5119.8977 519 5122.2349 520 5124.4237 521 5128.0542 522 5124.3269 523 5123.1174 524 5118.3164 525 5116.3532 526 5112.2552 527 5110.0300 528 5110.5000 529 5109.7169 530 5109.6563 531 5109.5122 532 5109.5764 533 5109.8290 534 5110.7003 535 5112.5729 536 5115.1733 537 5115.7492 538 5118.7251 539 5119.3062 540 5120.4520 541 5120.9437 542 5121.1596 543 5121.4331 544 5123.3924 545 5127.6660 546 5126.0324 547 5121.9859 548 5119.2924 549 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1976 5140.2767 1977 5141.0131 1978 5142.4594 1979 5141.8971 1980 5141.2000 1981 5141.2000 1982 5141.3000 1983 5132,2261 1984 5133,5709 1985 5136,0446 1986 5138.7159 1987 5140.1921 1988 5140.6097 1989 5143.7809 1990 5141.6393 1991 5183.0000 1992 5179.8300 1993 5181.7800 1994 5179.7900 1995 5182.7600 1996 5190.8800 1997 5200.3100 1998 5206.9600 1999 5207,5400 2000 5179.5100 2001 5181 0700 2002 5182 5200 2003 5182 0500 2004 5169 5800 2005 5171 7200 2006 5214.0400 2007 5217.8800 2008 5218.4300 2009 5220.3100 2010 5224.2500 2011 5225.2400 2012 5180.0500 2013 5140.5936 2014 5136.8719 2015 5139.4108 2016 5135.1526 2017 5176.4900 2018 5173.3600 2019 5171.0900 2020 5169.5700 2021 5167.0900 2022 5167.4124 2023 5164.8010 2024 5162.1204 2025 5160.1884 2026 5156.2435 2027 5153.2033 2028 5151.7151 2029 5150.3723 2030 5147.7285 2031 5145.2072 2032 5143.0764 2033 5140.4318 2034 5139.3441 2035 5141.1605 2036 5141.9253 2037 5141.0000 2038 5141.1000 2039 5141.2000 2040 5130.5072 2041 5133.2349 2042 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2242 5213.6000 2243 5218.5700 2244 5223.1300 2245 5181.0500 2246 5183.5900 2247 5185.7200 2248 5187.0300 2249 5226.7800 2250 5229.0600 2251 5231.0000 2252 5232.6200 2253 5234.8300 2254 5239.5700 2255 5190.2400 2256 5189.5400 2257 5190.9200 2258 5135.3477 2259 5135.9971 2260 5134.8890 2261 5138.6655 2262 5135.0913 2263 5136.1837 2264 5139.2358 2265 5138.3059 2266 5187.3600 2267 5189.1500 2268 5187.7000 2269 5188.8200 2270 5188.0200 2271 5188.5200 2272 5188.2500 2273 5132.2705 2274 5135.3367 2275 5177.5400 2276 5174.8600 2277 5173.1700 2278 5171.7600 2279 5169.5700 2280 5169.5109 2281 5168.1935 2282 5165.5406 2283 5162.6154 2284 5159.1389 2285 5155.0938 2286 5150.6233 2287 5147.9957 2288 5146.1052 2289 5142.9213 2290 5140.3643 2291 5140.2391 2292 5140.7121 2293 5138.7523 2294 5138.7901 2295 5140.9299 2296 5140.4970 2297 5139.6721 2298 5134.2383 2299 5130.6188 2300 5134.3431 2301 5199.2800 2302 5204.3100 2303 5207.7600 2304 5196.0300 2305 5209.4500 2306 5212.4600 2307 5217.1700 2308 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5129.6642 2453 5128.9000 2454 5135.9521 2455 5135.9073 2456 5139.2861 2457 5182.8700 2458 5185.3300 2459 5183.6600 2460 5184.4400 2461 5135.9118 2462 5136.1131 2463 5136.6415 2464 5130.3387 2465 5130.9159 2466 5135.2930 2467 5178.5700 2468 5176.2700 2469 5174.8000 2470 5173.5300 2471 5171.7100 2472 5170.6904 2473 5169.9542 2474 5168.6106 2475 5165.9181 2476 5162.4933 2477 5158.8588 2478 5153.1160 2479 5146.9552 2480 5141.5785 2481 5140.6505 2482 5141.3977 2483 5141.0923 2484 5139.9646 2485 5138.8242 2486 5138.3307 2487 5138.6863 2488 5139.2850 2489 5132.9591 2490 5213.4900 2491 5215.6100 2492 5219.9300 2493 5222.6100 2494 5224.7100 2495 5228.1000 2496 5206.4600 2497 5232.3300 2498 5235.9800 2499 5239.5700 2500 5242.2300 2501 5244.4600 2502 5249.4100 2503 5258.2600 2504 5263.8000 2505 5189.0800 2506 5187.4600 2507 5185.8100 2508 5184.5100 2509 5183.2600 2510 5182.0400 2511 5190.8300 2512 5129.0450 2513 5128.3733 2514 5136.5413 2515 5139.9851 2516 5179,0200 2517 5181.0000 2518 5178.9900 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2796 5140 2906 2797 5137 6939 2798 5138 2156 2799 5138 1270 2800 5137 5000 2801 5137.0000 2802 5136.5000 2803 5190.4100 2804 5207.7600 2805 5217.4900 2806 5222.9000 2807 5231.5800 2808 5235.8000 2809 5240.3500 2810 5244.9700 2811 5189.4800 2812 5250.8700 2813 5253.3900 2814 5256.8900 2815 5259.9100 2816 5260.7600 2817 5261.4800 2818 5178.9441 2819 5178.1363 2820 5176.7945 2821 5176.3789 2822 5132.5402 2823 5122.3654 2824 5123.1079 2825 5131.0067 2826 5132.9778 2827 5133.8173 2828 5132.7157 2829 5131.2876 2830 5130.7134 2831 5130.3875 2832 5130.4543 2833 5174.8156 2834 5172.9003 2835 5170.8190 2836 5169.3092 2837 5166.7114 2838 5162.7066 2839 5158.2983 2840 5152.4452 2841 5148.2129 2842 5146.0298 2843 5140.1000 2844 5138.8600 2845 5138.7100 2846 5138.8000 2847 5137.7315 2848 5135.0382 2849 5193.7000 2850 5197.9100 2851 5216.8700 2852 5223.1100 2853 5229.5300 2854 5233.2500 2855 5237.4800 2856 5245.0100 2857 5182.4700 2858 5251.0500 2859 5253.8500 2860 5257.4900 2861 5255.5800 2862 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3341 5189.7805 3342 5208.8253 3343 5216.2014 3344 5217.4568 3345 5184.9544
3346 5186.5548 3347 5182.2767 3348 5205.2564 3349 5199.6137 3350 5193.0807
3351 5213.4518 3352 5214.5486 3353 5195.1027 3354 5189.3706 3355 5208.2324
3356 5202.4761 3357 5210.3834 3358 5199.0197 3359 5205.7303
ZBASE ARRAY: INP,SFCT (I2,F10.0); NODE,AQUIFER BASE ELEVATION (5(I5,F10.0))
             2 5079.52 3 5079.81 4 5081.31 5 5082.46
    5079.06
             7 5082.68 8 5082.42 9 5082.17 10 5082.47
    5082.93
    5080.75 12 5081.68 13 5079.56 14 5079.62 15 5079.10
 11
                 5077.01 18 5077.83 19 5073.79 20 5075.43
     5075.19 17
 16
     5070.68 22 5072.77 23 5069.94 24 5075.85 25
                                                      5073.82
 21
                 5068.78 28
     5071.03 27
                             5067.23 29 5067.17 30
                                                      5068.17
 26
                 5080.28 33 5075.84 34
                                         5072.37 35
                                                      5068 30
 31
     5067.06 32
                 5066.03 38
 36
     5067.53 37
                             5065.96 39
                                         5066.34 40
                                                      5065.77
 41
     5083.40 42
                 5080.20 43
                             5075.43 44
                                         5072.07 45
                                                      5071.21
                 5065.96 48
                             5065.77 49
                                          5067.76 50
                                                      5066.42
 46
     5066.90 47
                             5078.72 54
                                          5077.00 55
                                                      5075.12
 51
     5086.68 52
                 5083.21 53
                             5066.34 59
                                          5066.02 60
                                                      5068.93
 56
     5070.39 57
                 5067.74 58
 61
     5068.90 62
                 5088.76 63
                             5086.52 64
                                          5084.89 65
                                                      5082.09
                                                      5066.77
                             5071.24 69
                                          5068.68
                                                  70
     5079.91 67
                 5074.15 68
  66
                             5068.42 74
 71
                 5069.49 73
                                          5090.57 75
                                                      5088.79
     5067.40
             72
                         78
                             5085.86 79
                                          5078.66 80
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 76
     5088.57 77
                 5086.70
 81
     5071.77 82
                 5069.98 83
                             5071.01 84
                                          5069.65 85
                                                      5071.09
     5068.90 87
                 5094.01 88
                             5092.09 89
                                          5090.97 90
                                                      5093.01
  86
                             5079.24 94
                                         5075.30 95 5073.32
  91
     5097.24 92
                 5086.21 93
     5074.87 97
                 5078.79 98 5074.11 99 5071.00 100 5072.71
 96
     5095.89 102 5096.91 103 5095.60 104 5097.89 105 5073.10
 101
                  5076.69 108 5079.43 109 5080.92 110
                                                        5081.89
      5074.55 107
 106
                               5084.23 114
                                            5083.99 115 5070.91
     5083.55 112
                  5083.56 113
 111
                               5072.56 119
                                            5073.22 120
                                                         5073.52
      5071.25 117
                  5072.20 118
 116
                               5082.31 124
                                            5082.57 125 5081.21
      5075.48 122
                  5077.18 123
 121
      5083.41 127
                  5084.30 128
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 126
      5092.43 132
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                               5104.04 139
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 136
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                                            5097.94 145
                                                         5089.22
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      5099.99 142
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                                            5100.18 155
                                                         5099.00
 151
                   5074.14 158
                               5074.08 159
                                            5075.86 160
                                                         5069 60
 156
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      5071.21 162 5070.74 163 5084.86 164
                                            5071.77 165
                                                         5073.06
 161
 166
      5072.65 167
                  5075.40 168
                               5075.16 169
                                            5075.51 170
                                                         5074.21
      5076.20 172
                  5077.15 173 5077.11 174
                                            5080.58 175
                                                         5071.71
 171
                               5086.56 179
                                            5086.57 180
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                   5087.99 178
 176
      5090.37 182 5092.48 183 5093.81 184
                                            5093.98 185
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  181
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      5100.33 192 5099.91 193 5099.98 194
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      5080.98 212 5076.78 213 5082.18 214 5083.21 215
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5154.15 3016 5153.27 3017 5152.39 3018 5150.89 3019 5148.14 3020 5141.02 3021 5138.29 3022 5136.88 3023 5136.48 3024 5136.78 3025 5160.06 3026 5162.18 3027 5163.11 3028 5164.68 3029 5170.34 3030 5172.21 3031 5174.92 3032 5178.00 3033 5185.00 3034 5181.00 3035 5187.00 3036 5191.00 3037 5197.00 3038 5198.93 3039 5137.87 3040 5137.05 3041 5127.58 3042 5129.43 3043 5129.35 3044 5125.02 3045 5127.86 3046 5115.84 3047 5120.11 3048 5119.61 3049 5115.97 3050 5118.69 3051 5122.22 3052 5117.57 3053 5159.39 3054 5158.86 3055 5158.43 3056 5157.29 3057 5155.33 3058 5153.15 3059 5151.80 3060 5150 46 3061 5146.23 3062 5139.67 3063 5137.02 3064 5137.09 3065 5136.87 3066 5161.71 3067 5162.70 3068 5164.04 3069 5165.50 3070 5169.21 3071 5170.05 3072 5174 96 3073 5182.00 3074 5184.00 3075 5178.04 3076 5187.00 3077 5194.00 3078 5199.00 3079 5133.64 3080 5135.31 3081 5128.85 3082 5129.32 3083 5124.19 3084 5128.21 3085 5117.30 3086 5119.16 3087 5117.25 3088 5119.00 3089 5117.62 3090 5116.92 3091 5120.62 3092 5161.07 3093 5160.38 3094 5160.09 3095 5159.92 3096 5157.78 3097 5154.40 3098 5152.26 3099 5151.05 3100 5148.38 3101 5142.04 3102 5138.40 3103 5137.37 3104 5138.11 3105 5162.11 3106 5163.49 3107 5164.87 3108 5166.21 3109 5169.33 3110 5170.76 3111 5183.00 3112 5176.00 3113 5185.00 3114 5172.76 3115 5192.00

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3136 5150.74 3137 5148.39 3138 5143.61 3139 5139.76 3140 5137.64
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3146 5171.27 3147 5182.00 3148 5178.00 3149 5169.00 3150 5188.00
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3186 5179.33 3187 5138.35 3188 5129.66 3189 5139.55 3190 5117.87
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3206 5146,20 3207 5143,43 3208 5140,72 3209 5163,93 3210 5165,16
3211 5166.27 3212 5166.49 3213 5166.52 3214 5175.04 3215 5166.49
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3231 5161.11 3232 5159.57 3233 5156.75 3234 5153.71 3235 5151.46
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 3306 5148.07 3307 5146.25 3308 5162.20 3309 5161.06 3310 5159.93
3311 5158.42 3312 5156.59 3313 5154.73 3314 5153.06 3315 5161.99
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3321 5152.65 3322 5151.78 3323 5150.52 3324 5150.16 3325 5160.76
 3326 5159.41 3327 5157.94 3328 5156.31 3329 5154.73 3330 5160.80
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 3346 5153.32 3347 5152.88 3348 5157.92 3349 5156.47 3350 5155.09
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 3356 5154.93 3357 5156.24 3358 5153.87 3359 5154.81
HYDK1 ARRAY: INP,SFCT (12,F10.0); NODE,HYDR. COND (AQ.1) (FT/DAY) 5(15,F10.0)
 1 1.0000
  1 1282.5900 2 1200.0000 3 1259.1100 4 1200.0000 5 1500.0000
  6 1200.0000 7 1375,7300 8 1500.0000 9 1334,2900 10 1200.0000
  11 1433.5200 12 1500.0000 13 1500.0000 14 1200.0000 15 1200.0000
  16 1200.0000 17 1500.0000 18 400.0000 19 1500.0000 20 1500.0000
  21 1346,6300 22 1200,0000 23 1096,7500 24 1337,2000 25 406,1300
  26 1500.0000 27 1500.0000 28 1500.0000 29 1500.0000 30 1257.0600
  31 1500,0000 32 1392,5800 33 605,5600 34 995,1000 35 1096,3200
  36 1479.2800 37 1500.0000 38 1500.0000 39 1218.7400 40 1500.0000
  41 690,0800 42 1086,3000 43 525,4500 44 80,0000 45 80,0000
  46 55.0000 47 1500.0000 48 1500.0000 49 416.1100 50 1462.9400
  51 400.0000 52 1419.7600 53 542.8100 54 80.0000 55 80.0000
  56 80,0000 57 55,0000 58 200,0000 59 1238,6400 60 540,9600
  61 1088.3900 62 497.5800 63 1411.7200 64 400.0000 65 80.0000
  66 80,0000 67 80,0000 68 55,0000 69 55,0000 70 200,0000
  71 400.0000 72 594.3200 73 858.4700 74 454.7900 75 1444.2600
  76 942.6100 77 30.0000 78 30.0000 79 30.0000 80 55.0000
  81 55,0000 82 55,0000 83 100,0000 84 400,0000 85 419,3000
  86 529.5100 87 510.0600 88 275.0000 89 865.4300 90 30.0000
  91 20.0000 92 35.0000 93 55.0000 94 55.0000 95 55.0000
      55,0000 97 50,0000 98 400,0000 99 553,9500 100 250,0000
  101 325,0000 102 275,0000 103 100,0000 104 70,0000 105 250,0000
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  111 250,0000 112 250,0000 113 250,0000 114 250,0000 115 150,0000
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  121 100,0000 122 100,0000 123 150,0000 124 200,0000 125 200,0000
  126 200.0000 127 200.0000 128 200.0000 129 200.0000 130 200.0000
  131 200.0000 132 200.0000 133 200.0000 134 228.8200 135 230.0000
  136 230.0000 137 230.0000 138 230.0000 139 230.0000 140 230.0000
  141 150.0000 142 150.0000 143 40.0000 144 15.0000 145 15.0000
  146 25,0000 147 55,0000 148 55,0000 149 55,0000 150 50,0000
  151 250.0000 152 250.0000 153 325.0000 154 275.0000 155 100.0000
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156 110.0000 157 250.0000 158 250.0000 159 250.0000 160 250.0000 161 250.0000 162 250.0000 163 250.0000 164 250,0000 165 250,0000 166 100.0000 167 150.0000 168 150.0000 169 125.0000 170 100.0000 171 100.0000 172 100.0000 173 100.0000 174 100.0000 175 215.0000 176 200.0000 177 200.0000 178 200.0000 179 200.0000 180 200.0000 181 200,0000 182 200,0000 183 200,0000 184 200,0000 185 228,7200 186 230,0000 187 230,0000 188 230,0000 189 230,0000 190 230,0000 191 230,0000 192 150,0000 193 150,0000 194 110,0000 195 20,0000 196 15.0000 197 15.0000 198 15.0000 199 25.0000 200 55.0000 201 90.0000 202 225.0000 203 250.0000 204 250.0000 205 325.0000 206 250,0000 207 100,0000 208 210,0000 209 250,0000 210 250,0000 211 250.0000 212 235.0700 213 100.0000 214 100.0000 215 100.0000 216 100.0000 217 100.0000 218 100.0000 219 125.0000 220 100.0000 221 100.0000 222 100.0000 223 100.0000 224 100.0000 225 100.0000 226 100.0000 227 100.0000 228 200.0000 229 200.0000 230 200.0000 231 200.0000 232 200.0000 233 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175.0000 467 190.0000 468 450.0000 469 250.0000 470 300.0000 471 340.0000 472 370.0000 473 380.0000 474 390.0000 475 400.0000 476 400.0000 477 550.0000 478 550.0000 479 400.0000 480 400.0000 481 400.0000 482 500.0000 483 500.0000 484 100.0000 485 100.0000 486 100.0000 487 100.0000 488 100.0000 489 100.0000 490 100.0000 491 100.0000 492 100.0000 493 100.0000 494 100.0000 495 230.0000 496 100 0000 497 100 0000 498 150 0000 499 150 0000 500 400 0000 501 400.0000 502 400.0000 503 300.0000 504 250.0000 505 65.0000 506 30.0000 507 30.0000 508 15,0000 509 50,0000 510 70,0000 511 100.0000 512 130.0000 513 160.0000 514 190.0000 515 220.0000 516 250,0000 517 100,0000 518 80,0000 519 110,0000 520 500,0000 521 300.0000 522 340.0000 523 370.0000 524 380.0000 525 390.0000 526 400.0000 527 550.0000 528 550.0000 529 550.0000 530 550.0000 531 400.0000 532 400.0000 533 400.0000 534 400.0000 535 100.0000 536 100.0000 537 100.0000 538 100.0000 539 100.0000 540 100.0000 541 100.0000 542 100.0000 543 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HYDK2 ARRAY: INP,SFCT (12,F10.0); NODE,HYDR. COND (AQ.2) (FT/DAY) 5(15,F10.0)
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2581	2.8100 2582	2.8100 2583	2.8100 2584	1.0000 2585	1.0000
2586	2.0000 2587	4.0000 2588	4.0000 2589	4.0000 2590	4.0000
2591	4.0000 2592	4.0000 2593	3.0000 2594	2.8000 2595	2.8100
2596	2.8100 2597	2.8100 2598	2.8100 2599	2.8100 2600	2.8100
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2616	2.0000 2617	2.0000 2618	2.0000 2619	2.0000 2620	0.5000
2621	1.0000 2622	1.0000 2623	1.0000 2624	1.0000 2625	1.0000
2626	1.0000 2627	2.8100 2628	2.8100 2629	2.8100 2630	2.8100
2631	1.0000 2632	2.8100 2633	2.8100 2634	2.8100 2635	2.8100
2636	2.8100 2637	2.8100 2638	2.8100 2639	1.0000 2640	1.5000
2641	4.0000 2642	4.0000 2643	4.0000 2644	4.0000 2645	4.0000
2646	4.0000 2647	4.0000 2648	2.8000 2649	2.8100 2650	2.8100
2651	2.8100 2652	2.8100 2653	2.8100 2654	2.0000 2655	2.8100
2656	2.8100 2657	2.8100 2658	2.8100 2659	0.2000 2660	2.5000
2661	3.0000 2662	3.5000 2663	1.5000 2664	1.5000 2665	2.0000
2666	2.0000 2667	0.5000 2668	2.0000 2669	2.0000 2670	2.0000
2671	2.0000 2672	2.0000 2673	2.0000 2674	0.5000 2675	1.0000
2676	1.0000 2677	1.0000 2678	1.0000 2679	1.0000 2680	1.0000
2681	2.8100 2682	2.8100 2683	2.8100 2684	2.8100 2685	2.8100
2686	2.8100 2687	2.8100 2688	2.8100 2689	2.8100 2690	1.5000
2691	4.0000 2692	4.0000 2693	4.0000 2694	4.0000 2695	4.0000
2696	4.0000 2697	4.0000 2698	3.0000 2699	2.8100 2700	2.8100
2701	2.8100 2702	2.8100 2703	2.8100 2704	2.8100 2705	2.8100
2706	2.8100 2707	2.8100 2708	2.8100 2709	0.2000 2710	2.5000
2711	3.0000 2712	3.0000 2713	1.5000 2714	1.5000 2715	1.5000
2716	2.0000 2717	0.5000 2718	2.0000 2719	2.0000 2720	2.0000
2721	2.0000 2717	2.0000 2723	2.0000 2713	1.5000 2725	1.5000
2726	1.5000 2727	1.5000 2728	1.5000 2729	1.5000 2723	2.8100
2731	2.8100 2732	2.8100 2733	2.8100 2734	2.8100 2735	
					2.8100
2736	2.8100 2737	2.8100 2738	2.8100 2739	4.0000 2740	4.0000
2741	4.0000 2742	4.0000 2743	4.0000 2744	4.0000 2745	4.0000
2746	3.0000 2747	2.8100 2748	2.8100 2749	2.8100 2750	2.8100
2751	2.8100 2752	2.8100 2753	2.8100 2754	2.8100 2755	2.8100
2756	2.8100 2757	0.3500 2758	0.2000 2759	2.5000 2760	3.0000
2761	3.5000 2762	1.5000 2763	1.5000 2764	1.5000 2765	0.5000
2766	2.0000 2767	2.0000 2768	2.0000 2769	2.0000 2770	2.0000
2771	2.0000 2772	4.0000 2773	4.0000 2774	4.0000 2775	4.0000
2776	4.0000 2777	2.8100 2778	2.8100 2779	2.8100 2780	2.8100
2781	2.8000 2782	2.8100 2783	2.8100 2784	2.8100 2785	2.8100
2786	4.0000 2787	4.0000 2788	4.0000 2789	4.0000 2790	4.0000
2791	4.0000 2792	4.0000 2793	3.0000 2794	2.8100 2795	2.8100
2796	2.8100 2797	2.8100 2798	2.8100 2799	2.8100 2793	2.8100
	2.8100 2797		1.0000 2804		
2801		2.8100 2803 3.5000 2808		0.2000 2805	0.2000
2806	2.0000 2807		1.5000 2809	1.5000 2810	1.5000
2811	1.5000 2812	2.0000 2813	2.0000 2814	2.0000 2815	2.0000
2816	2.0000 2817	2.0000 2818	4.0000 2819	4.0000 2820	4.0000
2821	4.0000 2822	2.8100 2823	2.8100 2824	2.8100 2825	2.8100
2826	2.8100 2827	2.8100 2828	2.8100 2829	2.8100 2830	2.8100
2831	2.8100 2832	2.8100 2833	4.0000 2834	4.0000 2835	4.0000
2836	4.0000 2837	4.0000 2838	4.0000 2839	4.0000 2840	2.8100
2841	2.8100 2842	2.8100 2843	2.8100 2844	2.8100 2845	2.8100
2846	2.8100 2847	2.8100 2848	2.8100 2849	1.0000 2850	0.3500
2851	0.2000 2852	0.2000 2853	2.0000 2854	3.5000 2855	1.5000
2856	1.5000 2857	4.0000 2858	1.5000 2859	1.5000 2860	1.5000
2861	1.5000 2862	1.5000 2863	2.0000 2864	4.0000 2865	4.0000
2866	4.0000 2867	2.8100 2868	2.8100 2869	2.8100 2870	2.8100
2871	2.8100 2872	2.8100 2873	2.8100 2874	2.8100 2875	2.8100
2876	2.8100 2877	2.8100 2878	2.8100 2879	4.0000 2880	4.0000
2881	4.0000 2882	4.0000 2883	4.0000 2884	4.0000 2885	4.0000
2886	4.0000 2887	4.0000 2888	4.0000 2889	4.0000 2890	4.0000
2891	2.8100 2892	2.8100 2893	2.8100 2894	4.0000 2895	1.0000
2896	0.3500 2897	0.2000 2898	0.5000 2899		
				2.0000 2900	1.5000
2901	1.5000 2902	4.0000 2903	1.5000 2904	1.5000 2905	1.5000
2906	1.5000 2907	1.5000 2908	1.5000 2909	4.0000 2910	4.0000
2911	2.8100 2912	2.8100 2913	2.8100 2914	2.8100 2915	2.8100
2916	2.8100 2917	2.8100 2918	2.8100 2919	2.8100 2920	2.8100
2921	2.8100 2922	2.8100 2923	2.8100 2924	4.0000 2925	4.0000
2926	4.0000 2927	4.0000 2928	4.0000 2929	4.0000 2930	4.0000
2931	4.0000 2932	4.0000 2933	4.0000 2934	4.0000 2935	2.8100

2936	2.8100 2937	2,8100 2938	4.0000 2939	4.0000 2940	0.5000
2941	0.3500 2942	0.3500 2943	0.5000 2944	2.0000 2945	3.0000
2946	4.0000 2947	1.5000 2948	1.5000 2949	1,5000 2950	1.5000
2951	1.5000 2952	3.0000 2953	4.0000 2954	2.8100 2955	2.8000
2956	2.8100 2957	2.8100 2958	2.8100 2959	2.8100 2960	2.8100
2961	2.8100 2962	2.8100 2963	2.8100 2964	2.8100 2965	2.8100
2966	2,8100 2967 4,0000 2972	2.8100 2968 4.0000 2973	2.8100 2969 4.0000 2974	4.0000 2970 4.0000 2975	4.0000 4.0000
2971 2976	4.0000 2972	4.0000 2978	4.0000 2974	4.0000 2973	2.8100
2981	2.8100 2982	4.0000 2978	4.0000 2984	3.0000 2985	0.5000
2986	0.5000 2987	0,5000 2988	1.5000 2989	1,5000 2990	4.0000
2991	1.5000 2992	1.5000 2993	1.5000 2994	1.5000 2995	1.5000
2996	1.5000 2997	2.8100 2998	2.8000 2999	2.8100 3000	2.8100
3001	2.8100 3002	2.8100 3003	2.8100 3004	2.8100 3005	2.8100
3006	2.8100 3007	2.8100 3008	2.8100 3009	2.8100 3010	2.8100 4.0000
3011 3016	2.8100 3012 4.0000 3017	4.0000 3013 4.0000 3018	4,0000 3014 4,0000 3019	4.0000 3015 2.8000 3020	4.0000
3021	4.0000 3017	4.0000 3013	4.0000 3024	2.8100 3025	4.0000
3026	4.0000 3027	4.0000 3028	0.5000 3029	0.5000 3030	0.5000
3031	0.5000 3032	1.5000 3033	1.5000 3034	1.5000 3035	1.5000
3036	1.5000 3037	1.5000 3038	1.5000 3039	2.8100 3040	2.8100
3041	2.8100 3042	2.8100 3043	2.8100 3044	2.8100 3045	2.8100
3046	2.8100 3047	2.8100 3048	2.8100 3049	2.8100 3050	2.8100
3051	2.8100 3052	2.8100 3053 4.0000 3058	4,0000 3054 4,0000 3059	4.0000 3055 4.0000 3060	4.0000 2.8000
3056 3061	4.0000 3057 2.8000 3062	4.0000 3058	4.0000 3039	1.5000 3065	2.8100
3066	3.0000 3067	4.0000 3068	3.0000 3069	0.5000 3070	0.5000
3071	0.5000 3072	0.5000 3073	0,5000 3074	1.5000 3075	0.5000
3076	1.5000 3077	1.5000 3078	1.5000 3079	2.8100 3080	2.8100
3081	2.8100 3082	2.8100 3083	2.8100 3084	2.8100 3085	2.8100
3086	2.8100 3087	2.8100 3088	2.8100 3089	2.8100 3090	2.8100
3091	2.8100 3092	3.0000 3093	4.0000 3094	4.0000 3095	4.0000
3096 3101	4.0000 3097 4.0000 3102	4.0000 3098 4.0000 3103	4.0000 3099 1.5000 3104	2.8000 3100 1.5000 3105	2.8000 3.0000
3106	1.5000 3102	0.5000 3103	0.5000 3109	0.5000 3110	0.5000
3111	0.5000 3112	0.5000 3113	1.5000 3114	0.5000 3115	1.5000
3116	1.5000 3117	2.8100 3118	2.8100 3119	2.8100 3120	2.8100
3121	2.8100 3122	2.8100 3123	2.8100 3124	2.8100 3125	2.8100
3126	2.8100 3127	2.8100 3128	2.8100 3129	3.0000 3130	4.0000
3131	4.0000 3132	4.0000 3133	4.0000 3134	4.0000 3135	4.0000
3136	0.5000 3137	0.5000 3138 1.5000 3143	2.8000 3139 1.5000 3144	4.0000 3140 0.5000 3145	1.5000 0.5000
3141 3146	1.5000 3142 0.5000 3147	0.5000 3143	0.5000 3149	0.5000 3143	0.5000
3151	0.5000 3152	0.5000 3153	2.8100 3154	2.8100 3155	2.8100
3156	2.8100 3157	2.8100 3158	2.8100 3159	2.8100 3160	2.8100
3161	2.8100 3162	2.8100 3163	2.8100 3164	1.5000 3165	0.5000
3166	0.5000 3167	0.5000 3168	0.5000 3169	0.5000 3170	0.5000
3171	0.5000 3172	0.5000 3173	0.5000 3174	0.5000 3175	1.0000
3176	1.5000 3177	1.5000 3178	0.5000 3179 0.5000 3184	0.5000 3180 0.5000 3185	0.5000
3181 3186	0.5000 3182 0.5000 3187	0.5000 3183 1.5000 3188	1.5000 3189	1.5000 3190	2.8100
3191	1.5000 3192	2.8100 3193	2.8100 3194	2.8100 3195	2.8100
3196	2.8100 3197	0.5000 3198	0.5000 3199	1.5000 3200	1.5000
3201	1.5000 3202	1.5000 3203	0.5000 3204	0.5000 3205	0.5000
3206	0.5000 3207	0.5000 3208	1.0000 3209	0.5000 3210	0.5000
3211	0.5000 3212	0.5000 3213	0.5000 3214	0.5000 3215	0.5000
3216	0.5000 3217 1.5000 3222	0.5000 3218 1.0000 3223	1.0000 3219 2.8100 3224	1.0000 3220 1.5000 3225	1.0000 1.5000
3221 3226	2.8100 3227	1.5000 3223	0.5000 3224	0.5000 3223	1.5000
3231	1.5000 3232	1.5000 3223	1.5000 3234	1.5000 3235	0.5000
3236	0.5000 3237	0.5000 3238	0.5000 3239	0.5000 3240	0.5000
3241	0.5000 3242	0.5000 3243	0.5000 3244	0.5000 3245	0.5000
3246	0.5000 3247	1.5000 3248	5.0000 3249	3.0000 3250	2.8100
3251	5.0000 3252	1.5000 3253	3.0000 3254	1.5000 3255	1.5000 0.5000
3256	1.5000 3257 0.5000 3262	0.5000 3258 1.5000 3263	0.5000 3259 2.8100 3264	0.5000 3260 1.5000 3265	1.5000
3261 3266	1.5000 3262	0.5000 3268	0.5000 3269	0.5000 3203	0.5000
3271	0.5000 3272	0.5000 3273	0.5000 3274	3.0000 3275	3.0000
3276	3.0000 3277	5.0000 3278	3.0000 3279	3.0000 3280	2.8100
3281	3.0000 3282	1,5000 3283	3.0000 3284	0.5000 3285	0.5000
3286	0.5000 3287	0.5000 3288	1.5000 3289	1.5000 3290	1.5000
3291	1.5000 3292	1.5000 3293	0.5000 3294	0.5000 3295	0.5000
3296	0.5000 3297	0.5000 3298 3.0000 3303	0.5000 3299 3.0000 3304	3,0000 3300 3,0000 3305	3.0000
3301 3306	3.0000 3302 3.0000 3307	3.0000 3303	0.5000 3304	0.5000 3310	0.5000
3311	1.5000 3307	1.5000 3313	1.5000 3314	1.5000 3315	0.5000
3316	0.5000 3317	0.5000 3318	0.5000 3319	0.5000 3320	1.5000
3321	3.0000 3322	3.0000 3323	3.0000 3324	3.0000 3325	0.5000
3326		1.5000 3328	1.5000 3329		1.5000
3331	1.5000 3332		1.5000 3334		1.5000
3336					1.5000 2.8100
3341	1.5000 3342	1.5000 3343	1.5000 3344	1.5000 5545	2.0100

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3346 3.0000 3347 3.0000 3348 1.5000 3349 1.5000 3350 1.5000
3351 1.5000 3352 1.5000 3353 1.5000 3354 3.0000 3355 1.5000
      1.5000 3357 1.5000 3358 1.5000 3359 1.5000
STORAGE COEFF. ARRAY: INP,SFCT (I2,F10.0); NODE, STORAGE (5(15,F10.0))
0 0.000000
INITIAL HEAD ARRAY: INP, SFCT (12,F10.0); NODE, HEAD (FT) (5(15,F10.0))
1 1.0000
  1 5096.6416 2 5096.9222 3 5096.0072 4 5097.2566 5 5096.1058
  6 5095,4489 7 5097,5197 8 5096,4103 9 5095,5517 10 5094,9426
 11 5098.1018 12 5097.4000 13 5095.7237 14 5095.0452 15 5094.5582
 16 5094.6151 17 5098.7487 18 5097.1177 19 5095.8701 20 5095.1945
 21 5094.7364 22 5094.2898 23 5094.3969 24 5099.6407 25 5097.5819
 26 5096.1891 27 5095.4000 28 5094.8695 29 5094.4950 30 5093.8055
 31 5094.0408 32 5100.7049 33 5098.4969 34 5096.6158 35 5095.5290
 36 5094.9972 37 5094.6841 38 5094.2342 39 5093.0204 40 5093.4629
 41 5101.2944 42 5099.5577 43 5097.1556 44 5095.7473 45 5095.2060
 46 5094.8395 47 5094.5189 48 5093.7911 49 5092.0584 50 5092.9724
 51 5102.0816 52 5100.5874 53 5098.1000 54 5096.1319 55 5095.3406
 56 5095.0299 57 5094.7682 58 5094.2201 59 5093.4537 60 5091.9879
 61 5092.42 62 5102.5952 63 5101.3349 64 5100.1215 65 5097.2687
 66 5096.4186 67 5095.2875 68 5094.9906 69 5094.7538 70 5093.69
 71 5092.8689 72 5091.7190 73 5091.9577 74 5103.0545 75 5101.6677
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 81 5094.9846 82 5094.5922 83 5093.6887 84 5092.4709 85 5091.2493
 86 5091.6292 87 5103.8159 88 5102.5153 89 5100.7280 90 5100.3641
 91 5101.4928 92 5099.6511 93 5098.3000 94 5095.9851 95 5095.2630
 96 5094.5672 97 5093.4982 98 5092.2104 99 5091.0390 100 5091.2684
101 5104.5460 102 5103.9183 103 5101.8840 104 5100.7657 105 5090.7376
106 5090.7118 107 5090.6264 108 5090.4775 109 5090.3755 110 5090.5518
111 5090.7060 112 5090.6289 113 5090.6759 114 5091.0854 115 5091.7825
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126 5103.3603 127 5104.3199 128 5105.1740 129 5105.2526 130 5106.2501
131 5106.9484 132 5107.4545 133 5107.8327 134 5108.7454 135 5108.6177
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141 5112.4271 142 5114.6155 143 5105.0312 144 5103.9725 145 5102.3584
146 5099.3070 147 5096.8488 148 5095.8335 149 5094.7474 150 5093.6215
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GHB CONDITIONS: NUMBS (15)
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  22043 5092.420
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  22052 5090.940
  22054 5111.900
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  23085 5139.600
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  23150 5139.100
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  23188 5140.150
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  24092 5139.100
  24122 5157.060
  24200 5138.170
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  25028 5180.400
  26010 5161.950
  26015 5144.520
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  26020 5149.170
  26040 5147.030
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   26076 5151.190
   26081 5148.000
   26083 5150.200
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26085 5179.380 26088 5142.910 26088 5142.910 26124 5154.310 26133 5146.140 26143 5174.730 26159 5201.040 26160 5143.900 26166 5151.440 26168 5155.510 26169 5148.990 26170 5140.770 26173 5147.710 27003 5097.700 27017 5148.100 27019 5148.530 27024 5125.800 27040 5120.800 27041 5113.700 27051 5128.300 27056 5098.400 27059 5127.300 27064 5093.690 27072 5095.800 27073 5097.900 27073 3097.900 27080 5120.000 27084 5136.400 35031 5174.210 35040 5165.080 35048 5216.780 35079 5197.980 35091 5182.200

## Appendix C Transient Calibration Input File

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SIMULATION OPTION IFLAG2, TOL, RELAX (I1,2F10.0) - (0=GAUSS & 1=PISOR)
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SIMULATION OPTION IFLAG3 (II) - (0=GWFLOW DATA & 1=GWTRAN DATA)
NUMNP, NUMEL, IBAND (315)
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		23.139 1148				
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1150	14.524	24.217 1151	14.467	24.563 1152	14.411	24.902
1153	14.357	25.234 1154	14.304	25.559 1155	14.252	25.878
1156	14.576	26.726 1157	14.894	27.567 1158	15.206	28.400
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1165	14.492	6,673 1166	15.774	7.146 1167		7.701
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1171	17.300	9.046 1172	17.160	9.733 1173	17.046	10.396
1174	16.954	11.035 1175	16.820	11.773 1176	16.810	12.248
1177	16.748	12.825 1178	16.686	13.384 1179	16.618	13.926
1180	16.670	14.417 1181	16.430	14.957 1182	16.338	15.462
1183	16.247	15.959 1184		16.450 1185		16.933
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1192	15.495	20.115 1193	15.418	20.541 1194	15.343	20.959
1195	15.270	21.371 1196	15.197	21.775 1197	15.126	22.172
1198	15.057	22.562 1199	14.989	22.945 1200	14.922	23.320
1201	14.857	23.689 1202	14.793	24.050 1203	14.730	24.404
1204	14.669	24.751 1205	14.610	25.090 1206	14.551	25.423
1207	14.494	25.748 1208	14.809	26.611 1209	15.118	27.465
1210	15.421	28.312 1211	15.718	29.151 1212	16.009	29.983
1213	16.293	30.806 1214	16.571	31.622 1215	16.844	32.430
1216	17.110	33.230 1217	16.223	6.764 1218	17.261	7.278
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1222	17.120	6.000 1223	17.654	9.288 1224	17.521	9.957
1225	17.411	10.600 1226	17.320	11.220 1227	17.242	11.818
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1231	16.934	14.024 1232	16.833	14.551 1233	16.733	15.070
1234	16.635	15.582 1235	16.538	16.087 1236	16.443	16.583
1237	16.350	17.073 1238	16.258	17.555 1239	16.168	18.029
1240	16.079	18.496 1241	15.991	18.955 1242	15.757	19.500
1243	15.821	19.852 1244	15.738	20.288 1245	15.657	20.718
1246	15.577	21.140 1247	15.499	21.554 1248	15.422	21.961
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1258	14.738	25.618 1259	15.044	26.494 1260	15.344	27.363
1261	15.638	28.224 1262	15.926	29.078 1263	16.208	29.923
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1276	17.761	10.790 1277	17.672	11.390 1278	17.593	11.968
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1288	16.612	17.236 1289	16.515	17.722 1290	16.420	18.201
1291	16.326	18.672 1292	16.234	19.136 1293	16.144	19.591
1294	16.055	20.039 1295	15.968	20.479 1296	15.882	20.911
1297	15.798	21.335 1298	15.716	21.752 1299	15.635	22.161
1300	15.556	22.562 1301	15.479	22.955 1302	15.403	23.340
1303	15.329	23.718 1304	15.256	24.087 1305		
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1306	15.116	24.803 1307	15.049	25.149 1308	14.983	25.488
1309	15.280	26.378 1310	15.570	27.261 1311	15.855	28.136
1312	16.134	29.003 1313	16.407	29.864 1314	16.675	30.716
1315	16.936	31.562 1316	17.191	32.400 1317	17.440	33.230
1318	19.080	6.648 1319	18.858	7.684 1320	18.646	8.396
1321	18.469	9.079 1322	19.663	6.472 1323	20.220	6.000
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1327		9.734 1325	18.200	10.363 1326	18.097	10.966
1327	18.008	11.545 1328	17.928	12.102 1329	17.850	12.638
1330	18.008 17.733	11.545 1328 13.201 1331	17.928 17.618	12.102 1329 13.757 1332	17.850 17.504	12.638 14.305
1330 1333	18.008 17.733 17.392	11.545 1328 13.201 1331 14.844 1334	17.928 17.618 17.282	12.102 1329 13.757 1332 15.376 1335	17.850 17.504 17.174	12.638 14.305 15.899
1330 1333 1336	18.008 17.733 17.392 17.067	11.545 1328 13.201 1331 14.844 1334 16.414 1337	17.928 17.618 17.282 16.962	12.102 1329 13.757 1332 15.376 1335 16.921 1338	17.850 17.504	12.638 14.305
1330 1333	18.008 17.733 17.392	11.545 1328 13.201 1331 14.844 1334	17.928 17.618 17.282	12.102 1329 13.757 1332 15.376 1335	17.850 17.504 17.174	12.638 14.305 15.899
1330 1333 1336	18.008 17.733 17.392 17.067	11.545 1328 13.201 1331 14.844 1334 16.414 1337	17.928 17.618 17.282 16.962	12.102 1329 13.757 1332 15.376 1335 16.921 1338	17.850 17.504 17.174 16.859	12.638 14.305 15.899 17.420
1330 1333 1336 1339 1342	18.008 17.733 17.392 17.067 16.757 16.463	11.545 1328 13.201 1331 14.844 1334 16.414 1337 17.911 1340 19.334 1343	17.928 17.618 17.282 16.962 16.692 16.369	12.102 1329 13.757 1332 15.376 1335 16.921 1338 18.190 1341 19.793 1344	17.850 17.504 17.174 16.859 16.560 16.276	12.638 14.305 15.899 17.420 18.868 20.243
1330 1333 1336 1339 1342 1345	18.008 17.733 17.392 17.067 16.757 16.463 16.185	11.545 1328 13.201 1331 14.844 1334 16.414 1337 17.911 1340 19.334 1343 20.685 1346	17.928 17.618 17.282 16.962 16.692 16.369 16.096	12.102 1329 13.757 1332 15.376 1335 16.921 1338 18.190 1341 19.793 1344 21.119 1347	17.850 17.504 17.174 16.859 16.560 16.276 16.008	12.638 14.305 15.899 17.420 18.868 20.243 21.545
1330 1333 1336 1339 1342 1345 1348	18.008 17.733 17.392 17.067 16.757 16.463 16.185 15.922	11.545 1328 13.201 1331 14.844 1334 16.414 1337 17.911 1340 19.334 1343 20.685 1346 21.963 1349	17.928 17.618 17.282 16.962 16.692 16.369 16.096 15.838	12.102 1329 13.757 1332 15.376 1335 16.921 1338 18.190 1341 19.793 1344 21.119 1347 22.372 1350	17.850 17.504 17.174 16.859 16.560 16.276 16.008 15.756	12.638 14.305 15.899 17.420 18.868 20.243 21.545 22.774
1330 1333 1336 1339 1342 1345 1348 1351	18.008 17.733 17.392 17.067 16.757 16.463 16.185 15.922 15.675	11.545 1328 13.201 1331 14.844 1334 16.414 1337 17.911 1340 19.334 1343 20.685 1346 21.963 1349 23.167 1352	17.928 17.618 17.282 16.962 16.692 16.369 16.096 15.838 15.597	12.102 1329 13.757 1332 15.376 1335 16.921 1338 18.190 1341 19.793 1344 21.119 1347 22.372 1350 23.553 1353	17.850 17.504 17.174 16.859 16.560 16.276 16.008 15.756 15.519	12.638 14.305 15.899 17.420 18.868 20.243 21.545 22.774 23.930
1330 1333 1336 1339 1342 1345 1348 1351 1354	18.008 17.733 17.392 17.067 16.757 16.463 16.185 15.922 15.675 15.444	11.545 1328 13.201 1331 14.844 1334 16.414 1337 17.911 1340 19.334 1343 20.685 1346 21.963 1349 23.167 1352 24.299 1355	17.928 17.618 17.282 16.962 16.692 16.369 16.096 15.838 15.597 15.370	12.102 1329 13.757 1332 15.376 1335 16.921 1338 18.190 1341 19.793 1344 21.119 1347 22.372 1350 23.553 1353 24.660 1356	17.850 17.504 17.174 16.859 16.560 16.276 16.008 15.756 15.519 15.299	12.638 14.305 15.899 17.420 18.868 20.243 21.545 22.774 23.930 25.013
1330 1333 1336 1339 1342 1345 1348 1351 1354 1357	18.008 17.733 17.392 17.067 16.757 16.463 16.185 15.922 15.675 15.444 15.228	11.545 1328 13.201 1331 14.844 1334 16.414 1337 17.911 1340 19.334 1343 20.685 1346 21.963 1349 23.167 1352 24.299 1355 25.357 1358	17.928 17.618 17.282 16.962 16.692 16.369 16.096 15.838 15.597 15.370 15.516	12.102 1329 13.757 1332 15.376 1335 16.921 1338 18.190 1341 19.793 1344 21.119 1347 22.372 1350 23.553 1353 24.660 1356 26.261 1359	17.850 17.504 17.174 16.859 16.560 16.276 16.008 15.756 15.519 15.299 15.798	12.638 14.305 15.899 17.420 18.868 20.243 21.545 22.774 23.930 25.013 27.158
1330 1333 1336 1339 1342 1345 1348 1351 1354	18.008 17.733 17.392 17.067 16.757 16.463 16.185 15.922 15.675 15.444	11.545 1328 13.201 1331 14.844 1334 16.414 1337 17.911 1340 19.334 1343 20.685 1346 21.963 1349 23.167 1352 24.299 1355	17.928 17.618 17.282 16.962 16.692 16.369 16.096 15.838 15.597 15.370	12.102 1329 13.757 1332 15.376 1335 16.921 1338 18.190 1341 19.793 1344 21.119 1347 22.372 1350 23.553 1353 24.660 1356	17.850 17.504 17.174 16.859 16.560 16.276 16.008 15.756 15.519 15.299	12.638 14.305 15.899 17.420 18.868 20.243 21.545 22.774 23.930 25.013
1330 1333 1336 1339 1342 1345 1348 1351 1354 1357	18.008 17.733 17.392 17.067 16.757 16.463 16.185 15.922 15.675 15.444 15.228	11.545 1328 13.201 1331 14.844 1334 16.414 1337 17.911 1340 19.334 1343 20.685 1346 21.963 1349 23.167 1352 24.299 1355 25.357 1358	17.928 17.618 17.282 16.962 16.692 16.369 16.096 15.838 15.597 15.370 15.516 16.344	12.102 1329 13.757 1332 15.376 1335 16.921 1338 18.190 1341 19.793 1344 22.372 1350 23.553 1353 24.660 1356 26.261 1359 28.929 1362	17.850 17.504 17.174 16.859 16.560 16.276 16.008 15.756 15.519 15.299 15.798 16.608	12.638 14.305 15.899 17.420 18.868 20.243 21.545 22.774 23.930 25.013 27.158 29.804
1330 1333 1336 1339 1342 1345 1348 1351 1354 1357 1360 1363	18.008 17.733 17.392 17.067 16.757 16.463 16.185 15.922 15.675 15.444 15.228 16.074 16.867	11.545 1328 13.201 1331 14.844 1334 16.414 1337 17.911 1340 19.334 1343 20.685 1346 21.963 1349 23.167 1352 24.299 1355 25.357 1358 28.047 1361 30.671 1364	17.928 17.618 17.282 16.962 16.692 16.369 16.096 15.838 15.597 15.370 15.516 16.344 17.119	12.102 1329 13.757 1335 15.376 1335 16.921 1338 18.190 1341 19.793 1344 21.119 1347 22.372 1350 23.553 1353 24.660 1356 26.261 1359 28.929 1362 31.532 1365	17.850 17.504 17.174 16.859 16.560 16.276 16.008 15.756 15.519 15.299 15.798 16.608 17.366	12.638 14.305 15.899 17.420 18.868 20.243 21.545 22.774 23.930 25.013 27.158 29.804 32.384
1330 1333 1336 1339 1342 1345 1348 1351 1354 1357 1360 1363 1366	18.008 17.733 17.392 17.067 16.757 16.463 16.185 15.922 15.675 15.444 15.228 16.074 16.867 17.607	11.545 1328 13.201 1331 14.844 1334 16.414 1337 17.911 1340 19.334 1343 20.685 1346 21.963 1349 23.167 1352 24.299 1355 25.357 1358 28.047 1364 30.671 1364 33.230 1367	17.928 17.618 17.282 16.962 16.369 16.096 15.838 15.597 15.370 15.516 16.344 17.119 19.382	12.102 1329 13.757 1332 15.376 1335 16.921 1338 18.190 1341 19.793 1344 21.119 1347 22.372 1350 23.553 1353 24.660 1356 26.261 1359 28.929 1362 31.532 1365 7.227 1368	17.850 17.504 17.174 16.859 16.560 16.276 16.008 15.751 15.299 16.608 17.366 19.144	12.638 14.305 15.899 17.420 18.868 20.243 21.545 22.774 23.930 25.013 27.158 29.804 32.384 7.949
1330 1333 1336 1339 1342 1345 1348 1351 1354 1357 1360 1363 1366 1369	18.008 17.733 17.392 17.067 16.757 16.463 16.185 15.922 15.675 15.444 15.228 16.074 16.867 17.607 18.944	11.545 1328 13.201 1331 14.844 1334 16.414 1337 17.911 1340 19.334 1343 20.685 1346 21.963 1349 23.167 1352 24.299 1355 25.357 1358 28.047 1361 30.671 1364 33.230 1367 8.641 1370	17.928 17.618 17.282 16.962 16.369 16.096 15.838 15.597 15.370 15.516 16.344 19.382 18.778	12.102 1329 13.757 1332 15.376 1335 16.921 1338 18.190 1341 19.793 1344 21.119 1347 22.372 1350 23.553 1353 24.660 1356 26.261 1359 28.929 1362 31.532 1365 7.227 1368 9.307 1371	17.850 17.504 17.174 16.859 16.560 16.276 16.008 15.756 15.519 15.299 15.798 16.608 17.366 19.144	12.638 14.305 15.899 17.420 18.868 20.243 21.545 22.774 23.930 25.013 27.158 29.804 32.384 7.949 6.767
1330 1333 1336 1339 1342 1345 1348 1351 1354 1357 1360 1363 1366 1369 1372	18.008 17.733 17.392 17.067 16.757 16.463 16.185 15.922 15.675 15.444 15.228 16.074 16.867 17.607 18.944 20.437	11.545 1328 13.201 1331 14.844 1334 16.414 1337 17.911 1340 19.334 1343 20.685 1346 21.963 1349 23.167 1352 24.299 1355 25.357 1358 28.047 1361 30.671 1364 33.230 1367 8.641 1370 6.306 1373	17.928 17.618 17.282 16.962 16.692 16.369 15.838 15.597 15.516 16.344 17.119 19.382 20.782	12.102 1329 13.757 1332 15.376 1335 16.921 1338 18.190 1341 19.793 1344 22.372 1350 23.553 1353 24.660 1356 26.261 1359 28.929 1362 31.532 1365 7.227 1368 9.307 1371 6.000 1374	17.850 17.504 17.174 16.859 16.560 16.276 16.008 15.756 15.519 15.299 15.798 16.608 17.366 19.144 19.908 18.637	12.638 14.305 15.899 17.420 18.868 20.243 21.545 22.774 23.930 25.013 27.158 29.804 32.384 7.949 6.767 9.937
1330 1333 1336 1339 1342 1345 1348 1351 1354 1357 1360 1363 1366 1369 1372	18.008 17.733 17.392 17.067 16.757 16.463 16.185 15.922 15.675 15.444 16.867 17.607 18.944 20.437 18.519	11.545 1328 13.201 1331 14.844 1334 16.414 1337 17.911 1340 19.334 1343 20.685 1346 21.963 1349 23.167 1352 24.299 1355 25.357 1358 28.047 1361 30.671 1364 33.230 1367 8.641 1370 6.306 1373 10.545 1376	17.928 17.618 17.282 16.962 16.692 16.369 16.096 15.838 15.597 15.370 15.370 16.344 17.119 19.382 18.778 20.782 18.419	12.102 1329 13.757 1332 15.376 1335 16.921 1338 18.190 1341 19.793 1344 21.119 1347 22.372 1350 23.553 1353 24.660 1356 26.261 1359 28.929 1362 31.532 1365 7.227 1368 9.307 1371 6.000 1374 11.127 1377	17.850 17.504 17.174 16.859 16.560 16.276 16.008 15.756 15.519 15.299 16.608 17.366 19.144 19.908 18.637 18.330	12.638 14.305 15.899 17.420 18.868 20.243 21.545 22.774 23.930 25.013 27.158 29.804 32.384 7.949 6.767 9.937 11.685
1330 1333 1336 1339 1342 1345 1348 1351 1354 1357 1360 1363 1366 1369 1372 1375	18.008 17.733 17.392 17.067 16.757 16.463 16.185 15.922 15.675 15.444 15.228 16.074 16.867 17.607 18.944 20.437 18.519	11.545 1328 13.201 1331 14.844 1334 16.414 1337 17.911 1340 19.334 1343 20.685 1349 23.167 1352 24.299 1355 25.357 1358 28.047 1361 30.671 1364 33.230 1367 8.641 1370 6.306 1373 10.545 1376 12.221 1379	17.928 17.618 17.282 16.962 16.969 16.096 15.838 15.597 15.370 15.516 16.344 19.382 18.778 20.782 18.419	12.102 1329 13.757 1335 15.376 1335 16.921 1338 18.190 1341 19.793 1344 21.119 1347 22.372 1350 23.553 1353 24.660 1356 26.261 1359 28.929 1362 31.532 1365 7.227 1368 9.307 1371 6.000 1374 11.127 1377 12.799 1380	17.850 17.504 17.174 16.859 16.560 16.276 15.078 15.798 16.608 17.366 19.144 19.908 18.637 18.330 18.001	12.638 14.305 15.899 17.420 18.868 20.243 21.545 22.774 23.930 25.013 27.158 29.804 7.949 6.767 9.937 11.685 13.369
1330 1333 1336 1339 1342 1345 1348 1351 1354 1357 1360 1363 1366 1369 1372	18.008 17.733 17.392 17.067 16.757 16.463 16.185 15.922 15.675 15.444 16.867 17.607 18.944 20.437 18.519	11.545 1328 13.201 1331 14.844 1334 16.414 1337 17.911 1340 19.334 1343 20.685 1346 21.963 1349 23.167 1352 24.299 1355 25.357 1358 28.047 1361 30.671 1364 33.230 1367 8.641 1370 6.306 1373 10.545 1376	17.928 17.618 17.282 16.962 16.692 16.369 16.096 15.838 15.597 15.370 15.370 16.344 17.119 19.382 18.778 20.782 18.419	12.102 1329 13.757 1332 15.376 1335 16.921 1338 18.190 1341 19.793 1344 21.119 1347 22.372 1350 23.553 1353 24.660 1356 26.261 1359 28.929 1362 31.532 1365 7.227 1368 9.307 1371 6.000 1374 11.127 1377	17.850 17.504 17.174 16.859 16.560 16.276 16.008 15.756 15.519 15.299 16.608 17.366 19.144 19.908 18.637 18.330	12.638 14.305 15.899 17.420 18.868 20.243 21.545 22.774 23.930 25.013 27.158 29.804 32.384 7.949 6.767 9.937 11.685
1330 1333 1336 1339 1342 1345 1351 1354 1357 1360 1363 1366 1369 1372 1375 1378	18.008 17.733 17.392 16.757 16.463 16.185 15.922 15.675 15.444 15.228 16.074 16.867 18.544 20.437 18.519 18.247 17.881	11.545 1328 13.201 1331 14.844 1334 16.414 1337 17.911 1340 19.334 1343 20.685 1346 21.963 1349 23.167 1352 24.299 1355 25.357 1358 28.047 1364 30.671 1364 33.230 1367 8.641 1370 6.306 1373 10.545 1376 12.221 1379 13.930 1382	17.928 17.618 17.282 16.962 16.969 16.096 15.838 15.597 15.370 15.516 16.344 17.119 19.382 18.778 20.782 18.419 18.123 17.762	12.102 1329 13.757 1332 15.376 1335 16.921 1338 18.190 1341 19.793 1344 21.119 1347 22.372 1350 23.553 1353 24.660 1356 26.261 1359 28.929 1362 31.532 1365 7.227 1368 9.307 1371 6.000 1374 11.127 1377 12.799 1380 14.483 1383	17.850 17.504 17.174 16.859 16.560 16.276 16.008 15.756 15.519 15.299 15.798 16.608 17.366 19.144 19.908 18.637 18.330 18.001 17.646	12.638 14.305 15.899 17.420 18.868 20.243 21.545 22.774 23.930 25.013 27.158 29.804 32.384 7.949 6.767 9.937 11.685 13.369 15.028
1330 1333 1336 1339 1342 1345 1348 1351 1354 1357 1360 1363 1366 1369 1372 1375	18.008 17.733 17.392 17.067 16.757 16.463 16.185 15.922 15.675 15.444 15.228 16.074 16.867 17.607 18.944 20.437 18.519	11.545 1328 13.201 1331 14.844 1334 16.414 1337 17.911 1340 19.334 1343 20.685 1349 23.167 1352 24.299 1355 25.357 1358 28.047 1361 30.671 1364 33.230 1367 8.641 1370 6.306 1373 10.545 1376 12.221 1379	17.928 17.618 17.282 16.962 16.969 16.096 15.838 15.597 15.370 15.516 16.344 19.382 18.778 20.782 18.419	12.102 1329 13.757 1335 15.376 1335 16.921 1338 18.190 1341 19.793 1344 21.119 1347 22.372 1350 23.553 1353 24.660 1356 26.261 1359 28.929 1362 31.532 1365 7.227 1368 9.307 1371 6.000 1374 11.127 1377 12.799 1380	17.850 17.504 17.174 16.859 16.560 16.276 15.078 15.798 16.608 17.366 19.144 19.908 18.637 18.330 18.001	12.638 14.305 15.899 17.420 18.868 20.243 21.545 22.774 23.930 25.013 27.158 29.804 7.949 6.767 9.937 11.685 13.369

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1798	19.747	14.885 1799	19.603	15.472 1800	19.462	16.048
1801	19.324	16.613 1802	19.189	17.167 1803	19.056	17.710
1804	18.926	18.242 1805	18.799	18.763 1806	18.675	19.274
1807	18.553	19.773 1808	18.434	20.262 1809	18.318	20.739
1810	18.204	21.206 1811	18.063	21.675 1812	17.986	22.107
1813	17.880	22.541 1814	17.778	22.964 1815	17.678	23.376
1816	17.581	23.778 1817	17.487	24.168 1818	17.692	25.198
1819	17.891	26.222 1820	18.086	27.241 1821	18.276	28.253
1822	18.460	29.260 1823	18.640	30.261 1824	18.814	31.257
1825	18.983	32.246 1826	19.148	33.230 1827	22.315	8.400
1828		8.179 1829				
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1831	23.863	7.472 1832	24.290	7.213 1833	20.822	11.475
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1837	21.132	11.168 1838	21.404	10.569 1839	21.655	9.987
1840	21.920	9.232 1841	22.091	8.882 1842	26.364	6.338
1843	27.007	6.341 1844	27.659	6.344 1845	28.320	6.347
1846	28.990	6.350 1847	29.670	6.354 1848	22.037	8.787
1849	20.661	12.128 1850	20.503	12.769 1851	20.347	13.399
1852	20.195	14.017 1853	20.045	14.625 1854	19.898	15.221
1855	19.754	15.806 1856	19.613	16.380 1857	19.475	16.942
1858	19.340	17.493 1859	19.167	18.202 1860	19.077	18.563
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1864	18.587	20.566 1865	18.471	21.039 1866	18.359	21.500
1867	18.249	21.951 1868	18.142	22.390 1869	18.038	22.818
1870	17.937	23.234 1871	17.838	23.640 1872	17.743	24.034
1873	17.939	25.078 1874	18.129	26.117 1875	18.315	27.150
1876	18.495	28.177 1877	18.671	29.199 1878	18.842	30.215
1879	19.007	31.226 1880	19.168	32.231 1881		
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1882	22.568	9.070 1883	22.814	8.400 1884	23.194	8.182

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2170	23.729	9.967 2171	23.401	10.170 2172	24.048	9.727
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2194	20.427	29.292 2195	20.719	31.512 2196	20.703	30.414
2197	20.913	33.787 2198	20.913	33.398 2199	20.933	31.557
2200	22.379	9.967 2201	22.855	10.473 2202	22.439	10.065
2203	22.794	10.421 2204	22.499	10.164 2205	22.732	10.365
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2209	21.487	12.626 2210	21.384	13.208 2211	21.283	13.784
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2215	20.907	16.018 2216	20.819	16.560 2217	20.733	17.095
2218	20.650	17.624 2219	20.570	18.146 2220	20.492	18.661
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2239	24.525	9.727 2240	24.848	9.450 2241	25.178	9.137
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2257	23.027	10.970 2258	20.382	28.207 2259	20.682	29.318
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2413	21.448	16.442 2414	21.394	16.964 2415	21.343	17.483
2416	21.294	17.998 2417	21.247	18.509 2418	21.203	19.016
2419	21.161	19.520 2420	21.100	19.802 2421	21.083	20.515
2422	21.047	21.008 2423	21.014	21,496 2424	20.982	21.981
2425	20.953	22,462 2426	20.926	22.939 2427	20.902	23.412
2428	20.879	23.882 2429	20.899	24.966 2430	24.014	11.366
2431	24.431	10.955 2432	24.854	10.556 2433	25.281	10.170
2434	25.612	9.967 2435	23.602	11.789 2436	25.948	9.727
2437	26.296	9.450 2438	26.664	9.137 2439	22.072	12.150
2440	27.162	9.137 2441	27.661	9.137 2442	28.162	9.137
			29.166		29.670	9.137
2443	28.663	9.137 2444				
2446	23.089	12.228 2447	22.981	12.231 2448	22.871	12.232
2449	22.760	12.229 2450	22.648	12.223 2451	23.197	12,222
2452	21.238	24.968 2453	21.549	26.066 2454	21.814	27.180
2455	21.951	29,446 2456	22.032	28.314 2457	22.189	12.170
2458	22.535	12.214 2459	22.306	12.188 2460	22.421	12.202
2461	21.988	31.779 2462	21.985	31.380 2463	22.203	29.471
2464	21.926	34.196 2465	21.926	33.820 2466	22.196	31.824
2467	22.013	12.691 2468	21.955	13.229 2469	21.900	13.764
2470	21.847	14.296 2471	21.796	14.826 2472	21.747	15.353
2473	21.700	15.877 2474	21.656	16.398 2475	21.613	16.917
		17.432 2477		17.945 2478	21.498	18.455
2476	21.573		21.535			
2479	21.464	18.963 2480	21.432	19.467 2481	21.402	19.969
2482	21.375	20.467 2483	21.349	20.963 2484	21.326	21.457
2485	21.304	21.947 2486	21.285	22.435 2487	21.220	23.065
2488	21.253	23,401 2489	21.200	24.365 2490	24.061	11.780
2491	24.473	11.359 2492	24.891	10.950 2493	25.313	10.554
						12.211
2494	25.740	10.170 2495	26.075	9.967 2496	23.655	
2497	26.419	9.727 2498	26.779	9.450 2499	27.261	9.450
2500	27.743	9.450 2501	28.225	9.450 2502	28.707	9.450
2503	29.189	9.450 2504	29.670	9.450 2505	23.136	12.670
2506	23.016	12.683 2507	22.894	12.694 2508	22.771	12.702
		12.707 2510	22.522	12.710 2511	23.256	12.653
2509	22.647					
2512	21.576	24.969 2513	21.866	26.072 2514	22.109	27.192
2515	22.305	28.332 2516	22.142	12.700 2517	22.396	12.709
2518	22.308	12.988 2519	22.327	30.655 2520	22.454	29.497
2521	22.091	34.263 2522	22.249	33.059 2523	22.404	31.868
2524	22.556	30.689 2525	22.255	34.330 2526	22.096	13.227
		13.753 2528	22.010	14.276 2529	21.970	14.798
2527	22.052					
2530	21.933	15.318 2531	21.897	15.837 2532	21.863	16.353
2533	21.832	16.868 2534	21.802	17.381 2535	21.774	17.892
2536	21.749	18.401 2537	21.725	18.908 2538	21.704	19.413
2539	21.684	19.917 2540	21.666	20.419 2541	21.651	20.919
2542	21.700	21.163 2543	21.626	21.913 2544	21.617	22.407
2545	21.609	22,900 2546	21.604	23.391 2547	21.600	23.880
				11.771 2550		11.352
2548	24.109	12.200 2549	24.516		24.928	
2551	25.346	10.945 2552	25.768	10.551 2553	26.194	10.170
2554	26.535	9.967 2555	23.709	12.641 2556	26.888	9.727
2557	27.356	9.727 2558	27.822	9.727 2559	28.286	9.727
2560	28.749	9.727 2561	29.210	9.727 2562	29.670	9.727
2563	23.316	13.091 2564	23.185	13.117 2565	23.052	13.140
2566	22.918	13.161 2567	22.783	13.178 2568	22.648	13.194
2569	22.511	13.206 2570	21.915	24.972 2571	22.183	26.078
2572	22.404	27.203 2573	22.578	28.350 2574	22.235	13.223
2575	22.374	13.216 2576	22.705	29.522 2577	22.434	33.114
2578	22.611	31.911 2579	22.784	30.723 2580	22.418	34.397
2581	22.418	34.003 2582	22.579	34.464 2583	22.740	34.530
2584	22.203	13.739 2585	22.173	14.254 2586	22.144	14.768
		15.282 2588	22.093	15.794 2589	22.070	16.306
2587	22.118					
2590	22.049	16.817 2591	22.031	17.327 2592	22.014	17.836
2593	21.999	18.345 2594	21.986	18.852 2595	21.975	19.359
2596	21.965	19.864 2597	21.958	20.369 2598	21.953	20.873
2599		21.376 2600	21.948	21.878 2601	21.948	22.380
2602		22.880 2603	21.955	23.380 2604	21.961	23.879
				12.189 2607	24.967	11.761
2605		12.628 2606	24.560			
2608		11.345 2609	25.797	10.940 2610		10.549
2611	26.644	10.170 2612	26.992	9.967 2613	23.764	13.077
2614	27.446	9.967 2615	27.896	9.967 2616	28.344	9.967
2617		9.967 2618	29.231	9.967 2619	29.670	9.967
2620		13.536 2621	23.234	13.570 2622		13.602
						13.682
2623			22.798	13.658 2625		
2626				24.974 2628	22.500	76 HX5
		13.703 2627	22.254			26.085
2629				28.368 2631		13.722

2632	22.955	29.548 2633	22.817	31.955 2634	23.012	30.757
2635	22.802	33.223 2636	23.022	31.999 2637	23.050	34.195
2638	23.256	34.530 2639	22.334	14.229 2640	22.317	14.736
2641	22.302	15.243 2642	22.288	15.750 2643		
					22.276	16.257
2644	22.267	16.765 2645	22.259	17.272 2646	22.253	17.780
2647	22.248	18.287 2648	22.246	18.795 2649	22.245	19.303
2650	22.246	19.811 2651	22.249	20.319 2652	22.254	20.827
	22.261					
2653		21.335 2654	22.269	21.844 2655	22.280	22.352
2656	22.292	22.861 2657	22.306	23.369 2658	22.322	23.878
2659	24.209	13.063 2660	24.604	12.616 2661	25.006	12.178
2662	25.414	11.752 2663	25.827	11.338 2664	26.244	10.936
2665	26.665	10.546 2666	27.090	10.170 2667	23.821	13.521
2668	27.531	10.170 2669	27.968	10.170 2670	28.400	10.170
2671	28.828	10.170 2672	29.251	10.170 2673	29.670	10.170
2674	23,440	13.988 2675	23.285	14.030 2676	23.128	14.069
2677	22.971	14.106 2678	22.813	14.140 2679	22.654	14.172
2680	22.495	14.202 2681	22.593	24.976 2682	22.817	26.091
2683	22.994	27.227 2684	23.123	28.386 2685	23.205	29.573
2686	23,239	30.791 2687	23.226	32.042 2688	23.522	34.210
2689	23,763	34.530 2690	22.489	14.702 2691	22,485	15.202
2692	22.483	15.704 2693	22.482	16.207 2694	22.483	16.711
2695	22.486	17.216 2696	22.491	17,722 2697	22.497	18.229
2698	22.505	18,737 2699	22.515	19.246 2700	22.527	19.757
		20.268 2702				
2701	22.540		22.555	20.780 2703	22.572	21.294
2704	22.591	21.809 2705	22.611	22.324 2706	22.633	22.841
2707	22.657	23.359 2708	22.683	23.878 2709	24.260	13.506
2710	24.718	12.938 2711	25.047	12.603 2712	25.449	12.167
				11.331 2715		
2713	25.857	11.743 2714	26.270		26.687	10.931
2716	27.108	10.544 2717	23.878	13.972 2718	27.545	10.541
2719	27.979	10.538 2720	28.408	10.536 2721	28.833	10.533
2722	29.254	10.531 2723	29.670	10.528 2724	23.504	14.447
2725	23.337	14.495 2726	23.169	14.541 2727	23.000	14.584
2728	22.830	14.626 2729	22.660	14.665 2730	22.932	24.979
2731	23.134	26.098 2732	23.288	27.239 2733	23.395	28.404
2734	23.454	29.598 2735	23.466	30.824 2736	23.698	32.037
2737	24.115	34.208 2738	24.264	34.530 2739	22.667	15.159
2740	22.676	15.656 2741	22.687	16.154 2742	22.699	16.655
2743	22.713	17.157 2744	22.729	17.662 2745	22.746	18.169
2746	22.765	18.678 2747	22.785	19.188 2748	22.807	19.701
2749	22.913	20.282 2750	22.857	20.733 2751	22.884	21.252
2752	22.912	21.773 2753	22.943	22.296 2754	22.975	22.821
2755	23.008	23.348 2756	23.043	23.878 2757	24.313	13.955
2758	24.697	13.490 2759	25.088	13.035 2760	25.485	12.590
2761	25.888	12.156 2762	26.297	11.734 2763	26.709	11.323
2764	27.126	10.926 2765	23.937	14.429 2766	27.560	10.921
2767	27.991	10.916 2768	28.417	10.911 2769	28.839	10.906
2770	29.670	10.896 2771	29.256	10.901 2772	23.568	14.912
2773	23.390	14.966 2774	23.210	15.017 2775	23.030	15.067
2776	22.849	15.114 2777	23.271	24.981 2778	23.450	26.105
2779	23.582	27.250 2780	23.666	28.422 2781	23.702	29.624
2782	23.917	30.818 2783	24.165	32.032 2784	24.404	34.206
2785	24.756	34.530 2786	22.869	15.605 2787	22.891	16.100
2788	22.915	16.597 2789	22.940	17.098 2790	22.966	17.601
2791	22.994	18.108 2792	23.024	18.617 2793	23.055	19.130
2794	23.087	19.645 2795	23.122	20.164 2796	23.157	20.685
				21.737 2799	23.274	
2797	23.195	21.210 2798	23.234			22.268
2800	23.316	22.801 2801	23.359	23.338 2802	23.405	23.878
2803	24.366	14.412 2804	24.744	13.939 2805	25.130	13.475
2806	25.522	13.021 2807	25.920	12.578 2808	26.324	12.146
2809	26.732	11.725 2810	27.144	11.316 2811	23.996	14.894
2812	27.630	11.318 2813	28.002	11.302 2814	28.425	11.295
2815	28.844	11.288 2816	29.259	11.281 2817	29.670	11.273
2818	23.634	15.384 2819	23.444	15.443 2820	23.253	15.499
2821	23.062	15.553 2822	23.609	24.984 2823	23.766	26.112
2824	23.895	27.530 2825	23.937	28.440 2826	24.132	29.617
2827	24.362	30.811 2828	24.625	32.027 2829	24.756	34.208
2830	25.241	34.530 2831	25.718	34.530 2832	26.188	34.530
2833	23.095	16.044 2834	23.129	16.538 2835	23.165	17.036
2836	23.203	17.539 2837	23.242	18.045 2838	23.282	18.556
2839	23.324	19.070 2840	23.367	19.588 2841	23.412	
						20.110
2842	23.458	20.637 2843	23.506	21.167 2844	23.555	21.701
2845	23.605	22.239 2846	23.708	22.757 2847	23.711	23.328
2848	23.766	23.878 2849	24.673	14.682 2850	24.793	14.395
2851	25.173	13.923 2852	25.559	13.460 2853	25.953	13.007
2854						
	26.351	12.565 2855	26.755	12.135 2856	27.163	11.716
		15.366 2858	27.591	11.707 2859	28.015	11.697
2857	24.057			11.688 2862	29.262	44 (80
	24.057 28.850	11.679 2861	28.434	11.000 2002	29.202	11.670
2857 2860	28.850	11.679 2861				11.670 15.926
2857 2860 2863	28.850 29.670	11.679 2861 11.661 2864	23.702	15.864 2865	23.500	15.926
2857 2860 2863 2866	28.850 29.670 23.298	11.679 2861 11.661 2864 15.986 2867	23.702 23.948	15.864 2865 24.987 2868	23.500 24.082	15.926 26.119
2857 2860 2863 2866 2869	28.850 29.670 23.298 24.169	11.679 2861 11.661 2864 15.986 2867 27.274 2870	23.702 23.948 24.346	15.864 2865 24.987 2868 28.433 2871	23.500 24.082 24.557	15.926 26.119 29.609
2857 2860 2863 2866 2869 2872	28.850 29.670 23.298 24.169 24.802	11.679 2861 11.661 2864 15.986 2867 27.274 2870 30.805 2873	23.702 23.948 24.346 25.079	15.864 2865 24.987 2868 28.433 2871 32.022 2874	23.500 24.082 24.557 25.267	15.926 26.119 29.609 34.212
2857 2860 2863 2866 2869	28.850 29.670 23.298 24.169	11.679 2861 11.661 2864 15.986 2867 27.274 2870 30.805 2873	23.702 23.948 24.346	15.864 2865 24.987 2868 28.433 2871 32.022 2874	23.500 24.082 24.557 25.267	15.926 26.119 29.609
2857 2860 2863 2866 2869 2872	28.850 29.670 23.298 24.169 24.802	11.679 2861 11.661 2864 15.986 2867 27.274 2870	23.702 23.948 24.346 25.079	15.864 2865 24.987 2868 28.433 2871	23.500 24.082 24.557	15.926 26.119 29.609 34.212

2881	23.439	17.475 2882	23.489	17.981 2883	23.540	18.493
2884	23.593	19.009 2885	23.647	19,530 2886	23.702	20.056
2887	23.759	20.588 2888	23.817	21.124 2889	23.876	21.665
2890	23.937	22.211 2891	23.999	22.762 2892	24.062	23.318
2893	24.127	23.878 2894	24.476	15.348 2895	24.842	14.859
2896	25.216	14.378 2897	25.598	13.906 2898	25.986	13.445
2899	26.380	12.993 2900	26.779	12.553 2901	27.183	12.124
2902	24.119	15.845 2903	27.607	12.113 2904	28.027	12,102
2905	28.856	12.080 2906	29.265	12.069 2907	28.443	12.091
2908	29.670	12.058 2909	23.770	16.350 2910	23.557	16.414
2911	24.287	24.991 2912	24.398	26.126 2913	24.557	27.268
2914	24.751	28.426 2915	24.978	29.602 2916	25.237	30.798
2917	25.527	32.017 2918	25.969	32.012 2919	26.800	34.208
2920	26,404	32.007 2921	27.551	34.530 2922	27.222	34.222
				16.909 2925	23.675	17.410
2923	27.990	34.530 2924	23.615			
2926	23.736	17.916 2927	23.798	18.429 2928	23.861	18.947
2929	23.926	19.472 2930	23.992	20.002 2931	24.059	20.538
2932	24.127	21.080 2933	24.197	21.628 2934	24.268	22.182
2935	24.340	22.742 2936	24.414	23.307 2937	24.488	23.879
2938	24.533	15.827 2939	24.893	15.330 2940	25.261	14.841
2941	25.637	14.361 2942	26.020	13.890 2943	26.409	13.429
2944	26.803	12.979 2945	27.203	12.540 2946	24.181	16.331
2947	27.623	12.528 2948	28.453	12.502 2949	28.040	12.515
2950	28.862	12.490 2951	29.268	12.477 2952	29.670	12.465
		16.843 2954	24.625	24.994 2955	24.766	26.121
2953	23.840					
2956	24.942	27.261 2957	25.152	28.419 2958	25.435	29.560
2959	25.667	30.792 2960	26.091	30.785 2961	26.834	32.002
2962	26.510	30.779 2963	27.615	34.225 2964	27.257	31.997
2965	28.422	34.530 2966	28.000	34.227 2967	28.845	34.530
2968	29.262	34.530 2969	23.910	17.343 2970	23.982	17.850
					24.205	19.412
2971	24.055	18.364 2972	24.129	18.884 2973		
2974	24.281	19.946 2975	24.359	20.488 2976	24.438	21.036
2977	24.518	21.591 2978	24.599	22.153 2979	24.682	22.722
2980	24,765	23.297 2981	24.850	23.880 2982	24.590	16.313
2983	24.944	15.808 2984	25.307	15.311 2985	25.677	14.823
2986	26.054	14.344 2987	26.438	13.874 2988	26.828	13.414
					27.640	12.951
2989	27.223	12.965 2990	24.245	16.825 2991		
2992	28.462	12.923 2993	28.868	12.909 2994	28.053	12.937
2995	29.271	12.895 2996	29.670	12.881 2997	24.972	24.991
2998	25.131	26.116 2999	25.324	27.255 3000	25.549	28.412
3001	25.806	29.588 3002	26.213	29.580 3003	26.924	30.772
3004	26.615	29.573 3005	27.675	31.992 3006	27.332	30.766
						34.230
3007	28.395	34.227 3008	28.086	31.987 3009	28.787	
3010	29.670	34.530 3011	29.185	34.232 3012	24.310	17.325
3013	24.377	17.832 3014	24.444	18.347 3015	24.512	18.868
3016	24.581	19.397 3017	24.652	19.932 3018	24.724	20.475
3019	24.796	21.025 3020	24.870	21.582 3021	24.945	22.146
3022	25.021	22.717 3023	25.098	23.295 3024	25.176	23.880
				16.294 3027	25.353	15.790
3025	24.649	16.806 3026	24.996			
3028	25.717	15.293 3029	26.089	14.805 3030	26.468	14.327
3031	26.854	13.858 3032	27.244	13.399 3033	28.066	13.369
3034	27.657	13.384 3035	28.472	13.353 3036	28.875	13.338
3037	29.274	13.323 3038	29.670	13.308 3039	25.430	25.558
3040	25.493	26.110 3041	25.702	27.248 3042	25.943	28.404
		28.397 3044	27.013	29.566 3045	26.719	28.390
3043	26.333					
3046	27.735	30.759 3047	27.406	29.559 3048	28.491	31.982
3049	28.133	30.753 3050	28.890	31.976 3051	29.670	33.234
3052	29.283	31.971 3053	24.708	17.306 3054	24.769	17.814
3055	24.830	18.329 3056	24.893	18.852 3057	24.957	19.381
3058	25.021	19.918 3059	25.087	20.462 3060	25.153	21.014
	25.221	21.573 3062	25.290	22.138 3063	25.359	22.712
3061						
3064	25.430	23.292 3065	25.502	23.880 3066	25.050	16.787
3067	25.400	16.275 3068	25.759	15.771 3069	26.125	15.275
3070	26.499	14.787 3071	26.879	14.309 3072	27.266	13.841
3073	28.080	13.809 3074	28.482	13.792 3075	27.674	13.825
3076	28.882	13,776 3077	29.277	13.760 3078	29.670	13.744
3079	25.661	24.986 3080	25.854	26.105 3081	26.078	27.242
		27.235 3083	27.101	28.383 3084	26.821	27.229
3082	26.451					
3085	27.795	29.551 3086	27.479	28.375 3087	28.525	30.746
3088	28.179	29.544 3089	29.075	31.063 3090	29.670	31.966
3091	29.294	30.733 3092	25.104	17.288 3093	25.159	17.796
3094	25.215	18.312 3095	25.272	18.835 3096	25.330	19.366
3097	25.389	19.904 3098	25.448	20.450 3099	25.509	21.003
	25.571	21.563 3101	25.633	22.131 3102	25.697	22.707
3100						
3103	25.761	23.290 3104	25.827	23.880 3105	25.455	16.925
3106	25.801	16.257 3107	26.162	15.752 3108	26.531	15.256
3109	26.906	14.770 3110	27.287	14.292 3111	28.493	14.241
3112	28.094	14.258 3113	28.888	14.224 3114	27.692	14.275
3115	29.281	14.207 3116	29.670	14.189 3117	26.003	24.983
				26.095 3120	27.187	27.222
3118	26.212	26.100 3119	26.568			
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ELEM ID DEFINIT .: ID, RECH(FT/D, - IS RECHARGE), VPRM(1/D), HDLEAK (15,3F10.0)
  1 -0.0002
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 31 -0.00137
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 33 -0.00105
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 35 -0.0000
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 65 -0.0122
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GS ARRAY: INP, SFCT (12,F10.0); NODE, GROUND SURFACE ELEVATION (5(15,F10.0))
  1 5129,4447
              2 5140.7201 3 5127.1738 4 5142.5613 5 5127.4628
  6 5127.8363
              7 5146.9969 8 5129.4176 9 5128.1809 10 5126.1001
 11 5149.0465 12 5146.0134 13 5129.8582 14 5128.0755 15 5127.7593
 16 5128.3173 17 5149.5409 18 5136.1113 19 5132.0060 20 5129.1152
 21 5129.5118 22 5127.4042 23 5129.4233 24 5149.4295 25 5137.5508
 26 5133.6523 27 5130.2817 28 5130.6920 29 5130.9855 30 5128.3482
 31 5128.3110 32 5147.3604 33 5138.9418 34 5134.8354 35 5131.3708
 36 5132.4126 37 5132.5294 38 5129.7477 39 5127.4007 40 5126.8978
 41 5145.4277 42 5140.2176 43 5139.7340 44 5132.0192 45 5134.6688
 46 5139.1257 47 5131.8738 48 5128.2196 49 5125.2732 50 5124.6316
 51 5144.0722 52 5140.9371 53 5144.4277 54 5133.6414 55 5142.0246
 56 5145.7745 57 5139.3132 58 5131.6952 59 5127.3056 60 5124.9845
 61 5125.3871 62 5144.0027 63 5140.9668 64 5140.8888 65 5138.3786
 66 5146.7521 67 5142.7706 68 5145.7494 69 5140.6834 70 5130.4015
 71 5127.5075 72 5124.8194 73 5129.1586 74 5146.3063 75 5141.9699
 76 5142.3294 77 5143.7993
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 81 5144.5470 82 5138.5232 83 5132.6192 84 5133.1101 85 5124.2292
 86 5131.7367 87 5147.5869 88 5142.6679 89 5143.7520 90 5139.4782
 91 5149.2820 92 5144.0778 93 5140.1538 94 5140.1272 95 5147.4070 96 5143.7915 97 5135.9312 98 5134.8949 99 5126.4638 100 5134.1607
 101 5150.0397 102 5143.8583 103 5145.4244 104 5138.7897 105 5129.1356
 106 5129.6980 107 5130.0544 108 5130.9097 109 5130.5803 110 5129.8408
 111 5129.4233 112 5128.2862 113 5127.9575 114 5128.2347 115 5128.8917
116 5129.4118 117 5130.1017 118 5130.2315 119 5130.7475 120 5131.0832
 121 5131.9723 122 5132.1816 123 5133.3349 124 5133.8261 125 5134.7322
 126 5136.6558 127 5137.5922 128 5140.1378 129 5141.3690 130 5143.1901
 131 5145.0101 132 5146.6565 133 5147.0012 134 5152.0882 135 5150.1761
136 5144.4124 137 5139.6006 138 5137.8374 139 5137.1530 140 5136.0884
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146 5140.7246 147 5143.1180 148 5152.1801 149 5146.9775 150 5138.5277
151 5136.4771 152 5137.8729 153 5153.2567 154 5147.1131 155 5147.3761
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5148,3703 459 5148,6687 460 5148,9058 461 5147.2970 462 5152.3057 463 5155.3796 464 5154.5991 465 5170.1543 466 5163.4528 467 5169.8811 468 5160.5924 469 5151.0437 470 5148.5593 471 5146.2425 472 5146.2495 473 5147.8695 474 5147.8299 475 5149.2364 476 5149.2497 477 5149.2733 478 5149.0387 479 5148.0284 480 5146.9560 481 5149.1567 482 5149.9494 483 5151.5813 484 5152.7857 485 5154.5979 486 5155.3610 487 5157.0258 488 5158.0470 489 5158.5659 490 5160.7585 491 5158.1990 492 5155.2671 493 5150.1743 494 5145.9406 495 5144.5963 496 5142.6638 497 5141.9382 498 5140.9471 499 5140.3277 500 5156.2192 501 5158.4839 502 5158.9058 503 5159.3001 504 5155.8796 505 5156.2077 506 5154.0765 507 5150.3877 508 5148.8120 509 5149.2956 510 5150.4912 511 5153.7162 512 5154.8182 513 5158.2266 514 5158.8186 515 5161.7617 516 5157,7580 517 5171,1877 518 5168,3961 519 5169,7410 520 5166,7232 521 5154.5604 522 5151.4257 523 5148.2899 524 5149.9499 525 5150.9305 526 5151.8019 527 5151.7840 528 5152.8394 529 5151.4909 530 5151.2760 531 5150.6725 532 5151.3036 533 5151.8858 534 5154.6417 535 5155.1713 536 5157.4458 537 5157.9574 538 5159.5185 539 5159.3765 540 5160.4612 541 5161.1287 542 5158,8509 543 5156.8675 544 5151.1262 545 5146.9312 546 5145.0518 547 5144.8280 548 5142.2557 549 5142.1546 550 5141.4252 551 5163.2964 552 5165.8674 553 5161.6766 554 5160.8456 555 5157.3456 556 5157.7517 557 5162.3461 558 5156.8113 559 5152.0888 560 5150.6446 561 5150.5056 562 5152.0755 563 5153.5937 564 5155.5448 565 5160.0378 566 5161.3862 567 5157.8357 568 5156.6686 569 5170.9631 570 5169.5058 571 5171.2778 572 5167.0851 573 5151.9277 574 5152.0411 575 5152.3624 576 5153,7896 577 5155,3421 578 5155,6345 579 5154,0703 580 5153,8706 581 5153.5582 582 5153.2986 583 5153.2692 584 5153.5780 585 5155.2870 586 5156.5196 587 5158.2894 588 5159.5062 589 5160.7046 590 5161.7168 591 5162.7985 592 5162.0939 593 5160.3157 594 5157.2308 595 5152.6042 596 5148.1141 597 5146.6928 598 5145.8730 599 5143.1313 600 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5176.4397 2803 5224.2271 2804 5236.6743 2805 5238.7816 2806 5242.2974 2807 5244.4446 2808 5253.3643 2809 5256.9040 2810 5256.6123 2811 5220.5373 2812 5259.1104 2813 5259.3625 2814 5260.5530 2815 5261.8388 2816 5266.4763 2817 5266.2837 2818 5218.7300 2819 5216.2204 2820 5211.2146 2821 5208.8715 2822 5171.9529 2823 5168.6928 2824 5165.3342 2825 5163.0794 2826 5159.5321 2827 5156.6231 2828 5153.3479 2829 5147.9793 2830 5153.6114 2831 5154.2902 2832 5154.5727 2833 5217.2528 2834 5218.3480 2835 5217.4937 2836 5214.6507 2837 5211.3898 2838 5207.8431 2839 5203.3657 2840 5199.7648 2841 5197.1322 2842 5194.2029 2843 5190.4475 2844 5186.0870 2845 5185.0964 2846 5182.5547 2847 5179.0673 2848 5176.5715 2849 5230.8136 2850 5234.0211 2851 5241 3879 2852 5243.6955 2853 5246.7368 2854 5250.4214 2855 5256.8211 2856 5260,0145 2857 5223,8004 2858 5263,1588 2859 5262,7097 2860 5263,5595 2861 5263,0980 2862 5264.4269 2863 5262.9687 2864 5221.7786 2865 5219.4983 2866 5217,4901 2867 5172,1879 2868 5168,9742 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3306 5189.7482 3307 5185.2260 3308 5232.0536 3309 5226.6601 3310 5221.4359
3311 5217.6188 3312 5214.8509 3313 5211.2355 3314 5206.1633 3315 5231.5254
3316 5232.7580 3317 5232.3479 3318 5231.4862 3319 5233.7011 3320 5207.7430
3321 5204.5900 3322 5200.6454 3323 5196.2365 3324 5191.3772 3325 5225.6911
3326 5221.2906 3327 5219.3427 3328 5217.9320 3329 5213.7498 3330 5226.8882
3331 5227.4140 3332 5228.2045 3333 5232.0643 3334 5210.2995 3335 5205.4077
3336 5200.5153 3337 5195.3114 3338 5222.3849 3339 5222.7765 3340 5223.6359
3341 5217.7607 3342 5226.1544 3343 5230.7802 3344 5232.1914 3345 5210.6133
3346 5205.7282 3347 5200.1882 3348 5224.9434 3349 5223.1982 3350 5217.0881
3351 5226.0454 3352 5229.7503 3353 5210.9046 3354 5205.4543 3355 5223.0537
3356 5216.6667 3357 5224.9144 3358 5211.7149 3359 5218.3934
ZBED ARRAY: INP,SFCT (12,F10.0); NODE, BEDROCK ELEVATION (5(15,F10.0))
  1 5080.0613
               2 5080.5223 3 5080.8140 4 5082.3097 5 5083.4592
               7 5083.6762 8 5083.4239 9 5083.1709 10 5083.5861
  6 5083.9279
 11 5081.7525 12 5082.6807 13 5080.5572 14 5080.6219 15 5080.1033
 16 5076.1856 17 5078.0083 18 5078.8291 19 5075.2575 20 5076.4334
 21 5071.6757 22 5073.7695 23 5070.9392 24 5076.8517 25 5074.8233
 26 5072.9252 27 5070.9712 28 5068.7307 29 5068.1716 30 5069.1693
 31 5068 0597
               32 5081.2807 33 5076.8411 34 5073.3741 35 5069.6959
 36 5069.0304 37 5067.0263 38 5066.9614 39 5067.3373 40 5066.7689
 41 5084.4025
               42 5081.2007 43 5076.4314 44 5073.0688 45 5072.2090
               47 5066.9638 48 5066.7720 49 5068.7559 50 5067.4170
 46 5067.8995
 51 5087.6836
               52 5084.2106 53 5079.7203 54 5078.0043 55 5076.9939
 56 5071.5494
               57 5068.7428 58 5067.3435 59 5067.0194 60 5069.9307
 61 5069.8999
               62 5089.7568 63 5087.5179
                                           64 5085.8933 65 5083.0935
 66 5082.8875 67 5079.1482 68 5074.7661 69 5069.6822
                                                        70 5067.7736
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101 5096.8919 102 5097.9074 103 5096.5976 104 5098.8947 105 5075.1000
106 5076.5500 107 5078.6900 108 5081.4300 109 5082.9200 110 5083.6700
111 5084.6200 112 5085.2500 113 5085,9600 114 5085,8200 115 5084,6700
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121 5088.4900 122 5092.2500 123 5094.7100 124 5097.1900 125 5098.6400
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131 5103.9200 132 5105.8500 133 5107.2500 134 5109.4610 135 5112.4164
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5102.4400 273 5104.6800 274 5107.4300 275 5108.6800 276 5104.5200 277 5101.0800 278 5102.0100 279 5103.7100 280 5103.6000 281 5103.1200 282 5102.8800 283 5103.0200 284 5104.1600 285 5106.3400 286 5111.2031 287 5112.3243 288 5114.3180 289 5117.1471 290 5119.3305 291 5120.7435 292 5120.5128 293 5119.0757 294 5117.8798 295 5119.1289 296 5117.3110 297 5112.4324 298 5117.6928 299 5117.6830 300 5113.7100 301 5111.7100 302 5104.3739 303 5099.5338 304 5102.5559 305 5104.8371 306 5107.0686 307 5106.1531 308 5104.8509 309 5105.0459 310 5110.8925 311 5115.6484 312 5117.7383 313 5104.1021 314 5104.9608 315 5105.9034 316 5106.4960 317 5107.0803 318 5108.8859 319 5090.7500 320 5094.3200 321 5099.5000 322 5104.5900 323 5107.9200 324 5109.1300 325 5109.0300 326 5107,7900 327 5105,2900 328 5103,4600 329 5102,9700 330 5103,6600 331 5103,6700 332 5103,3700 333 5103,2200 334 5103,7900 335 5105,0000 336 5106.8800 337 5109.0200 338 5113.1522 339 5114.8593 340 5118.3780 341 5121.0099 342 5122.0332 343 5120.5745 344 5119.1601 345 5118.8334 346 5119,7425 347 5119,9540 348 5117.4188 349 5119.6222 350 5121.6605 351 5116.2000 352 5115.8300 353 5112.6600 354 5106.0047 355.5105.1789 356 5111.2719 357 5115.3213 358 5114.2045 359 5115.3280 360 5115.8940 361 5109.0110 362 5112.5258 363 5118.2338 364 5120.1271 365 5115.1691 366 5114.5740 367 5114.5822 368 5115.1190 369 5114.0337 370 5112.8155 371 5112.5452 372 5111.3499 373 5110.2855 374 5109.2800 375 5109.6500 376 5109.1100 377 5107.1600 378 5104.9600 379 5103.6400 380 5104.1100 381 5104.8300 382 5104.6000 383 5104.0800 384 5103.8700 385 5104.1300 386 5105.7500 387 5107.4900 388 5109.6100 389 5116.3399 390 5116.6445 391 5119.2292 392 5121.6618 393 5122.7179 394 5121.2116 395 5119.1546 396 5118,9989 397 5120,5476 398 5120,4017 399 5119,1333 400 5120,4863 401 5123,9266 402 5122,8255 403 5120,9200 404 5117,7100 405 5113,9700 406 5111.2200 407 5113.9934 408 5118.3369 409 5119.3188 410 5122.0386 411 5122,5205 412 5121,8650 413 5113,4927 414 5117,0696 415 5119,4593 416 5121.3619 417 5121.6874 418 5120.7335 419 5119.6053 420 5118.5243 421 5116.9550 422 5115.0270 423 5112.7090 424 5111.8580 425 5110.0032 426 5109.5927 427 5108.2546 428 5107.5081 429 5107.5190 430 5107.8041 431 5108.3757 432 5110.0557 433 5110.8580 434 5111.9237 435 5113.4570 431 5108.3757 432 5110.0557 433 5110.8580 434 5111.9237 435 5113.4570 436 5114.4194 437 5117.7829 438 5118.1796 439 5118.3138 440 5117.8884 441 5118.1872 442 5120.3578 443 5123.4783 444 5123.5742 445 5120.8679 446 5119.3688 447 5119.1418 448 5120.8120 449 5122.2425 450 5120.0125 451 5120.7349 452 5124.4798 453 5125.5844 454 5124.0635 455 5121.4589 456 5121,9070 457 5118.6658 458 5116.1170 459 5118.0541 460 5120.7381 461 5123.1261 462 5125.3585 463 5125.8759 464 5124.9333 465 5119.1797 466 5119.1114 467 5120.5716 468 5122.8872 469 5124.3156 470 5123.1896 471 5121.1012 472 5119.4876 473 5117.2227 474 5114.1164 475 5111.5814 476 5110.3694 477 5109.5227 478 5109.1080 479 5108.9113 480 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2602 5133.9000 2603 5134.0000 2604 5133.7000 2605 5207.1800 2606 5215.8300 2607 5222.1500 2608 5227.1200 2609 5230.6000 2610 5232.7900 2611 5235.7000 2612 5239.6000 2613 5194.6000 2614 5245.2100 2615 5250.8000 2616 5255.4900 2617 5260.7500 2618 5265.0400 2619 5268.5500 2620 5185.9200 2621 5184.1500 2622 5182.8600 2623 5181.5800 2624 5180.3200 2625 5179.1200 2626 5177.9400 2627 5129.6830 2628 5125.6215 2629 5134.0384 2630 5139.1772 2631 5177.0500 2632 5138.0628 2633 5133.7694 2634 5134.0942 2635 5131.3683 2636 5132.8537 2637 5128.9312 2638 5126.3980 2639 5175.8800 2640 5174.6000 2641 5172.9935 2642 5171.6188 2643 5170.3734 2644 5168.6249 2645 5166.0038 2646 5162.4360 2647 5158.1738 2648 5151.9019 2649 5145.1623 2650 5140.9209 2651 5139.5133 2652 5139.6090 2653 5141.1321 2654 5140.7127 2655 5138.3271 2656 5134.8000 2657 5134.4440 2658 5134.1470 2659 5202.5700 2660 5211.5500 2661 5220.5800 2662 5227.1900 2663 5231.9000 2664 5234.3800 2665 5235.9400 2666 5241.0400 2667 5192.0000 2668 5247.5100 2669 5252.8100 2670 5258.3700 2671 5262.0000 2672 5264.7300 2673 5268.3700 2674 5185.2200 2675 5183.4500 2676 5181.9200 2677 5180.4900 2678 5179.1100 2679 5177.9400 2680 5176.7800 2681 5130.1883 2682 5124.1161 2683 5131.2677 2684 5138.3944 2685 5137.6497 2686 5134.0105 2687 5132.6010 2688 5128.7691 2689 5126.2577 2690 5175.6600

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5139.1948 2753 5138.4413 2754 5136.8000 2755 5136.5000 2755 5 2756 5136,0000 2757 5193,1600 2758 5213,0200 2759 5216,4400 2760 5224,2500 2761 5232,2800 2762 5236,6700 2763 5239,5300 2764 5242,1100 2765 5189,4400 2766 5247.2100 2767 5250.8200 2768 5256.0000 2769 5259.4100 2770 5263.3000 2771 5260.2800 2772 5184.9900 2773 5182.8700 2774 5177.9411 2775 5177.6146 2776 5175,9061 2777 5131,9321 2778 5122,8209 2779 5124,1917 2780 5133,5870 2781 5135.3191 2782 5134.1283 2783 5132.1760 2784 5130.6406 2785 5130.3432 2786 5174,9542 2787 5173,6057 2788 5172,0330 2789 5169,9372 2790 5167,3991 2791 5164.2653 2792 5160.1695 2793 5155.5037 2794 5150.3016 2795 5145.6035 2796 5140.2906 2797 5137.6939 2798 5138.2156 2799 5138.1270 2800 5137.5000 2801 5137.0000 2802 5136.5000 2803 5190.4100 2804 5207.7600 2805 5217.4900 2806 5222.9000 2807 5231.5800 2808 5235.8000 2809 5240.3500 2810 5244.9700 2811 5189.4800 2812 5250.8700 2813 5253.3900 2814 5256.8900 2815 5259.9100 2816 5260.7600 2817 5261.4800 2818 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5185.6438 2947 5234.7800 2948 5241.7600 2949 5238.4700 2950 5243.6500 2951 5244.2700 2952 5244.3400 2953 5177.0775 2954 5138.8020 2955 5133.4212 2956 5124.2430 2957 5121.2698 2958 5121.2701 2959 5127.7375 2960 5124.0779 2961 5129.9287 2962 5119.3536 2963 5129.4873 2964 5128.3297 2965 5125.8724 2966 5127,9683 2967 5124,6697 2968 5123,8156 2969 5174,1478 2970 5172,6880 2971 5170.9283 2972 5169.1244 2973 5167.4139 2974 5165.9036 2975 5164.4568 2976 5160.7289 2977 5155.9818 2978 5149.5480 2979 5143.6265 2980 5138.3300 2981 5138.2000 2982 5187.3183 2983 5189.7301 2984 5190.9035 2985 5207.5700 2986 5212.4600 2987 5215.4600 2988 5218.9100 2989 5224.9700 2990 5182.1734 2991 5228.0700 2992 5235.2400 2993 5239.2800 2994 5231.7800 2995 5242.0500 2996 5243.9000 2997 5139.7694 2998 5136.7372 2999 5126.4523 3000 5125.5744 3001 5126.2180 3002 5128.8612 3003 5118.6427 3004 5129.6106 3005 5125.5923 3006 5117.5007 3007 5126.4758 3008 5122.2377 3009 5124.9433 3010 5123.4452 3011 5124.4461 3012 5179.1053 3013 5176.4364 3014 5174.2582 3015 5173.1668 3016 5171,5672 3017 5169,7655 3018 5168,4986 3019 5165,0347 3020 5159,5750 3021 5153,7112 3022 5145,9821 3023 5141,5082 3024 5138,2800 3025 5182,5585 3026 5187.6260 3027 5187.9752 3028 5188.2731 3029 5202.3400 3030 5206.2100 3031 5210.9200 3032 5217.7700 3033 5226.4300 3034 5221.8500 3035 5229.4100 3036 5234.4600 3037 5240.5100 3038 5244.0500 3039 5138.8720 3040 5138.0516 3041 5128.5793 3042 5130.4292 3043 5130.3529 3044 5126.0173 3045 5128.8582 3046 5116.8373 3047 5121.1103 3048 5120.6053 3049 5116.9704 3050 5119.6956 3051 5123.2212 3052 5118.5693 3053 5180.9400 3054 5180.5387 3055 5179.9421 3056 5177.7765 3057 5174.0777 3058 5171.1401 3059 5169.4477 3060 5166.0199 3061 5161.2721 3062 5155.2464 3063 5147.3029 3064 5138.5900 3065 5138.3700 3066 5182.6244 3067 5180.9814 3068 5181.9679 3069 5184.4445 3070 5199.2100 3071 5204,0500 3072 5210,9600 3073 5223,4000 3074 5227,2200 3075 5216,0400 3076 5230.8500 3077 5238.8100 3078 5244.1000 3079 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3341 5189.7805 3342 5208.8253 3343 5216.2014 3344 5217.4568 3345 5184.9544
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3351 5213.4518 3352 5214.5486 3353 5195.1027 3354 5189.3706 3355 5208.2324
3356 5202.4761 3357 5210.3834 3358 5199.0197 3359 5205.7303
ZBASE ARRAY: INP,SFCT (I2,F10.0); NODE,AQUIFER BASE ELEVATION (5(15,F10.0))
   1.0000
     5079 06
                  5079.52 3 5079.81 4 5081.31 5 5082.46
    5082.93
               7 5082.68 8 5082.42 9 5082.17 10 5082.47
     5080.75 12 5081.68 13 5079.56 14 5079.62 15 5079.10 5075.19 17 5077.01 18 5077.83 19 5073.79 20 5075.43
 11
 16
     5070.68 22
                   5072.77
                                  5069.94
                                                5075.85 25
                                                               5073.82
                             23
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     5071.03 27
                   5068.78 28
                                  5067.23
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     5067.06 32
                   5080.28 33
                                  5075.84
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                                                5072.37 35
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     5067.53
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                   5066.03 38
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                                                5066.34 40
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     5083.40
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                                  5075.43
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                                                               5071.21
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                                  5065.77
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                                                5067.76 50
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     5086.68
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                                  5078.72
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     5070.39 57
                   5067.74 58
                                  5066.34
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     5079.91 67
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                                                  5101.97 140
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141
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166
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186
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191
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201
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                                 5162.28 3259
                                              5161 48 3260
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      5158.99 3262
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                                                            5149.97
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                                              5161.06 3310
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      5159.41 3327 5157.94 3328
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                                 5157.92 3349
                                              5156.47 3350
                                                            5155.09
3351 5157.75 3352 5157.79 3353 5153.89 3354 5153.43 3355 5156.30
3356 5154.93 3357 5156.24 3358 5153.87 3359 5154.81
HYDK1 ARRAY: INP,SFCT (I2,F10.0); NODE,HYDR. COND (AQ.1) (FT/DAY) 5(I5,F10.0)
  1.0000
  1 1282.5900
              2 1200.0000 3 1259.1100 4 1200.0000 5 1500.0000
  6 1200.0000
              7 1375.7300 8 1500.0000 9 1334.2900 10 1200.0000
 11 1433.5200
              12 1500.0000 13 1500.0000 14 1200.0000 15 1200.0000
 16 1200.0000 17 1500.0000 18 400.0000 19 1500.0000 20 1500.0000
 21 1346.6300 22 1200.0000 23 1096.7500 24 1337.2000 25 406.1300
 26 1500,0000 27 1500,0000 28 1500,0000 29 1500,0000 30 1257,0600
 31 1500.0000
              32 1392,5800 33 605,5600 34 995,1000 35 1096,3200
 36 1479.2800 37 1500.0000 38 1500.0000 39 1218.7400 40 1500.0000
 41 690.0800 42 1086.3000 43 525.4500 44 80.0000 45 80.0000
    55.0000 47 1500.0000 48 1500.0000 49 416.1100 50 1462.9400
    400.0000 52 1419.7600 53 542.8100 54 80.0000 55 80.0000
 56 80.0000 57 55.0000 58 200.0000 59 1238.6400 60 540.9600 61 1088.3900 62 497.5800 63 1411.7200 64 400.0000 65 80.0000
 66 80.0000 67 80.0000 68 55.0000 69 55.0000 70 200.0000
    400.0000 72 594.3200 73 858.4700 74 454.7900 75 1444.2600
    942 6100 77
                 30.0000 78 30.0000 79 30.0000 80 55.0000
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    55.0000 82 55.0000 83 100.0000 84 400.0000 85 419.3000
    529.5100
             87
                 510.0600 88 275.0000 89 865.4300 90 30.0000
    20.0000 92 35.0000 93 55.0000 94 55.0000 95 55.0000
    55.0000 97 50.0000 98 400.0000 99 553.9500 100 250.0000
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171 100,0000 172 100,0000 173 100,0000 174 100,0000 175 215,0000
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191 230.0000 192 150.0000 193 150.0000 194 110.0000 195 20.0000
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2616	2.0000 2617	2.0000 2618	2.0000 2619	2.0000 2620	0.5000 1.0000
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2836				2.8100 2845	2.8100
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2866	4.0000 2867	2.8100 2868	2.8100 2869	2.8100 2870	
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2881	4.0000 2882	4.0000 2883	4.0000 2884	4.0000 2885	4.0000
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STORAGE COEFF. ARRAY: INP,SFCT (I2,F10.0); NODE, STORAGE (5(I5,F10.0))
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26 31	0.25 27	0.25 28	0.25 29		.25
36	0.25 37	0.25 38	0.25 39	0.25 40 0	.25
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46	0.25 47	0.25 48	0.25 49	0.25 50 0	.25
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61	0.25 62	0.25 63	0.25 64		.25
66	0.25 67	0.25 68	0.25 69	0.25 70 0	.25
71	0.25 72	0.25 73	0.25 74	0.25 75 0	.25
76	0.25 77	0.25 78	0.25 79	0.25 80 0	.25
81	0.25 82	0.25 83	0.25 84		.25
86	0.25 87	0.25 88	0.25 89		.25
91	0.25 92	0.25 93	0.25 94 0.25 99		.25 0.25
96	0.25 97 0.25 102	0.25 98 0.25 103	0.25 99	0.25 100	0.25
101 106	0.25 102 0.25 107	0.25 103 0.25 108	0.25 104	0.25 110	0.25
111	0.25 107	0.25 113	0.25 114	0.25 115	0.25
116	0.25 117	0.25 118	0.25 119	0.25 120	0.25
121	0.25 122	0.25 123	0.05 124	0.05 125	0.05
126	0.05 127	0.05 128	0.05 129	0.05 130	0.05
131	0.05 132	0.25 133	0.25 134	0.05 135	0.05
136	0.05 137	0.05 138	0.05 139	0.05 140	0.05
141	0.05 142	0.05 143	0.05 144	0.25 145	0.25
146	0.25 147	0.25 148	0.25 149	0.25 150	0.25
151	0.25 152	0.25 153	0.25 154	0.25 155	0.25
156	0.25 157	0.25 158	0.25 159	0.25 160	0.25
161	0.05 162	0.05 163	0.25 164	0.05 165	0.05
166	0.25 167	0.25 168	0.25 169	0.25 170	0.25
171	0.25 172	0.25 173	0.25 174	0.25 175	0.25
176	0.05 177	0.05 178	0.05 179 0.25 184	0.05 180 0.25 185	0.05 0.25
181	0.05 182 0.05 187	0.05 183 0.05 188	0.25 184 0.05 189		0.25
186 191	0.05 187 0.05 192	0.05 188	0.05 189		0.05
196	0.05 192	0.05 198	0.05 199		0.25
201	0.25 202	0.25 203	0.25 204	0.25 205	0.25
206	0.05 207	0.25 208	0.25 209		0.25
211	0.25 212	0.25 213	0.05 214		0.05
216	0.05 217	0.05 218	0.05 219	0.25 220	0.25
221	0.25 222	0.25 223	0.25 224		0.25
226	0.25 227	0.25 228	0.05 229	0.05 230	0.05
231	0.05 232	0.05 233	0.05 234		0.05
236	0.05 237	0.05 238	0.05 239		0.05
241	0.05 242	0.05 243	0.05 244		0.05
246	0.25 247 0.25 252	0.05 248 0.25 253	0.25 249 0.05 254		0.25 0.25
251 256	0.25 252 0.25 257	0.25 253 0.25 258	0.05 254		0.25
261	0.25 262	0.25 258	0.05 264		0.05
266	0.25 267	0.05 268	0.05 269		0.05
271	0.05 272	0.25 273	0.25 274		0.25
276	0.25 277	0.25 278	0.25 279	0.05 280	0.05
281	0.05 282	0.05 283	0.05 284		0.25
286	0.05 287	0.05 288	0.05 289		0.05
291	0.05 292	0.05 293	0.05 294		0.05
296	0.05 297	0.25 298	0.05 299		0.05
301	0.25 302	0.25 303	0.25 304		0.05
306	0.05 307	0.05 308	0.05 309		0.25
311	0.05 312	0.05 313	0.05 314		0.05 0.05
316 321	0.05 317 0.05 322	0.05 318 0.05 323	0.05 319 0.05 324		0.03
326	0.05 322	0.05 323	0.05 324		0.25
331	0.25 327	0.05 333	0.05 334		0.05
336	0.05 337	0.05 338	0.05 339		0.05
341	0.05 342	0.05 343	0.05 344		0.05
346	0.05 347	0.05 348	0.25 349	0.25 350	0.25
351	0.25 352	0.25 353	0.25 354	0.25 355	0.25
356	0.05 357	0.05 358	0.05 359		0.05
361	0.25 362	0.25 363	0.05 364		0.05
366	0.05 367	0.05 368	0.05 369		0.05
371	0.05 372	0.05 373	0.05 374		0.05
376	0.25 377	0.25 378	0.25 379	0.25 380	0.25
381	0.25 382	0.25 383	0.05 384 0.05 389		0.05 0.05
386 391	0.05 387 0.05 392	0.05 388 0.05 393	0.05 389		0.05
396	0.05 392	0.05 393	0.05 399		0.03
401	0.05 402	0.05 398	0.25 404		0.25
406	0.05 402	0.05 408	0.05 409		0.05
411	0.05 412	0.05 413	0.05 414		0.25

416	0.25 417	0.05 418	0.05 419	0.05 420	0.05
421	0.05 422	0.05 423	0.05 424	0.05 425	0.05
426	0.05 427	0.25 428	0.25 429	0.25 430	0.25
431		0.25 433			
			0.05 434	0.05 435	0.05
436	0.05 437	0.05 438	0.05 439	0.05 440	0.05
441	0.05 442	0.05 443	0.05 444	0.05 445	0.05
446	0.05 447	0.05 448	0.05 449	0.25 450	0.25
451	0.25 452	0.05 453	0.05 454	0.25 455	0.25
456	0.05 457	0.05 458	0.05 459	0.05 460	0.05
461	0.05 462	0.05 463	0.05 464	0.05 465	0.05
466	0.25 467	0.25 468	0.25 469	0.05 470	0.05
471	0.05 472	0.05 473	0.05 474	0.05 475	0.05
476	0.05 477	0.25 478	0.25 479	0.25 480	0.25
481	0.25 482	0.25 483	0.25 484		
				0.05 485	0.05
486	0.05 487	0.05 488	0.05 489	0.05 490	0.05
491	0.05 492	0.05 493	0.05 494	0.05 495	0.05
496	0.05 497	0.05 498	0.05 499	0.05 500	0.05
501	0.25 502	0.25 503	0.05 504	0.05 505	0.05
506	0.25 507	0.25 508	0.25 509	0.05 510	0.05
511	0.05 512	0.05 513	0.05 514	0.05 515	0.05
516	0.05 517	0.05 518	0.25 519	0.25 520	0.25
521	0.05 522	0.05 523	0.05 524	0.05 525	0.05
526	0.05 527	0.25 528	0.25 529	0.25 530	0.25
531	0.25 532	0.25 533	0.25 534	0.25 535	0.25
536	0.05 537	0.05 538	0.05 539	0.05 540	0.05
541	0.05 542	0.05 543	0.05 544	0.05 545	0.05
546	0.05 547	0.05 548	0.05 549	0.05 550	0.05
551	0.05 552	0.05 553	0.05 554	0.05 555	0.05
556	0.05 557	0.25 558	0.25 559	0.25 560	0.25
561	0.25 562	0.05 563	0.05 564	0.05 565	0.05
566	0.05 567				
		0.05 568	0.05 569	0.05 570	0.05
571	0.25 572	0.05 573	0.05 574	0.05 575	0.05
576	0.05 577	0.25 578	0.25 579	0.25 580	0.25
581	0.25 582	0.25 583	0.25 584	0.25 585	0.25
586	0.25 587	0.05 588	0.05 589	0.05 590	0.05
591	0.05 592	0.05 593	0.05 594	0.05 595	0.05
596	0.05 597	0.05 598	0.05 599	0.05 600	0.05
601	0.05 602	0.25 603	0.25 604	0.05 605	0.05
606	0.05 607	0.05 608	0.05 609	0.25 610	0.25
611	0.25 612	0.25 613	0.25 614	0.25 615	0.25
616	0.05 617	0.05 618	0.05 619	0.05 620	0.05
621	0.25 622	0.25 623	0.25 624	0.25 625	
					0.25
626	0.05 627	0.05 628	0.25 629	0.25 630	0.25
631	0.25 632	0.25 633	0.25 634	0.25 635	0.25
636	0.25 637	0.25 638	0.25 639	0.05 640	0.05
641		0.05 643	0.05 644	0.05 645	0.05
646	0.05 647	0.05 648	0.05 649	0.05 650	0.05
651	0.05 652	0.05 653	0.25 654	0.25 655	0.25
656	0.05 657	0.05 658	0.05 659	0.05 660	0.05
661	0.25 662	0.25 663			
					0.25
666	0.25 667	0.25 668	0.05 669	0.05 670	0.05
671	0.05 672	0.05 673	0.25 674	0.25 675	0.25
676	0.25 677	0.05 678	0.05 679	0.25 680	0.25
681	0.25 682	0.25 683	0.25 684	0.25 685	0.25
686	0.25 687	0.25 688	0.25 689	0.25 690	0.25
691	0.05 692	0.05 693	0.05 694	0.05 695	0.05
696	0.05 697	0.05 698	0.05 699	0.05 700	0.05
701	0.05 702	0.05 703			
	0.05 702	0.05 705		0.05 705	0.05
706	0.25 707	0.05 708	0.05 709	0.05 710	0.05
711	0.05 712	0.05 713	0.25 714	0.25 715	0.25
716	0.25 717	0.25 718	0.25 719	0.25 720	0.25
721	0.05 722	0.05 723	0.05 724	0.05 725	0.05
726	0.25 727	0.25 728	0.05 729	0.05 730	0.05
731	0.25 732	0.25 733	0.25 734	0.25 735	0.25
736	0.05 737	0.05 738	0.25 739	0.25 740	0.25
741	0.05 742	0.05 743	0.05 744	0.05 745	0.05
746	0.05 747	0.05 748	0.05 749	0.05 750	0.05
751	0.05 752	0.05 753	0.05 754	0.05 755	0.05
756	0.25 757	0.25 758	0.05 759	0.05 760	0.05
761	0.05 762	0.05 763	0.05 764	0.05 765	0.05
766	0.25 767	0.25 768	0.25 769	0.25 770	0.25
<b>7</b> 71	0.25 772	0.25 773	0.25 774	0.05 775	0.05
776	0.05 777	0.05 778	0.25 779	0.25 780	0.25
781	0.05 782	0.25 783	0.25 784	0.25 785	0.25
786	0.25 787	0.05 788	0.05 789	0.25 790	0.25
791	0.25 792	0.05 793	0.25 794	0.05 795	0.05
796	0.05 797	0.05 798	0.05 799	0.05 800	0.05
801	0.05 802	0.05 803	0.05 804	0.05 805	0.05
806	0.05 807	0.05 808	0.25 809	0.05 810	0.05
811	0.05 812	0.05 813	0.05 814	0.05 815	0.05
816	0.25 817	0.25 818	0.25 819	0.25 820	0.25
821	0.25 822	0.25 823	0.25 824		
				0.25 825	0.25
826	0.05 827	0.05 828	0.05 829	0.05 830	0.05

831	0.25 832	0.05 833	0.25 834	0.25 835	0.25
836	0.25 837	0.25 838	0.25 839	0.05 840	0.05
841	0.25 842	0.25 843	0.25 844	0.05 845	0.05
846	0.05 847	0.05 848	0.05 849	0.25 850	0.25
851	0.05 852	0.05 853	0.05 854	0.05 855	0.05
856	0.05 857	0.05 858	0.05 859	0.25 860	0.25
861	0.05 862	0.05 863	0.05 864	0.05 865	0.05
866	0.05 867	0.25 868	0.25 869	0.25 870	0.25
871	0.25 872	0.25 873	0.25 874	0.25 875	0.25
876	0.25 877	0.25 878	0.25 879	0.25 880	0.25
881	0.05 882	0.25 883	0.25 884	0.25 885	0.25
886	0.25 887	0.25 888	0.25 889	0.25 890	0.25
891	0.05 892	0.25 893	0.25 894	0.25 895	0.25
896	0.05 897	0.05 898	0.05 899	0.25 900	0.25
901	0.05 902	0.05 903	0.05 904	0.05 905	0.05
906	0.05 907	0.05 908	0.25 909	0.25 910	0.25
	0.05 907	0.05 913	0.05 914	0.05 915	0.05
911		0.05 918	0.25 919	0.25 920	0.05
916	0.05 917		0.25 924	0.25 925	0.25
921	0.25 922	0.25 923		0.25 925	0.25
926	0.25 927	0.25 928	0.25 929		
931	0.25 932	0.25 933	0.05 934		0.25
936	0.25 937	0.25 938	0.25 939	0.25 940	0.25
941	0.25 942	0.25 943	0.25 944	0.25 945	0.25
946	0.25 947	0.05 948	0.05 949	0.05 950	0.05
951	0.25 952	0.25 953	0.05 954	0.05 955	0.05
956	0.05 957	0.05 958	0.05 959	0.05 960	0.05
961	0.25 962	0.25 963	0.25 964	0.25 965	0.25
966	0.05 967	0.05 968	0.05 969	0.25 970	0.25
971	0.25 972	0.25 973	0.25 974	0.25 975	0.25
976	0.25 977	0.25 978	0.25 979	0.25 980	0.25
981	0.25 982	0.25 983	0.25 984	0.25 985	0.25
986	0.25 987	0.25 988	0.25 989	0.25 990	0.25
991	0.25 992	0.25 993	0.25 994	0.25 995	0.25
996	0.25 997	0.25 998	0.25 999	0.05 1000	0.05
1001	0.25 1002	0.25 1003	0.05 1004		
1006	0.05 1002	0.05 1008	0.05 1009		
1011	0.25 1012	0.25 1013	0.25 1014		
	0.25 1012	0.25 1018	0.05 1019		
1016		0.25 1018	0.05 1019		
1021	0.25 1022	0.25 1023	0.25 1024		
1026	0.25 1027				
1031	0.25 1032	0.25 1033	0.25 1034		
1036	0.25 1037	0.25 1038	0.25 1039		
1041	0.25 1042	0.25 1043	0.25 1044		
1046	0.25 1047	0.25 1048	0.25 1049		
1051	0.25 1052	0.25 1053	0.25 1054		
1056	0.05 1057	0.05 1058	0.05 1059		
1061	0.05 1062	0.25 1063	0.05 1064		
1066	0.25 1067	0.25 1068	0.25 1069		
1071	0.25 1072	0.25 1073	0.25 1074		
1076	0.25 1077	0.25 1078	0.25 1079		
1081	0.25 1082	0.25 1083	0.25 1084		
1086	0.25 1087	0.25 1088	0.25 1089		
1091	0.25 1092	0.05 1093	0.25 1094		
1096	0.25 1097	0.25 1098	0.25 1099		
1101	0.25 1102	0.25 1103	0.25 1104		
1106	0.05 1107	0.05 1108	0.05 1109	0.05 111	0.05
1111	0.05 1112	0.05 1113	0.25 1114	0.05 111	5 0.05
1116	0.05 1117	0.05 1118	0.05 1119		
1121	0.25 1122	0.25 1123	0.25 1124	0.25 112	25 0.25
1126	0.25 1127	0.25 1128	0.25 1129	0.25 113	
1131	0.25 1132	0.25 1133	0.25 1134		
1136	0.25 1137	0.25 1138	0.25 1139	0.25 114	0.25
1141	0.25 1142	0.25 1143			
1146	0.25 1147	0.25 1148	0.25 1149	0.25 115	50 0.25
1151	0.25 1152	0.25 1153			55 0.25
1156	0.05 1157	0.05 1158			50 0.05
1161	0.05 1162	0.05 1163		4 0.05 116	65 0.05
1166	0.25 1167	0.05 1168			
1171	0.05 1172	0.25 1173			
1176	0.05 1172	0.25 1178			
1181	0.05 1177	0.25 1170			
1186	0.25 1182	0.25 1188			
1191	0.25 1192	0.25 1193			
1191	0.25 1192	0.25 1198			
	0.25 1197	0.25 1198			
1201	0.25 1202	0.25 1208			
1206		0.25 1208			
1211	0.05 1212				
1216	0.05 1217				
1221	0.05 1222	0.05 1223			
1226	0.05 1227	0.05 1228			30 0.25
1231	0.25 1232				
1236	0.25 1237				
1241	0.25 1242	0.25 1243	0.25 124	4 0.25 12	45 0.25

1246	0.05 1247	0.25 1248	0.25 1249	0.25 1250	0.25
1251	0.25 1252	0.25 1253	0.25 1254	0.25 1255	0.25
1256	0.25 1257	0.25 1258	0.25 1259	0.05 1260	0.05
1261	0.05 1262	0.05 1263	0.05 1264	0.05 1265	0.05
1266	0.05 1267	0.05 1268	0.05 1269		
				0.05 1270	0.05
1271	0.05 1272	0.05 1273	0.05 1274	0.25 1275	0.25
1276	0.25 1277	0.05 1278	0.05 1279	0.05 1280	0.05
1281	0.25 1282	0.25 1283	0.25 1284	0.25 1285	0.25
1286	0.25 1287	0.25 1288	0.25 1289	0.25 1290	0.25
1291	0.25 1292	0.25 1293	0.05 1294	0.05 1295	0.05
1296	0.05 1297	0.05 1298	0.05 1299	0.25 1300	0.25
1301	0.25 1302	0.25 1303	0.25 1304	0.25 1305	0.25
1306	0.25 1307	0.25 1308	0.25 1309	0.05 1310	0.05
1311	0.05 1312	0.05 1313	0.05 1314	0.05 1315	0.05
1316	0.05 1312	0.05 1313	0.05 1314	0.05 1313	0.05
1321					
	0.25 1322	0.05 1323	0.05 1324	0.25 1325	0.25
1326	0.25 1327	0.05 1328	0.05 1329	0.05 1330	0.05
1331	0.05 1332	0.25 1333	0.25 1334	0.25 1335	0.25
1336	0.25 1337	0.25 1338	0.05 1339	0.05 1340	0.05
1341	0.05 1342	0.05 1343	0.05 1344	0.05 1345	0.05
1346	0.05 1347	0.05 1348	0.05 1349	0.25 1350	0.25
1351	0.25 1352	0.25 1353	0.25 1354	0.25 1355	0.25
1356	0.25 1357	0.25 1358	0.05 1359	0.05 1360	0.05
1361	0.05 1362	0.05 1363	0.05 1364	0.05 1365	0.05
1366	0.05 1367	0.05 1368	0.05 1369	0.05 1303	0.05
1371	0.05 1307				
		0.05 1373	0.05 1374	0.25 1375	0.25
1376	0.05 1377	0.05 1378	0.05 1379	0.05 1380	0.05
1381	0.05 1382	0.25 1383	0.25 1384	0.25 1385	0.25
1386	0.25 1387	0.05 1388	0.05 1389	0.05 1390	0.05
1391	0.05 1392	0.05 1393	0.05 1394	0.05 1395	0.05
1396	0.05 1397	0.05 1398	0.25 1399	0.25 1400	0.25
1401	0.25 1402	0.25 1403	0.25 1404	0.25 1405	0.25
1406	0.25 1407	0.05 1408	0.05 1409	0.05 1410	0.05
1411	0.05 1412	0.05 1413	0.05 1414	0.05 1415	0.05
1416	0.05 1417	0.05 1418	0.05 1419	0.25 1420	0.25
1421	0.05 1417	0.05 1413	0.05 1424	0.25 1425	0.25
1426	0.05 1427	0.05 1428	0.05 1429	0.05 1430	0.05
1431	0.05 1427	0.05 1428	0.05 1429	0.05 1430	0.03
1436	0.05 1432				0.25
		0.05 1438	0.05 1439	0.05 1440	
1441	0.05 1442	0.05 1443	0.05 1444	0.05 1445	0.05
1446	0.05 1447	0.05 1448	0.25 1449	0.25 1450	0.25
1451	0.25 1452	0.25 1453	0.25 1454	0.25 1455	0.25
1456	0.05 1457	0.05 1458	0.05 1459	0.05 1460	0.05
1461	0.05 1462	0.05 1463	0.05 1464	0.05 1465	0.05
1466	0.05 1467	0.05 1468	0.25 1469	0.25 1470	0.25
1471	0.05 1472	0.05 1473	0.05 1474	0.25 1475	0.25
1476	0.05 1477	0.05 1478	0.05 1479	0.05 1480	0.05
1481	0.05 1482	0.05 1483	0.05 1484	0.05 1485	0.05
1486	0.05 1487	0.05 1488	0.05 1489	0.05 1490	0.05
1491	0.05 1492	0.05 1493	0.05 1494	0.05 1495	0.05
1496	0.05 1497	0.25 1498	0.25 1499	0.25 1500	0.25
1501	0.25 1502	0.25 1503	0.25 1504	0.25 1505	0.25
1506	0.05 1507	0.05 1508	0.05 1509	0.05 1510	0.05
1511	0.05 1512	0.05 1513	0.05 1514	0.05 1515	0.05
1516	0.05 1512	0.05 1518	0.25 1519	0.25 1519	0.25
1521	0.05 1517	0.05 1518	0.25 1519	0.25 1525	0.25
1526	0.05 1522	0.05 1528		0.25 1525	
	0.05.1500		0.05 1529		0.05
1531	0.05 1532	0.05 1533	0.05 1534	0.05 1535	0.05
1536	0.05 1537	0.05 1538	0.05 1539	0.05 1540	0.05
1541	0.05 1542	0.05 1543	0.05 1544	0.05 1545	0.05
1546	0.25 1547	0.25 1548	0.25 1549	0.25 1550	0.25
1551	0.25 1552	0.25 1553	0.25 1554	0.25 1555	0.25
1556	0.05 1557	0.05 1558	0.05 1559	0.05 1560	0.05
1561	0.05 1562	0.05 1563	0.05 1564	0.05 1565	0.05
1566	0.05 1567	0.05 1568	0.25 1569	0.25 1570	0.25
1571	0.05 1572	0.25 1573	0.25 1574	0.25 1575	0.25
1576	0.25 1577	0.05 1578	0.05 1579	0.05 1580	0.05
1581	0.05 1582	0.05 1583	0.05 1584	0.05 1585	0.05
1586	0.05 1587	0.05 1588	0.05 1589	0.05 1590	0.05
1591	0.05 1592	0.05 1593	0.05 1594	0.05 1595	0.05
1596	0.05 1597	0.25 1598	0.25 1599	0.05 1595	0.03
1601	0.05 1597	0.25 1603	0.25 1604	0.25 1605	0.25
1606	0.25 1602 0.05 1607	0.25 1603		0.25 1605	
1611			0.05 1609		0.05
	0.05 1612	0.05 1613	0.05 1614	0.05 1615	0.05
1616	0.05 1617	0.05 1618	0.05 1619	0.25 1620	0.25
1621	0.25 1622	0.25 1623	0.25 1624	0.25 1625	0.25
1626	0.25 1627	0.25 1628	0.05 1629	0.05 1630	0.05
1631	0.05 1632	0.05 1633	0.05 1634	0.05 1635	0.05
1636	0.05 1637	0.05 1638	0.05 1639	0.05 1640	0.05
1641	0.05 1642	0.05 1643	0.05 1644	0.05 1645	0.05
1646	0.05 1647	0.25 1648	0.25 1649	0.25 1650	0.25
1651	0.25 1652	0.25 1653	0.25 1654	0.25 1655	0.25
1656	0.25 1657	0.25 1658	0.05 1659	0.05 1660	0.05
		,	1007	3.00 1000	0.00

1661	0.05 1662	0.05 1663	0.05 1664	0.05 1665	0.05
1666	0.05 1667	0.05 1668	0.25 1669	0.25 1670	0.25
1671	0.25 1672	0.25 1673	0.25 1674	0.25 1675	0.25
1676	0.25 1677	0.25 1678	0.25 1679	0.25 1680	0.25
1681	0.05 1682	0.05 1683	0.05 1684	0.05 1685 0.05 1690	0.05 0.05
1686	0.05 1687	0.05 1688 0.05 1693	0.05 1689 0.05 1694	0.05 1695	0.05
1691 1696	0.05 1692 0.05 1697	0.05 1698	0.05 1699	0.25 1700	0.25
1701	0.05 1097	0.25 1703	0.25 1704	0.25 1705	0.25
1706	0.25 1707	0.25 1708	0.25 1709	0.25 1710	0.25
1711	0.05 1712	0.05 1713	0.05 1714	0.05 1715	0.05
1716	0.05 1717	0.05 1718	0.25 1719	0.25 1720	0.25
1721	0.25 1722	0.25 1723	0.25 1724	0.25 1725	0.25
1726	0.25 1727	0.25 1728	0.25 1729	0.25 1730	0.25
1731	0.25 1732	0.25 1733	0.25 1734	0.25 1735 0.05 1740	0.25 0.05
1736	0.05 1737	0.05 1738 0.05 1743	0.05 1739 0.05 1744	0.05 1740	0.05
1741 1746	0.05 1742 0.05 1747	0.05 1748	0.05 1749	0.05 1750	0.05
1751	0.05 1752	0.25 1753	0.25 1754	0.25 1755	0.25
1756	0.25 1757	0.25 1758	0.25 1759	0.25 1760	0.25
1761	0.25 1762	0.25 1763	0.25 1764	0.25 1765	0.25
1766	0.05 1767	0.05 1768	0.05 1769	0.05 1770	0.05
1771	0.25 1772	0.25 1773	0.25 1774	0.25 1775	0.25
1776	0.05 1777	0.25 1778	0.25 1779	0.25 1780 0.25 1785	0.25 0.25
1781	0.25 1782	0.25 1783 0.25 1788	0.25 1784 0.25 1789	0.25 1783	0.25
1786 1791	0.25 1787 0.25 1792	0.25 1788	0.25 1789	0.05 1795	0.05
1796	0.05 1797	0.05 1798	0.05 1799	0.05 1800	0.05
1801	0.05 1802	0.05 1803	0.05 1804	0.05 1805	0.05
1806	0.05 1807	0.05 1808	0.05 1809	0.25 1810	0.25
1811	0.25 1812	0.25 1813	0.25 1814	0.25 1815	0.25
1816	0.25 1817	0.25 1818	0.25 1819	0.25 1820	0.25
1821	0.25 1822	0.05 1823 0.25 1828	0.05 1824 0.25 1829	0.05 1825 0.25 1830	0.05 0.25
1826	0.05 1827 0,25 1832	0.25 1828	0.25 1829	0.25 1835	0.25
1831 1836	0.25 1837	0.25 1838	0.25 1839	0.25 1840	0.25
1841	0.25 1842	0.25 1843	0.25 1844	0.25 1845	0.25
1846	0.25 1847	0.25 1848	0.25 1849	0.05 1850	0.05
1851	0.05 1852	0.05 1853	0.05 1854	0.05 1855	0.05
1856	0.05 1857	0.05 1858	0.05 1859	0.05 1860	0.05
1861	0.05 1862	0.05 1863	0.05 1864	0.25 1865	0.25
1866	0.25 1867	0.25 1868	0.25 1869 0.25 1874	0.25 1870 0.25 1875	0.25 0.25
1871 1876	0.25 1872 0.25 1877	0.25 1873 0.25 1878	0.25 1874	0.25 1875	0.25
1881	0.05 1882	0.25 1883	0.25 1884	0.25 1885	0.25
1886	0.25 1887	0.25 1888	0.25 1889	0.05 1890	0.05
1891	0.25 1892	0.05 1893	0.25 1894	0.25 1895	0.25
1896	0.25 1897	0.25 1898	0.25 1899	0.25 1900	0.25
1901	0.25 1902	0.25 1903	0.25 1904	0.05 1905 0.05 1910	0.05
1906	0.05 1907 0.05 1912	0.05 1908 0.05 1913	0.05 1909 0.05 1914	0.05 1910	0.05
1911 1916	0.05 1912	0.05 1913	0.05 1919	0.25 1920	0.25
1921	0.25 1922	0.25 1923	0.25 1924	0.25 1925	0.25
1926	0.05 1927	0.05 1928	0.05 1929	0.05 1930	0.05
1931	0.05 1932	0.05 1933	0.05 1934	0.05 1935	0.05
1936	0.25 1937	0.25 1938	0.25 1939	0.25 1940	0.25
1941	0.25 1942	0.25 1943	0.25 1944 0.25 1949	0.05 1945 0.25 1950	0.05 0.25
1946 1951	0.05 1947	0.25 1948 0.25 1953	0.25 1949	0.25 1955	0.25
1956	0.25 1957	0.25 1958	0.05 1959	0.05 1960	0.25
1961	0.05 1962	0.05 1963	0.05 1964	0.05 1965	0.05
1966	0.05 1967	0.05 1968	0.05 1969	0.05 1970	0.05
1971	0.05 1972	0.05 1973	0.05 1974	0.25 1975	0.25
1976	0.25 1977	0.25 1978	0.25 1979	0.25 1980	0.25 0.05
1981	0.25 1982 0.05 1987	0.05 1983 0.05 1988	0.05 1984 0.05 1989	0.05 1985 0.05 1990	0.05
1986 1991	0.05 1987	0.05 1988	0.25 1994	0.25 1995	0.25
1996	0.25 1997	0.25 1998	0.25 1999	0.25 2000	0.25
2001	0.05 2002	0.25 2003	0.25 2004	0.25 2005	0.25
2006	0.25 2007	0.25 2008	0.25 2009	0.25 2010	0.25
2011	0.05 2012	0.25 2013	0.05 2014	0.05 2015	0.05
2016	0.05 2017	0.05 2018	0.05 2019	0.05 2020 0.05 2025	0.05 0.05
2021	0.05 2022	0.05 2023 0.05 2028	0.05 2024 0.05 2029	0.05 2025	0.05
2026 2031	0.05 2027 0.25 2032	0.05 2028	0.05 2029	0.05 2035	0.03
2036	0.25 2032	0.25 2038	0.25 2039	0.05 2040	0.05
2041	0.05 2042	0.05 2043	0.05 2044	0.05 2045	0.05
2046	0.05 2047	0.25 2048	0.25 2049	0.25 2050	0.25
2051	0.25 2052	0.25 2053	0.25 2054	0.25 2055	0.25
2056	0.05 2057	0.05 2058	0.05 2059	0.25 2060	0.25
2061	0.25 2062	0.25 2063	0.25 2064	0.25 2065 0.05 2070	0.25 0.05
2066	0.05 2067 0.05 2072	0.05 2068 0.05 2073	0.25 2069 0.05 2074	0.05 2075	0.03
2071	0.03 2012	0.03 2013	0.03 20 /4	0.05 2015	9.20

2076	0.05 2077	0.05 2078	0.05 2079	0.05 2080	0.05
2081	0.05 2082	0.05 2083	0.05 2084	0.05 2085	0.05
2086	0.05 2087	0.05 2088	0.05 2089	0.25 2090	0.25
2091	0.25 2092	0.25 2093	0.25 2094	0.25 2095	0.25
2096	0.25 2097	0.05 2098	0.05 2099	0.05 2100	0.05
2101	0.05 2102	0.05 2103	0.05 2104	0.05 2105	0.05
2106	0.25 2107	0.25 2108	0.25 2109	0.25 2110	0.25
2111	0.25 2112	0.25 2113	0.05 2114	0.05 2115	0.05
2116	0.25 2112	0.25 2118			
2121	0.05 2122		0.25 2119	0.25 2120	0.25
		0.05 2123	0.05 2124	0.05 2125	0.05
2126	0.05 2127	0.05 2128	0.05 2129	0.05 2130	0.05
2131	0.05 2132	0.05 2133	0.25 2134	0.05 2135	0.05
2136	0.05 2137	0.25 2138	0.25 2139	0.25 2140	0.25
2141	0.25 2142	0.05 2143	0.05 2144	0.05 2145	0.05
2146	0.05 2147	0.05 2148	0.05 2149	0.05 2150	0.05
2151	0.05 2152	0.05 2153	0.25 2154	0.05 2155	0.05
2156	0.25 2157	0.25 2158	0.25 2159	0.25 2160	0.25
2161	0.25 2162	0.25 2163	0.25 2164	0.05 2165	0.05
2166	0.05 2167	0.05 2168	0.05 2169	0.05 2170	0.25
2171	0.05 2172	0.05 2173	0.05 2174	0.05 2175	0.05
2176	0.05 2177	0.05 2178	0.05 2179	0.05 2180	0.05
2181	0.05 2182	0.25 2183	0.25 2184	0.05 2185	0.05
2186	0.05 2187	0.05 2188	0.05 2189	0.05 2190	0.05
2191	0.05 2192	0.05 2193	0.05 2194	0.05 2195	0.05
2196	0.05 2197	0.05 2198	0.05 2199	0.05 2200	0.25
2201	0.05 2202	0.25 2203	0.05 2204	0.25 2205	0.25
2206	0.05 2207	0.05 2208	0.05 2209	0.05 2210	0.05
2211	0.05 2212	0.05 2213	0.05 2214	0.05 2215	0.05
2216	0.05 2217	0.05 2218	0.05 2219	0.05 2220	0.05
2221	0.25 2222	0.25 2223	0.25 2224	0.25 2225	0.25
2226	0.25 2227	0.25 2228	0.25 2229	0.25 2223	0.25
2231	0.05 2232	0.05 2233	0.05 2234	0.05 2235	0.25
2236	0.05 2237	0.05 2238	0.05 2239	0.05 2233	0.05
2241	0.05 2242	0.05 2238	0.05 2239	0.05 2245	0.05
2246	0.05 2242	0.05 2248	0.05 2249	0.05 2243	0.05
2251	0.05 2252	0.05 2253	0.05 2254	0.05 2255	0.05
2256	0.05 2257	0.05 2258	0.05 2259	0.05 2255	0.05
2261	0.05 2262	0.05 2258	0.05 2259	0.05 2265	0.05
2266	0.05 2267	0.05 2268	0.05 2269	0.05 2203	0.05
2271	0.05 2272	0.05 2208	0.05 2274	0.05 2275	0.03
2276	0.05 2272	0.05 2278	0.05 2279	0.05 2275	
2281	0.05 2287	0.05 2278	0.05 2279	0.05 2285	0.05
2286	0.05 2282	0.05 2288	0.05 2289	0.05 2285	0.05
2291	0.25 2292	0.25 2293	0.25 2294	0.25 2290	0.25 0.25
2296	0.25 2292	0.25 2298	0.25 2294	0.25 2293	
2301	0.25 2297	0.05 2298	0.05 2299	0.05 2305	0.05 0.05
2306	0.05 2302	0.05 2308	0.05 2304	0.05 2303	0.05
2311	0.05 2307	0.05 2308	0.05 2314	0.05 2310	0.05
2316	0.05 2312	0.05 2318	0.05 2314	0.05 2313	0.05
2321	0.05 2317	0.05 2318	0.05 2319	0.05 2325	0.05
2326	0.05 2322	0.05 2328	0.05 2329	0.05 2323	0.05
2331	0.05 2327	0.05 2328	0.05 2329	0.05 2335	0.05
2336	0.05 2332	0.05 2338	0.05 2339	0.05 2340	0.05
2341	0.05 2342	0.05 2343	0.05 2334	0.05 2345	0.05
2346	0.05 2347	0.05 2348	0.05 2349	0.05 2343	0.05
2351	0.05 2352	0.05 2348	0.05 2349	0.05 2355	0.03
2356	0.25 2357	0.25 2358	0.25 2359	0.25 2360	0.25
2361	0.25 2362	0.25 2363	0.05 2364	0.25 2365	0.25
2366	0.05 2367	0.05 2368	0.05 2369	0.05 2370	
2371	0.05 2372	0.05 2373	0.05 2374	0.05 2375	0.05
2376	0.05 2372	0.05 2378	0.05 2374	0.05 2373	
2381	0.05 2377	0.05 2378	0.05 2379		0.05
2386	0.05 2382		0.05 2389	0.05 2385	0.05
2391		0.05 2388		0.05 2390	0.05
2396	0.05 2392	0.05 2393 0.05 2398	0.05 2394	0.05 2395	0.05
	0.05 2397 0.05 2402		0.05 2399 0.05 2404	0.05 2400	0.05
2401 2406	0.05 2402	0.05 2403		0.05 2405	0.05
		0.05 2408	0.05 2409	0.05 2410	0.05
2411 2416	0.05 2412 0.05 2417	0.05 2413	0.05 2414 0.25 2419	0.05 2415	0.05
		0.25 2418		0.25 2420	0.25
2421	0.25 2422	0.25 2423	0.25 2424	0.25 2425	0.25
2426	0.25 2427	0.25 2428	0.05 2429	0.05 2430	0.25
2431	0.05 2432	0.05 2433	0.05 2434	0.05 2435	0.05
2436	0.05 2437	0.05 2438	0.05 2439	0.05 2440	0.05
2441	0.05 2442	0.05 2443	0.05 2444	0.05 2445	0.05
2446	0.05 2447	0.05 2448	0.05 2449	0.05 2450	0.05
2451	0.05 2452	0.05 2453	0.05 2454	0.05 2455	0.05
2456	0.05 2457	0.05 2458	0.05 2459	0.05 2460	0.05
2461	0.05 2462	0.05 2463	0.05 2464	0.05 2465	0.05
2466	0.05 2467	0.05 2468	0.05 2469	0.05 2470	0.05
2471	0.05 2472	0.05 2473	0.05 2474	0.05 2475	0.05
2476	0.05 2477	0.05 2478	0.25 2479	0.25 2480	0.25
2481	0.25 2482	0.25 2483	0.25 2484	0.25 2485	0.25
2486	0.25 2487	0.25 2488	0.25 2489	0.05 2490	0.25

2491	0.05 2492	0.05 2493	0.05 2494	0.05 2495	0.05
2496	0.05 2497	0.05 2498	0.05 2499	0.05 2500	0.05
2501	0.05 2502	0.05 2503	0.05 2504	0.05 2505	0.05
2506	0.05 2507	0.05 2508	0.05 2509	0.05 2510	0.05
2511	0.05 2512	0.05 2513	0.05 2514	0.05 2515	0.05
2516	0.05 2517	0.05 2518	0.05 2519	0.05 2520	0.05
2521	0.05 2522	0.05 2523	0.05 2524	0.05 2525	0.05
2526	0.05 2527	0.05 2528	0.05 2529	0.05 2530	0.05
2531	0.05 2532	0.05 2533	0.05 2534	0.05 2535	0.05
2536	0.05 2537	0.25 2538	0.25 2539	0.25 2540	0.25
2541	0.25 2542	0.25 2543	0.25 2544	0.25 2545	0.25
2546	0.25 2547	0.05 2548	0.05 2549	0.05 2550	0.05
2551	0.05 2552	0.05 2553	0.05 2554	0.05 2555	0.05
2556	0.05 2557	0.05 2558	0.05 2559	0.05 2560	0.05
2561	0.05 2562	0.05 2563	0.05 2564	0.05 2565	0.05
2566	0.05 2567	0.05 2568	0.05 2569	0.05 2570	0.05
2571	0.05 2572	0.05 2573	0.05 2574	0.05 2575	0.05
2576	0.05 2577	0.05 2578	0.05 2579	0.05 2580	0.05
2581	0.05 2582	0.05 2583	0.05 2584	0.05 2585	0.05
2586	0.05 2587	0.05 2588	0.05 2589	0.05 2590	0.05
2591	0.05 2592	0.05 2593	0.05 2594	0.25 2595	0.25
2596	0.25 2597	0.25 2598	0.25 2599	0.25 2600	0.25
2601	0.25 2602	0.25 2603	0.25 2604	0.05 2605	0.25
2606	0.05 2607	0.05 2608	0.05 2609	0.05 2610	0.05
2611	0.05 2612	0.05 2613	0.05 2614	0.05 2615	0.05
2616	0.05 2617	0.05 2618	0.05 2619	0.05 2620	0.05
2621	0.05 2622	0.05 2623	0.05 2624	0.05 2625	0.05
2626	0.05 2627	0.05 2628	0.05 2629	0.05 2630	0.05
2631	0.05 2632	0.05 2633	0.05 2634	0.05 2635	0.05
2636	0.05 2637	0.05 2638	0.05 2639	0.05 2640	0.05
2641	0.05 2642	0.05 2643	0.05 2644	0.05 2645	0.05
2646	0.05 2647	0.05 2648	0.25 2649	0.25 2650	0.25
2651	0.25 2652	0.25 2653	0.25 2654	0.25 2655	0.25
2656	0.25 2657	0.25 2658	0.05 2659	0.05 2660	0.05
2661	0.05 2662	0.05 2663	0.05 2664	0.05 2665	0.05
2666	0.05 2667	0.05 2668	0.05 2669	0.05 2670	0.05
2671	0.05 2672	0.05 2673	0.05 2674	0.05 2675	0.05
2676	0.05 2677	0.05 2678	0.05 2679	0.05 2680	0.05
2681	0.05 2682	0.05 2683	0.05 2684	0.05 2685	0.05
2686	0.05 2687	0.05 2688	0.05 2689	0.05 2690	0.25
2691	0.05 2692	0.05 2693	0.05 2694	0.05 2695	0.05
2696	0.05 2697	0.05 2698	0.25 2699	0.25 2700	0.25
2701	0.25 2702	0,25 2703	0.25 2704	0.25 2705	0.25
2706	0.25 2707	0.25 2708	0.05 2709	0.05 2710	0.05
2711	0.05 2712	0.05 2713	0.05 2714	0.05 2715	0.05
2716	0.05 2717	0.05 2718	0.05 2719	0.05 2720	0.05
2721	0.05 2722	0.05 2723	0.05 2724	0.05 2725	0.05
2726	0.05 2727	0.05 2728	0.05 2729	0.05 2730	0.05
2731	0.05 2732	0.05 2733	0.05 2734	0.05 2735	0.05
2736	0.05 2737	0.05 2738	0.05 2739	0.05 2740	0.05
2741	0.05 2742	0.05 2743	0.05 2744	0.05 2745	0.05
2746	0.05 2747	0.25 2748	0.25 2749	0.25 2750	0.25
2751	0.25 2752	0.25 2753	0.25 2754	0.25 2755	0.25
2756	0.05 2757	0.05 2758	0.05 2759	0.05 2760	0.05
2761	0.05 2762	0.05 2763	0.05 2764	0.05 2765	0.05
2766	0.05 2767	0.05 2768	0.05 2769	0.05 2770	0.05
2771	0.05 2772	0.05 2773	0.05 2774	0.05 2775	0.05
2776	0.05 2777	0.05 2778	0.05 2779	0.05 2780	0.05
2781	0.05 2782	0.05 2783	0.05 2784	0.05 2785	0.05
2786	0.05 2787	0.05 2788	0.05 2789	0.05 2790	0.05
2791	0.05 2792	0.05 2793	0.05 2794	0.25 2795	0.25
2796	0.25 2797	0.25 2798	0.25 2799	0.25 2800	0.25
2801	0.25 2802	0.05 2803	0.05 2804	0.05 2805	0.05
2806	0.05 2807	0.05 2808	0.05 2809	0.05 2810	0.05
2811	0.05 2812	0.05 2813	0.05 2814	0.05 2815	0.05
2816	0.05 2817	0.05 2818	0.05 2819	0.05 2820	0.05
2821	0.05 2822	0.05 2823	0.05 2824	0.05 2825	0.05
2826	0.05 2827	0.05 2828	0.05 2829	0.05 2830	0.05
2831	0.05 2832	0.05 2833	0.05 2834	0.05 2835	0.05
2836	0.05 2837	0.05 2838	0.05 2839	0.05 2840	0.05
2841	0.25 2842	0.25 2843	0.25 2844	0.25 2845	0.25
2846	0.25 2847	0.25 2848	0.05 2849	0.05 2850	0.05
2851	0.05 2852	0.05 2853	0.05 2854	0.05 2855	0.05
2856	0.05 2857	0.05 2858	0.05 2859	0.05 2860	0.05
2861	0.05 2862	0.05 2863	0.05 2864	0.05 2865	0.05
2866	0.05 2867	0.05 2868	0.05 2869	0.05 2870	0.05
2871	0.05 2872	0.05 2873	0.05 2874	0.05 2875	0.05
2876	0.05 2877	0.05 2878	0.05 2879	0.05 2880	0.05
2881	0.05 2882	0.05 2883	0.05 2884	0.05 2885	0.05
2886	0.05 2887	0.05 2888	0.05 2889	0.05 2890	0.05
2891	0.25 2892	0.25 2893	0.05 2894	0.05 2895	0.05
2896	0.05 2897	0.05 2898	0.05 2899	0.05 2900	0.05
2901	0.05 2902	0.05 2903	0.05 2904	0.05 2905	0.05
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2906	0.05 2907	0.05 2908	0.05 2909	0.05 2910	0.05
2911	0.05 2912	0.05 2913	0.05 2914	0.05 2915	0.05
2916	0.05 2917	0.05 2918	0.05 2919	0.05 2920	0.05
2921	0.05 2922	0.05 2923	0.05 2924	0.05 2925	0.05
2926	0.05 2927	0.05 2928	0.05 2929	0.05 2930	0.05
2931	0.05 2932	0.05 2933	0.05 2934	0.05 2935	0.05
2936	0.25 2937	0.05 2938	0.05 2939	0.05 2940	0.05
2941	0.05 2942	0.05 2943	0.05 2944	0.05 2945	0.05
2946	0.05 2947	0.05 2948	0.05 2949	0.05 2950	0.05
2951	0.05 2952	0.05 2953	0.05 2954	0.05 2955	0.05
2956	0.05 2957	0.05 2958	0.05 2959	0.05 2960	0.05
2961	0.05 2962	0.05 2963	0.05 2964	0.05 2965	0.05
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2971	0.05 2972	0.05 2973	0.05 2974	0.05 2975	0.05
2976	0.05 2977	0.05 2978	0.05 2979	0.05 2980	0.05
2981 2986	0.05 2982	0.05 2983	0.05 2984	0.05 2985	0.05
2991	0.05 2987 0.05 2992	0.05 2988 0.05 2993	0.05 2989	0.05 2990 0.05 2995	0.05
2996	0.05 2992	0.05 2998	0.05 2994 0.05 2999		0.05
3001	0.05 2997	0.05 2998	0.05 2999	0.05 3000	0.05
3006	0.05 3002	0.05 3008	0.05 3004	0.05 3005 0.05 3010	0.05
3011	0.05 3007	0.05 3008	0.05 3009	0.05 3015	0.05
3016	0.05 3012	0.05 3018	0.05 3014	0.05 3015	0.05
3021	0.05 3022	0.05 3018	0.05 3019	0.05 3025	0.03
3026	0.05 3022	0.05 3028	0.05 3024	0.05 3025	0.25
3031	0.05 3032	0.05 3033	0.05 3034	0.05 3035	0.05
3036	0.05 3032	0.05 3038	0.05 3034	0.05 3040	0.05
3041	0.05 3042	0.05 3043	0.05 3044	0.05 3045	0.05
3046	0.05 3047	0.05 3048	0.05 3049	0.05 3050	0.05
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3056	0.05 3057	0.05 3058	0.05 3059	0.05 3060	0.05
3061	0.05 3062	0.05 3063	0.05 3064	0.25 3065	0.05
3066	0.05 3067	0.05 3068	0.05 3069	0.05 3070	0.05
3071	0.25 3072	0.05 3073	0.05 3074	0.05 3075	0.05
3076	0.05 3077	0.05 3078	0.05 3079	0.05 3080	0.05
3081	0.05 3082	0.05 3083	0.05 3084	0.05 3085	0.05
3086	0.05 3087	0.05 3088	0.05 3089	0.05 3090	0.05
3091	0.05 3092	0.05 3093	0.05 3094	0.05 3095	0.05
3096	0.05 3097	0.05 3098	0.05 3099	0.05 3100	0.05
3101	0.05 3102	0.05 3103	0.25 3104	0.05 3105	0.25
3106	0.25 3107	0.25 3108	0.25 3109	0.25 3110	0.25
3111	0.05 3112	0.05 3113	0.05 3114	0.05 3115	0.05
3116	0.05 3117	0.05 3118	0.05 3119	0.05 3120	0.05
3121 3126	0.05 3122 0.05 3127	0.05 3123	0.05 3124	0.05 3125	0.05
3131	0.05 3127	0.05 3128 0.05 3133	0.05 3129 0.05 3134	0.05 3130 0.05 3135	0.05
3136	0.05 3132	0.05 3138	0.05 3134	0.05 3133	0.05 0.05
3141	0.05 3137	0.25 3138	0.05 3139	0.05 3140	0.03
3146	0.25 3147	0.05 3148	0.05 3149	0.05 3150	0.25
3151	0.25 3152	0.05 3153	0.05 3154	0.05 3155	0.05
3156	0.05 3157	0.05 3158	0.05 3159	0.05 3160	0.05
3161	0.05 3162	0.05 3163	0.05 3164	0.25 3165	0.25
3166	0.25 3167	0.25 3168	0.25 3169	0.25 3170	0.25
3171	0.25 3172	0.25 3173	0.25 3174	0.25 3175	0.25
3176	0.05 3177	0.25 3178	0.25 3179	0.25 3180	0.25
3181	0.25 3182	0.05 3183	0.05 3184	0.05 3185	0.05
3186	0.05 3187	0.05 3188	0.05 3189	0.05 3190	0.05
3191	0.05 3192	0.05 3193	0.05 3194	0.05 3195	0.05
3196	0.05 3197	0.25 3198	0.25 3199	0.25 3200	0.25
3201 3206	0.25 3202	0.25 3203	0.25 3204	0.25 3205	0.25
	0.25 3207 0.25 3212	0.25 3208 0.25 3213	0.25 3209	0.25 3210	0.25
3211 3216	0.25 3212 0.05 3217	0.25 3213	0.05 3214 0.25 3219	0.05 3215	0.05
3221	0.05 3217	0.05 3218	0.25 3219	0.05 3220 0.05 3225	0.25
3226	0.05 3222	0.05 3228	0.05 3224	0.05 3223	0.05 0.25
3231	0.05 3227	0.05 3228	0.25 3229	0.25 3235	0.25
3236	0.25 3237	0.25 3238	0.25 3239	0.25 3233	0.25
3241	0.05 3242	0.05 3243	0.05 3244	0.05 3245	0.05
3246	0.05 3247	0.25 3248	0.25 3249	0.25 3250	0.05
3251	0.25 3252	0.05 3253	0.05 3254	0.05 3255	0.05
3256	0.05 3257	0.25 3258	0.05 3259	0.05 3260	0.05
3261	0.05 3262	0.05 3263	0.25 3264	0.25 3265	0.25
3266	0.25 3267	0.25 3268	0.05 3269	0.05 3270	0.05
3271	0.05 3272	0.05 3273	0.05 3274	0.25 3275	0.25
3276	0.25 3277	0.25 3278	0.25 3279	0.05 3280	0.25
3281	0.05 3282	0.05 3283	0.05 3284	0.05 3285	0.05
3286	0.05 3287	0.05 3288	0.05 3289	0.05 3290	0.05
3291	0.05 3292	0.05 3293	0.05 3294	0.05 3295	0.05
3296	0.05 3297	0.05 3298	0.05 3299	0.05 3300	0.05
3301	0.05 3302	0.05 3303	0.05 3304	0.05 3305	0.05
3306 3311	0.05 3307	0.05 3308	0.05 3309	0.05 3310	0.05
3316	0.05 3312 0.05 3317	0.05 3313 0.05 3318	0.05 3314	0.05 3315	0.05
2210	0.03 331/	0.03 3318	0.05 3319	0.05 3320	0.05

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0.05 3323
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3321
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         0.05 3327
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3336
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                                        0.05 3344
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          0.05 3342
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                                                       0.05 3350
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          0.05 3347
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3346
                                        0.05 3354
                                                      0.05 3355
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3351
          0.05 3352
                         0.05 3353
                                        0.05 3359
                                                       0.05
3356
          0.05 3357
                         0.05 3358
INITIAL HEAD ARRAY: INP,SFCT (12,F10.0); NODE, HEAD (FT) (5(15,F10.0))
1 1.0000
                  2 5096.9222 3 5096.0072 4 5097.2566 5 5096.1058 7 5097.5197 8 5096.4103 9 5095.5517 10 5094.9426
  1 5096.6416
  6 5095,4489
                  12 5097,4000 13 5095,7237 14 5095,0452 15 5094,5582
  11 5098,1018
                  17 5098.7487 18 5097.1177 19 5095.8701 20 5095.1945
  16 5094.6151
                  22 5094.2898 23 5094.3969 24 5099.6407 25 5097.5819
  21 5094.7364
                  27 5095.4000 28 5094.8695 29 5094.4950 30 5093.8055
  26 5096.1891
                  32 5100.7049 33 5098.4969 34 5096.6158 35 5095.5290
  31 5094.0408
                  37 5094.6841 38 5094.2342 39 5093.0204 40 5093.4629
  36 5094.9972
                  42 5099.5577 43 5097.1556 44 5095.7473 45 5095.2060
  41 5101.2944
  46 5094.8395 47 5094.5189 48 5093.7911 49 5092.0584 50 5092.9724
  51 5102.0816 52 5100.5874 53 5098.1000 54 5096.1319 55 5095.3406 56 5095.0299 57 5094.7682 58 5094.2201 59 5093.4537 60 5091.9879
  61 5092.42 62 5102.5952 63 5101.3349 64 5100.1215 65 5097.2687
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71 5092,8689 72 5091,7190 73 5091,9577 74 5103,0545 75 5101,6677
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  86 5091.6292 87 5103.8159 88 5102.5153 89 5100.7280 90 5100.3641
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  206 5107.2048 207 5108.0794 208 5107.9904 209 5090.9245 210 5090.8125
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5125.8861 509 5120.0468 510 5119.2252 511 5117.9542 512 5118.0425 513 5116.4690 514 5116.3533 515 5114.4279 516 5113.7917 517 5117.4443 518 5121.7848 519 5124.9374 520 5125.2910 521 5112.8760 522 5112.7371 523 5113.2950 524 5111.9227 525 5112.3766 526 5111.0977 527 5111.5281 528 5112.0000 529 5111.2478 530 5111.2736 531 5111.3791 532 5111.5534 533 5111.8642 534 5111.6966 535 5111.7248 536 5111.6608 537 5111.6646 538 5111.7851 539 5112.0076 540 5111.9030 541 5111.7783 542 5112.2471 543 5113.5269 544 5113.5360 545 5113.2157 546 5112.6309 547 5111.4061 548 5113.4110 549 5117.5211 550 5117.8925 551 5126.5507 552 5125.6106 553 5125.9000 554 5126.5297 555 5128.7659 556 5130.9160 557 5132.8974 558 5134.1289 559 5132.8183 560 5129.2976 561 5125.2000 562 5126.3253 563 5124.8269 564 5124.1352 565 5123.0060 566 5121.6440 567 5120.0512 568 5119.2047 569 5118.9840 570 5127.3000 571 5127.9749 572 5127.4967 573 5118.0755 574 5118.3307 575 5116.9637 576 5116.7030 577 5115.3266 578 5114.5301 579 5114.2971 580 5113.0651 581 5112.9755 582 5112.4882 583 5112.6610 584 5112.6736 585 5112.5971 586 5113.1254 587 5112.2428 588 5112.6959 589 5113.0306 590 5113.6932 591 5113.8297 592 5113.7365 593 5113.1367 594 5115.1979 595 5115.5772 596 5115.5211 597 5113.1440 598 5112.0000 599 5115.2889 600 5117.8126 601 5118.3446 602 5130.6649 603 5128.8745 604 5128.4177 605 5129.2802 606 5131.3689 607 5133.4741 608 5135.0947 609 5137.6040 610 5139.2008 611 5137.6837 612 5136.5524 613 5135.7235 614 5134.9622 615 5132.4630 616 5131.6841 617 5128.7221 618 5127.5323 619 5125.2871 620 5124.7226 621 5121.4604 622 5128.4652 623 5130.7770 624 5131.7205 625 5123.9877 626 5124.1191 627 5123.6183 628 5122.9417 629 5121.1156 630 5119.9794 631 5118.8960 632 5118.4827 633 5117.2895 634 5117.1226 635 5115.9767 636 5116.1751 637 5115.2174 638 5115.6105 639 5115.0613 640 5115.0136 641 5115.1883 642 5114.3361 643 5114.1369 644 5117.9071 645 5116.8423 646 5117.4291 647 5117.1872 648 5115.6343 649 5112.4417 650 5116.9920 651 5118.5668 652 5118.8448 653 5135.6944 654 5133.7713 655 5132.3051 656 5131.7578 657 5133.0340 658 5134.7929 659 5137.2910 660 5140.2769 661 5148.5300 662 5143.4864 663 5143.5451 664 5143.8489 665 5142.5234 666 5142.2701 667 5140.4293 668 5136.8949 669 5135.6013 670 5131.6424 671 5131.5508 672 5129.2221 673 5124.6497 674 5131.7982 675 5137.0723 676 5137.2401 677 5130.6017 678 5129.5919 679 5129.2088 680 5129.0448 681 5126.2058 682 5124.7335 683 5123.0634 684 5122.4361 685 5120.6004 686 5120.0522 687 5118.6933 688 5118.0475 689 5117.3838 690 5116.8624 691 5118.0766 692 5117.1760 693 5116.1993 694 5115.2812 695 5120.7404 696 5119.5916 697 5119.7759 698 5119.7991 699 5117.0366 700 5115.4038 701 5117.2634 702 5119.7622 703 5119.3497 704 5139.2485 705 5137.3979 706 5136.0253 707 5134.9947 708 5134.7982 709 5136.3389 710 5138.2969 711 5140.9870 712 5144.4922 713 5147.4223 714 5148.4940 715 5148.6714 716 5147.2000 717 5147.6385 718 5144.9394 719 5144.0708 720 5142.9010 721 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    1.17280
              0.000
                      0.00
    2.05240
 26
              0.000
                      0.00
    2.34560
              0.000
                      0.00
 28
    4.03150
              0.000
 29
    15.97940
              0.000
                       0.00
 30
    0.03996
              0.000
                      0.00
 31
    30.19968
               0.000
                       0.00
 32 19.70567
              0.000
                       0.00
    0.51365
              0.000
                      0.00
 34 37.13810
               0.000
                       0.00
 35
    35.08466
               0.000
                       0.00
    34.76495
               0.000
 36
                       0.00
 37 30.76035
               0.000
                       0.00
 38 67.41947
               0.000
                       0.00
    0.01939
              0.000
                      0.00
    40.05722
               0.000
                       0.00
    94.80523
              0.000
                       0.00
    3.25534
              0.000
                      0.00
    6.87944
 43
              0.000
                      0.00
    3.39189
              0.000
                      0.00
    0.00667
              0.000
                      0.00
    -0.75715
              0.000
                      0.00
 47 -0.75715
              0.000
                      0.00
    -0.75715
              0.000
                      0.00
 49 -0.75715
              0.000
                      0.00
 50 -1.89467
              0.000
                      0.00
 51 -1.89467
              0.000
                      0.00
    -1.89467
              0.000
                      0.00
 53 -1.89467
              0.000
                      0.00
 54 -1.03401
              0.000
                      0.00
    -1.03401
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    -1.03401
              0.000
                      0.00
 57 -1.03401
              0.000
                      0.00
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58 0.00000	0.000	0.00
59 0.00000	0.000	0.00
60 -23.05097	0.000	0.00
61 -32.90975	0.000	0.00
62 7.42662	0.000	0.00
63 -12.03665	0.000	0.00
64 13.11146	0.000	0.00
65 -16.16509	0.000	0.00
66-131.29794	0.000	0.00
67 -51.27368	0.000	0.00
68 -74.93688 69 -47.20008	0.000	0.00
69 -47.20008	0.000	0.00
70 -33.12642	0.000	0.00
71 -16.89155	0.000	0.00
72 -10.22913	0.000	0.00
73 1.10799	0.000	0.00
74 -0.40557	0.000	0.00
75 -1.28843	0.000	0.00
76 2.28924	0.000	0.00
77 -3.03639	0.000	0.00
78 -0.18435	0.000	0.00
79 1.53042	0.000	0.00
80 -0.24032	0.000	0.00
81 1.50910	0.000	0.00
82 0.76961	0.000	0.00
83 -0.20735	0.000	0.00
84 0.47021	0.000	0.00
85 1.74270	0.000	0.00
86 2.34524	0.000	0.00
87 3.92467	0.000	0.00
88 -0.90622	0.000	0.00
89 14.37600	0.000	0.00
90 -8.73412	0.000	0.00
91 -1.38269	0.000	0.00
92 0.33634	0.000	0.00
93 -3.32862	0.000	0.00
94 1.03531	0.000	0.00
95 -11.18642	0.000	0.00
96 -2.32159	0.000	0.00
97 -0.30986	0.000	0.00
98 -0.09587	0.000	0.00
99 -0.02074	0.000	0.00
100 -0.00151	0.000	0.00
101 0.00702	0.000	0.00
102 -0.02442	0.000	0.00
103 -0.09075	0.000	0.00
104 -0.20197 105 -0.19096	0.000	0.00
106 -0.59290	0.000	0.00
107 -0.82305	0.000	0.00
108 -1.44399	0.000	0.00
109 -2.08795	0.000	0.00
110 -1.41528	0.000	0.00
111 -2.09593	0.000	0.00
112 -1.23989	0.000	0.00
113 -0.97725	0.000	0.00
114 -1.46235	0.000	0.00
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116 -0.36533	0.000	0.00
117 0.06802	0.000	0.00
118 -0.13435	0.000	0.00
119 0.22637	0.000	0.00
120 -0.00942	0.000	0.00
121 -0.13265	0.000	0.00
122 0.16430	0.000	0.00
123 0.02671	0.000	0.00
124 -0.02792	0.000	0.00
125 0.03127	0.000	0.00
126 -0.00940	0.000	0.00
127 -0.04960	0.000	0.00
128 0.07216	0.000	0.00
129 0.03457	0.000	0.00
130 0.01848	0.000	0.00
131 0.03328	0.000	0.00
132 -0.02891	0.000	0.00
133 -0.02201	0.000	0.00
134 -0.00408	0.000	0.00
135 0.01442 136 38.95630		0.00
136 38.95630 137 -0.03792	0.000	0.00
137 -0.03792		
139 0.02185	0.000	0.00
140 4.08017	0.000	0.00
170 4.0001/	0.000	0.00

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 142 -9.77792
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 143 0.03035
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 144 -8.18122
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 145 0.01095
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 146 -9.97479
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 147 -0.07544
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 148 -3.49700
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 149 -0.00732
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 150 -3.47277
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 151 0.00342
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 153 -0.01941
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 154 -0.82363
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 155 -0.11265
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                          0.00
 156 -0.21490
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                          0.00
 157 -0.28868
                 0.000
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 158 -0.05096
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 159 -0.30613
                 0.000
                          0.00
 160 0.16872
                 0.000
                          0.00
 161 -0.22511
                 0.000
                          0.00
 162 -0.03323
                 0.000
                          0.00
 163 -0.18955
                 0.000
                          0.00
 164 -0.22527
                 0.000
                          0.00
 165 -0.19265
                 0.000
                          0.00
GHB CONDITIONS: NUMBS (15)
OBSERVED HEAD DATA(WELL NODEID, OBSERVED HEAD)(I10, F10.0)
 74
  22012 5143,470
   22025 5109.180
   22043 5091.860
   22049 5110.010
   22052 5090.260
   22054 5111.380
   23013 5138.240
  23058 5139.100
  23085 5138.250
  23096 5138.970
  23122 5135.630
23134 5138.180
23135 5144.100
23150 5138.050
23179 5139.860
  23182 5112.840
  23185 5139.990
  23188 5138.700
  23191 5139.980
   23223 5137.200
  24010 5139.590
  24092 5139.240
  24122 5155.854
  24200 5137.560
  25022 5212.730
  25022 5212.750
25028 5179.110
26010 5161.760
26015 5145.660
26017 5145.450
26020 5148.650
  26040 5147.030
26041 5145.790
  26046 5145.680
  26049 5150.880
  26050 5156.920
  26062 5162.270
  26063 5183.150
  26065 5161.120
  26068 5159.030
  26073 5176.060
  26076 5151.410
  26081 5147.430
26083 5152.550
  26085 5178.840
  26088 5142.300
  26124 5154.410
  26133 5146.720
  26143 5173.800
  26159 5199.750
  26160 5144.460
  26166 5151.110
  26168 5155.800
  26169 5148.270
  26170 5141.820
```

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26173 5148.600
   27003 5097.810
   27017 5147.630
   27019 5148.060
   27024 5124.790
   27040 5119.700
  27040 5119.700
27041 5112.720
27051 5128.390
27056 5097.330
27059 5126.410
27064 5093.250
   27072 5095.750
   27073 5097.930
   27080 5119.070
   27084 5135.820
   35031 5173.220
   35040 5164.400
   35048 5216.270
   35079 5199.060
   35091 5182.040
UPDATES FOR PUMPING PERIOD # 2
  PINT PRINTIT CHANGEM (F10.0,4X,A1,1X,A4)
   90.00 Y BOTH
  NODEID REC DRCOND DRELEV (I5,3F10.0) 1 0.00000 0.000 0.000
     0.00000
                 0.000
                           0.00
     0.00000
0.00000
                  0.000
                           0.00
                  0.000
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      0.00000
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      0.00000
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7
      0.00000
                  0.000
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      0.00000
                  0.000
                            0.00
      0.00000
                  0.000
                            0.00
  10
      0.00000
                  0.000
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      0.00000
                  0.000
                            0.00
  11
      0.00000
                  0.000
                            0.00
  13
      0.00000
                  0.000
                            0.00
      0.00000
1.30000
0.00000
0.25000
2.77500
                  0.000 \\ 0.000
                             0.00
                             0.00
  15
                   0.000
                             0.00
  16
                   0.000
                             0.00
  17
                   0.000
                             0.00
  18
      3.87500
                   0.000
                             0.00
  19
  20
      3.45000
                   0.000
                             0.00
  21
      05.80000
                   0.000
                              0.00
  22
23
      07.55000
                   0.000
                              0.00
      11.43480
                   0.000
                             0.00
      1.43480
1.24610
1.17280
2.05240
2.34560
4.03150
15.97940
  24
25
26
27
28
29
                   0.000
                             0.00
                   0.000
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                             0.00
                  0.000 \\ 0.000
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                   0.000
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                   0.000
                             0.00
  30
      0.02058
                   0.000
                             0.00
  31 36.86463
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                              0.00
  32 24.46959
                   0.000
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  33
      0.00000
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      7.51994
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                              0.00
  37 30.89646
38 77.76269
39 0.02205
40 2.54340
41 95.52829
                   0.000
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                             0.00
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      2.27906
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                             0.00
   43
       4.81629
                   0.000
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      2.37466
                   0.000
                              0.00
   45 0.03000
                   0.000
                             0.00
   46 -0.58528
                   0.000
                              0.00
   47 -0.58528
                   0.000
                              0.00
                             0.00
0.00
   48 -0.58528
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   49 -0.58528
                   0.000 \\ 0.000
  50 -1.46459
51 -1.46459
52 -1.46459
53 -1.46459
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                   0.000
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   54 -0.79929
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   57 -0.79929
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60 -23.10441 0.000 0.00 61 -32.98300 0.000 0.00 62 7.22125 0.000 0.00 63 -12.17736 0.000 0.00 64 12.89926 0.000 0.00 65 -16.47956 0.000 0.00 66-131.70788 0.000 0.00 67 -51.75439 0.000 68 -75.43665 0.000 0.00 69 -47.76448 0.000 0.0070 -33.54935 0.0000.00 71 -17.21722 0.000 0.00 72 -10.51823 0.000 0.0073 0.90592 74 -0.62149 0.000 0.00 0.000 0.00 75 -1.53413 0.000 0.00 76 2.28684 0.000 0.00 77 -3.07490 0.000 0.00 78 -0.30108 0.000 0.00 79 1.40027 0.000 0.00 80 -0.26193 0.000 0.00 1.41266 0.000 0.00 82 0.69999 0.000 0.00 -0.25962 0.000 83 0.00 0.46693 0.000 0.00 85 1.77473 0.000 0.00 2.40992 86 0.000 0.00 4.03353 0.000 0.00 88 -0.88352 0.000 0.00 89 13.98297 0.000 0.00 90 -8.64160 0.000 0.00 91 -1.46789 0.000 0.00 92 0.23492 0.000 0.00 93 -3.41963 0.000 0.00 94 0.91972 95 -11.76557 0.000 0.00 0.000 0.00 96 -2.51123 97 -0.33915 0.000 0.000.000 0.00 98 -0.12151 0.000 0.00 99 -0.02259 0.000 0.00 100 -0.00195 0.000 0.00 101 0.00854 0.000 0.00 102 -0.02180 0.000 0.00 103 -0.08627 0.000 0.00 104 -0.18999 0.000 0.00 105 -0.19146 0.000 0.00106 -0.67064 0.000 0.00 107 -0.95578 0.000 108 -1.53340 0.0000.00109 -2.08650 0.0000.00110 -1.28399 0.000 0.00 111 -1.86141 0.000 0.00 112 -1.04165 0.000 0.00 113 -0.97542 0.000 0.00 114 -1.41333 0.000 0.00 115 -0.47715 0.000 0.00 116 -0.30227 0.0000.00 117 0.13341 0.0000.00 118 -0.09126 0.0000.00 119 0.25947 0.0000.00120 0.01432 0.0000.000.000121 -0.11622 0.00122 0.18468 0.000 0.00 123 0.04034 0.000 0.00 124 -0.01680 0.000 0.00 125 0.04141 0.000 0.00 126 -0.00137 0.000 0.00 127 -0.04376 0.000 0.00128 0.07866 0.000 0.00 129 0.04039 0.000 0.00 0.02082 130 0.000 0.00 0.03242 0.000 0.00 132 -0.03133 0.000 0.00 133 -0.02600 0.000 0.00 134 -0.01430 0.0000.00 135 0.00299 0.0000.00136 38.63945 0.000 0.00 137 -0.04397 0.0000.00138 -35.01601 0.000 0.00 139 0.02333 0.000 0.00140 3.31579 0.000 0.00 141 0.04310 0.000 0.00 142 -10.56950 0.000 0.00

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143 0.03033
                0.000
                         0.00
                         0.00
144 -8.79322
                0.000
145 0.00783
                0.000
                         0.00
                          0.00
146 -10.23647
                 0.000
147 -0.07204
                0.000
                         0.00
                         0.00
148 -3.60679
                0.000
149 0.00162
                         0.00
                0.000
                0.000
                         0.00
150
     -3.50922
151 0.00566
                0.000
                         0.00
     -1.88993
                0.000
                         0.00
152
153 -0.02974
                0.000
                         0.00
154 -0.88228
                         0.00
                0.000
155 -0.13993
                0.000
                         0.00
156 -0.24174
                0.000
                         0.00
 157 -0.33718
                0.000
                         0.00
 158 -0.06852
                0.000
                         0.00
 159 -0.35708
                0.000
                         0.00
 160 0.17013
                0.000
                         0.00
 161
     -0.27335
                0.000
                         0.00
 162 -0.04197
                0.000
                         0.00
 163 -0.23405
                0.000
                         0.00
 164 -0.25312
                0.000
                         0.00
                0.000 0.00
VPRM HDLEAK (I5,3F10.0)
 165 -0.23064
 EL.ID RECH. VPF
1 -0.0001 0.0000
                        0.00
    -0.0001
              0.0000
                        0.00
    -0.0001
              0.0000
                        0.00
    -0.0001
              0.0000
                        0.00
    -0.0001
              0.0000
                        0.00
  6
    -0.0001
              0.0000
                        0.00
     -0.0001
              0.0000
                        0.00
     -0.0001
              0.0000
                        0.00
     -0.0001
              0.0000
                        0.00
 10
     -0.0001
               0.0000
                         0.00
 31 -0.00127
                0.0000
                          0.00
 33 -0.00095
               0.0000
                         0.00
 35 -0.0000
65 -0.0121
               0.0000
                         0.00
               0.0000
                         0.00
UPDATES FOR PUMPING PERIOD # 3
  PINT PRINTIT CHANGEM (F10.0,4X,A1,1X,A4)
   90.00 Y BOTH
  NODEID REC DRCOND DRELEV (15,3F10.0)
     0.00000
                0.000
                        0.00
     0.00000
                0.000
                         0.00
     0.00000
                0.000
                         0.00
     0.00000
                0.000
                         0.00
     0.00000
                0.000
                         0.00
     0.00000
                0.000
                         0.00
     0.00000
                0.000
                         0.00
                         0.00
     0.00000
                0.000
                0.000
                         0.00
     0.00000
                0.000
                         0.00
  10
      0.00000
                0.000
                         0.00
      0.00000
                0.000
                         0.00
      0.00000
                 0.000
                          0.00
      0.00000
                0.000
                         0.00
      1.30000
                0.000
                         0.00
  16
      0.00000
                0.000
                          0.00
      0.25000
                          0.00
  17
                0.000
  17 0.23000
18 2.77500
19 3.87500
20 3.45000
21 05.80000
22 07.55000
                          0.00
                 0.000
                 0.000
                          0.00
                 0.000
                          0.00
                 0.000
                          0.00
                 0.000
                          0.00
  23
     11.43480
                 0.000
                          0.00
      1.24610
                 0.000
                          0.00
      1.17280
                 0.000
                          0.00
      2.05240
                 0.000
                          0.00
      2.34560
                 0.000
                          0.00
     4.03150
                          0.00
                 0.000
     15.97940
0.19274
33.04775
14.54943
  29
                 0.000
                          0.00
                          0.00
  30
                 0.000
                 0.000
  31
                           0.00
                 0.000
                           0.00
  32
      0.00147
  33
                 0.000
                          0.00
     41.06178
                 0.000
                           0.00
      0.03678
                 0.000
     28.92083
                  0.000
                           0.00
  36
     88.40443
                  0.000
                           0.00
     60.81731
                  0.000
                           0.00
  39 0.00000
                 0.000
                          0.00
  40 46.64159
                  0.000
                           0.00
                  0.000
                           0.00
  41 33.07129
```

42 2.52935 0.000 0.00 43 5.34522 0.000 0.00 44 2.63544 0.000 0.00 45 0.34000 0.000 0.00 46 -0.71898 0.000 0.00 47 -0.71898 0.000 0.00 48 -0.71898 0.000 0.00 49 -0.71898 0.000 0.00 50 -1.79915 0.000 0.00 51 -1.79915 0.000 0.00 52 -1.79915 0.000 0.00 53 -1.79915 0.000 0.00 54 -0.98188 0.0000.00 55 -0.98188 0.0000.00 56 -0.98188 0.0000.00 57 -0.98188 0.000 0.00 0.000 58 0.00000 0.00 59 0.00000 0.00 60 -22 88391 0.000 0.00 0.000 61 -32.69602 0.00 62 7.72661 63 -11.79272 0.000 0.00 0.000 0.00 64 13.31648 0.000 0.00 65 -16.02127 0.000 0.00 66-131.21848 0.00 0.000 0.000 67 -51.31587 0.00 68 -75.03797 0.0000.00 69 -47.36816 0.000 0.00 70 -33.23750 0.0000.00 0.000 71 -16.95750 0.00 72 -10.25068 0.000 0.00 73 1.17436 74 -0.27658 0.000 0.00 0.000 0.00 75 -1.07084 0.000 0.00 76 2.57730 0.000 0.00 77 -2.94757 0.000 0.00 78 -0.16336 0.000 0.00 1.51965 0.000 0.00 80 -0.13665 0.000 0.00 81 1.53121 0.000 0.00 0.79904 0.000 0.0083 -0.15677 0.0000.000.60121 84 0.000 0.001.94643 2.58615 85 0.0000.0086 0.000 0.00 87 4.21659 0.000 0.00 88 -0.74147 0.000 0.00 89 14.23038 0.000 0.00 90 -8.56693 0.000 0.00 -1.34039 0.000 0.00 0.37196 0.000 0.00 -3.28508 0.000 0.00 1.05341 0.000 0.00 95 -11.26855 0.000 0.0096 -2.21504 0.0000.0097 -0.18506 0.0000.0098 -0.05602 0.000 0.00 99 -0.00224 0.000 0.00 0.000 100 0.01838 0.00 101 0.03041 0.00 102 -0.00079 0.000 0.00 103 -0.06093 0.000 0.00 104 -0.15411 0.000 0.00 105 -0.15653 0.0000.00 106 -0.65339 0.00 0.000107 -0.93338 0.000 0.00 108 -1.47155 0.000 0.00 109 -1.96785 0.000 0.00 110 -1.11149 0.0000.00111 -1.68677 0.0000.00112 -0.90345 113 -0.96083 114 -1.36506 0.0000.00 $0.000 \\ 0.000$ 0.000.00 115 -0.42062 0.00 0.000 116 -0.24974 0.000 0.00 117 0.19012 0.000 0.00 118 -0.04424 0.000 0.00 119 0.30299 0.000 0.00 120 0.05118 0.000 0.00 -0.08671 0.000 0.00 0.22669 0.000 0.00 123 0.07738 0.0000.00 124 0.01878 0.0000.00

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125 0.07814
                0.000
                         0.00
126 0.03233
                0.000
                         0.00
                0.000
                         0.00
127 -0.01562
                0.000
                         0.00
128 0.11471
                0.000
                         0.00
129 0.07784
                0.000
130
     0.05755
                         0.00
131 0.05949
                0.000
                         0.00
132 -0.00982
                0.000
                         0.00
133 -0.00167
                0.000
                         0.00
134 0.01341
                0.000
                         0.00
135 0.02861
                0.000
                         0.00
136 39.19635
                0.000
                         0.00
137 -0.01628
                0.000
                         0.00
138 -33.73046
                 0.000
                          0.00
139 0.05476
                0.000
                         0.00
140 4.89590
                0.000
                         0.00
141 0.07699
                0.000
                         0.00
142 -8.84549
                0.000
                         0.00
143 0.05894
                0.000
                         0.00
144 -7.30433
                0.000
                         0.00
145 0.04155
146 -9.48743
147 -0.03417
148 -3.26882
149 0.04060
                0.000 \\ 0.000
                         0.00
                         0.00
                0.000
                         0.00
                0.000
                         0.00
                0.000
                         0.00
150 -3.39075
151 0.04195
                0.000
                         0.00
                0.000
                         0.00
152 -1.80363
                0.000
                         0.00
153 0.00156
                0.000
                         0.00
154 -0.82881
                 0.000
                          0.00
 155 -0.11060
                 0.000
                          0.00
 156 -0.21099
                 0.000
                          0.00
 157 -0.30121
                 0.000
                          0.00
                         0.00
                 0.000
 158 -0.03226
                0.000
 159 -0.32007
160 0.21661
161 -0.23617
162 0.00867
                         0.00
                 0.000
                          0.00
                          0.00
                 0.000
                 0.000
                          0.00
 163 -0.19588
 164 -0.21054
                 0.000
                          0.00
 165 -0.19116
                 0.000
                          0.00
 EL.ID RECH.
                  VPRM HDLEAK (15,3F10.0)
     -0.0005
              0.0000
                        0.00
     -0.0005
              0.0000
                         0.00
     -0.0005
              0.0000
                         0.00
     -0.0005
              0.0000
                         0.00
     -0.0003
              0.0000
                         0.00
     -0.0003
              0.0000
                         0.00
     -0.0003
-0.0003
-0.0003
              0.0000
                         0.00
                         0.00
               0.0000
              0.0000
                         0.00
 10 -0.0003
               0.0000
                         0.00
 31 -0.00167
                0.0000
                          0.00
 33 -0.00135
                0.0000
                          0.00
 35 -0.0000
               0.0000
                         0.00
     -0.0125
               0.0000
                         0.00
UPDATES FOR PUMPING PERIOD # 4
  PINT PRINTIT CHANGEM (F10.0,4X,A1,1X,A4)
  90.00 Y BOTH
NODEID REC DRCOND DRELEV (15,3F10.0)
1 0.00000 0.000 0.00
     0.00000
                         0.00
                0.000
     0.00000
                0.000
                         0.00
                0.000
     0.00000
                         0.00
     0.00000
                0.000
                         0.00
     0.00000
                0.000
                         0.00
     0.00000
                0.000
                         0.00
     0.00000
                0.000
                         0.00
     0.00000
                0.000
                         0.00
  10
      0.00000
                 0.000
                          0.00
  11
     0.00000
                 0.000
                         0.00
                0.000
  12
      0.00000
                          0.00
     0.00000
0.00000
  13
                 0.000
                          0.00
  14
      1.30000
                 0.000
                          0.00
  15
      0.00000
                 0.000
                          0.00
  16
  17
      0.25000
                 0.000
                          0.00
  18 2.77500
19 3.87500
                 0.000
                          0.00
                 0.000
                          0.00
      3.45000
                 0.000
                          0.00
  21 05.80000
                  0.000
                           0.00
  22 07.55000
                  0.000
                           0.00
  23 11.43480
                  0.000
                           0.00
```

24 1.24610 0.000 0.00 1.17280 0.000 0.00 26 2.05240 0.000 0.00 2.34560 0.000 4.03150 0.000 0.00 29 15.97940 0.0000.00 30 0.18829 0.0000.00 31 25.97548 0.000 0.00 32 0.00000 0.0000.00 33 0.00000 34 38.58411 0.000 0.00 0.000 0.00 35 0.00000 36 3.15367 0.000 0.00 0.000 0.00 37 52.50426 0.000 0.00 38 44.11461 0.000 0.00 39 42.30467 0.000 0.00 40 29.56212 0.000 0.00 41 6.16184 0.000 0.00 2.32960 0.000 0.00 43 4.92309 0.000 0.00 2.42731 0.000 0.00 45 0.03000 0.00 0.000 46 -0.74859 0.000 0.00 47 -0.74859 0.000 0.00 48 -0.74859 0.000 0.00 49 -0.74859 0.000 0.00 50 -1.87325 0.000 0.00 51 -1.87325 0.000 0.00 52 -1.87325 0.000 0.00 53 -1.87325 0.000 0.00 54 -1.02232 0.000 0.00 55 -1.02232 0.000 0.00 56 -1.02232 0.000 0.00 57 -1.02232 0.000 0.00 58 -118.5000 59 -127.9000 0.000 0.0060 -17.71239 0.0000.00 61 -22.12447 62 50.72384 0.0000.00 0.000 0.00 63 17.27286 64 35.22105 0.0000.00 0.000 0.0065 -1.34117 0.000 0.00 66-121.26754 0.00 0.000 67 -45.00870 0.000 0.00 68 -71.07982 0.000 0.00 69 -44.30846 0.000 0.00 70 -31.62340 0.000 0.00 71 -16.23601 0.000 0.00 -9.79893 0.000 0.00 73 1.49720 0.000 0.00 74 0.12815 0.000 0.00 75 -0.42506 0.000 0.0076 2.95559 0.000 0.00 -2.86587 77 0.0000.0078 -0.02110 0.0000.00 0.000 79 1.61913 0.00 80 -0.07500 0.000 0.00 81 1.61076 0.000 0.000.86090 0.000 0.00 -0.09300 83 0.000 0.00 0.68635 0.000 0.00 2.05889 0.000 0.00 2.69191 0.000 0.00 4.32885 0.000 0.00 -0.65747 0.000 89 14.60113 0.000 0.00 90 -8.60446 0.000 0.0091 -1.24765 0.000 0.0092 0.47570 0.0000.0093 -3.19278 0.0000.0094 1.15228 95 -10.84634 0.000 0.000.0000.00 -1.99252 0.000 0.00 96 -0.07599 0.000 0.00 -0.01265 98 0.000 0.00 0.01300 0.000 0.00 100 0.03294 0.000 0.00 101 0.04603 0.000 0.00 102 0.01340 0.000 0.00 103 -0.04176 0.0000.00104 -0.12707 0.0000.00 105 -0.12731 0.0000.00106 -0.62565 0.000 0.00

```
107 -0.88692
               0.000
                       0.00
108 -1.39383
               0.000
                        0.00
               0.000
                       0.00
109 -1.85832
110 -0.97858
               0.000
                        0.00
                        0.00
111 -1.56996
               0.000
112 -0.81940
               0.000
                        0.00
113 -0.95340
               0.000
                        0.00
114 -1.33726
               0.000
                        0.00
115 -0.38681
               0.000
                        0.00
116 -0.21748
               0.000
                        0.00
117 0.22642
               0.000
                        0.00
118 -0.01387
               0.000
                        0.00
119 0.33195
               0.000
                        0.00
120 0.07627
               0.000
                        0.00
121
    -0.06629
               0.000
                        0.00
122 0.25605
               0.000
                        0.00
123
     0.10376
               0.000
                        0.00
124
     0.04618
               0.000
                        0.00
125
     0.10832
               0.000
                        0.00
126
     0.06101
               0.000
                        0.00
127
     0.00873
               0.000
                        0.00
     0.14589
               0.000
                        0.00
128
               0.000
                        0.00
129
     0.11220
     0.08979
               0.000
                        0.00
130
     0.08157
               0.000
                        0.00
131
     0.00681
               0.000
                        0.00
132
133
     0.01894
                        0.00
               0.000
     0.03924
               0.000
                        0.00
134
135
     0.05227
               0.000
                        0.00
136 39.79051
                0.000
                        0.00
137 0.00875
               0.000
                        0.00
138 -32.39414
                0.000
                        0.00
139 0.08263
               0.000
                        0.00
140
     6.50840
               0.000
                        0.00
141 0.10681
               0.000
                        0.00
                        0.00
142
     -7.08708
                0.000
143 0.08303
144 -5.81684
                        0.00
               0.000
                0.000
                        0.00
145 0.07082
                0.000
                        0.00
     -8.77293
                0.000
                        0.00
146
147 -0.00244
                0.000
                        0.00
148 -2.95715
                        0.00
                0.000
149 0.07242
                0.000
                        0.00
150
     -3.29710
                0.000
                        0.00
151 0.07241
                0.000
                        0.00
152
     -1.73120
                0.000
                        0.00
153 0.02928
                0.000
                        0.00
154 -0.78648
                        0.00
                0.000
                0.000
                        0.00
155 -0.08276
                0.000
                        0.00
156 -0.18935
157 -0.26297
                0.000
                        0.00
158 -0.00479
                0.000
                        0.00
159 -0.28098
                0.000
                        0.00
 160 0.25095
                0.000
                        0.00
 161 -0.19811
                0.000
                        0.00
 162 0.04913
                0.000
                        0.00
 163 -0.15818
                0.000
                        0.00
 164 -0.17334
                0.000
                        0.00
 165 -0.15430
                0.000
                        0.00
 EL.ID RECH.
1 -0.0007 0
                 VPRM HDLEAK (15,3F10.0)
             0.0000
                       0.00
                       0.00
     -0.0007
              0.0000
     -0.0007
                       0.00
              0.0000
                       0.00
     -0.0007
              0.0000
     -0.0004
              0.0000
                        0.00
     -0.0004
              0.0000
                        0.00
     -0.0004
              0.0000
                        0.00
     -0.0004
              0.0000
                        0.00
     -0.0004
              0.0000
                        0.00
     -0.0004
 10
              0.0000
                        0.00
    -0.00187
-0.00155
 31
               0.0000
                         0.00
                        0.00
 33
               0.0000
     -0.0000
                        0.00
              0.0000
 35
     -0.0127
              0.0000
                        0.00
 65
UPDATES FOR PUMPING PERIOD # 5
  PINT PRINTIT CHANGEM (F10.0,4X,A1,1X,A4)
   90.00 Y BOTH
  NODEID REC DRCOND DRELEV (15,3F10.0)
               0.000
     0.00000
                        0.00
     0.00000
               0.000
                       0.00
     0.00000
               0.000
                        0.00
     0.00000
               0.000
                        0.00
                        0.00
     0.00000
               0.000
```

6 0.00000 0.000 0.00 0.00000 0.000 0.00 0.00000 0.0000.00 0.000000.000 0.00 10 0.00000 0.000 0.00 0.00000 0.000 11 0.00 0.00000 0.000 12 0.00 0.00000 0.000 13 0.00 0.00000 0.000 14 0.00 0.00000 0.000 0.00 15 0.00000 0.000 0.00 16 0.48920 0.000 0.00 17 0.00000 0.000 18 0.00 7.49010 19 0.000 0.00 20 0.48920 0.000 0.00 0.00000 0.000 0.00 0.03060 0.000 0.00 23 0.09170 0.000 0.00 0.09170 0.000 0.00 0.09170 0.000 0.00 0.09170 0.000 0.00 15.01090 0.000 0.00 0.00000 0.000 0.00 29 0.00000 0.000 0.00 0.20471 0.000 0.00 31 28.41458 0.000 0.00 32 22.42945 0.000 0.00 7.17198 33 0.000 0.00 34 42.55147 0.000 0.00 35 0.00000 0.000 0.00 36 2.14414 37 55.19799 0.000 0.00 0.0000.00 38 64.14255 0.0000.000.000 39 33,79919 0.0040 50.08436 0.00 17.32765 0.000 41 0.00 42 0.92288 0.000 0.00 5.39639 43 0.000 0.00 4.07741 44 0.000 0.00 45 1.13000 0.000 0.00 46 -1.19145 0.000 0.00 47 -1.19145 0.000 0.00 48 -1.19145 0.000 0.00 49 -1.19145 0.000 0.00 50 -1.39227 0.000 0.00 51 -1.39227 0.000 0.00 52 -1.39227 0.0000.0053 -1.39227 0.000 0.0054 -0.93545 55 -0.93545 0.0000.00  $0.000 \\ 0.000$ 0.0056 -0.93545 0.00 57 -0.93545 0.000 0.00 58 -80.5000 0.000 0.00 59 -146.4000 0.000 0.00 60 -18.51770 0.000 0.00 61 -23.56409 0.000 0.00 62 47.41259 0.000 0.00 63 15.35095 0.000 0.00 64 34.31006 0.000 0.00 65 -2.34470 0.000 0.00 66-122.19400 0.000 67 -45.76328 0.000 0.0068 -71.65788 0.0000.0069 -44.82061 70 -31.96739 71 -16.46625 0.000 0.00  $0.000 \\ 0.000$ 0.00 0.00 72 -10.00371 0.000 0.00 73 1.30624 0.000 0.00 74 -0.07701 0.000 0.00 75 -0.64529 0.000 0.00 76 2.69993 0.0000.0077 -3.00184 0.0000.0078 -0.22025 0.0000.00 79 1.45063 0.0000.00 80 -0.19831 0.000 0.00 1.46994 0.00 0.000 81 82 0.74520 0.00 0.000 -0.19792 83 0.000 0.00 0.59689 84 0.000 0.00 85 1.97730 0.000 0.00 2.59441 86 0.000 0.00 4.23060 0.0000.00 88 -0.76006 0.0000.00

```
89 14.28135
                0.000
 90 -8.65298
                0.000
                         0.00
    -1.39405
                0.000
                         0.00
 92 0.31116
                0.000
                         0.00
    -3.34841
                0.000
                         0.00
 94 0.99290
                0.000
                         0.00
 95 -11.46323
                0.000
                          0.00
96
    -2.26792
                0.000
                         0.00
97 -0.19606
                0.000
                         0.00
98 -0.07682
                         0.00
                0.000
99 -0.00372
100 0.01745
101 0.03180
102 0.00069
                0.000
                         0.00
                0.000
                          0.00
                          0.00
                0.000
                          0.00
                0.000
103 -0.05143
                 0.000
                          0.00
104 -0.13769
                 0.000
                          0.00
105 -0.15037
                 0.000
                          0.00
106 -0.66432
                 0.000
                          0.00
107 -0.93938
                 0.000
                          0.00
108 -1.44717
                 0.000
                          0.00
109 -1.90127
                 0.000
                          0.00
110 -1.01388
                 0.000
                          0.00
111 -1.60379
                 0.000
                          0.00
                          0.00
112 -0.86075
                 0.000
                 0.000
                          0.00
113 -0.96707
                 0.000
                          0.00
114 -1.36161
                 0.000
                          0.00
115 -0.40842
                          0.00
116 -0.23566
                 0.000
117 0.20981
118 -0.03072
                          0.00
                 0.000
                 0.000
                          0.00
                 0.000
                          0.00
119 0.31499
120 0.06079
                 0.000
                          0.00
121
     -0.07956
                 0.000
                          0.00
122
     0.23587
                 0.000
                          0.00
123
     0.08404
                 0.000
                          0.00
 124
     0.02925
                 0.000
                          0.00
 125
     0.09295
                 0.000
                          0.00
 126
     0.04730
                 0.000
                          0.00
     -0.00303
                          0.00
 127
                 0.000
128 0.12969
129 0.09626
130 0.06977
131 0.06301
                          0.00
                 0.000
                 0.000
                          0.00
                 0.000
                          0.00
                 0.000
                          0.00
     -0.01039
                 0.000
                          0.00
 132
 133 -0.00007
                 0.000
                           0.00
 134 0.01780
                 0.000
                           0.00
 135 0.03278
                 0.000
                           0.00
 136 48.45687
                  0.000
                           0.00
 137 -0.00969
                 0.000
                           0.00
 138 -18.91841
                  0.000
                           0.00
 139 0.06495
                 0.000
                           00.0
 140 8.40587
141 0.08947
                 0.000
                           0.00
                 0.000
                           0.00
     -4.91285
                 0.000
                           0.00
 142
 143 0.06648
                 0.000
                           0.00
     -4.83322
 144
                 0.000
                           0.00
 145 0.05237
                 0.000
                           0.00
 146 -8.63157
                 0.000
                           0.00
 147 -0.02273
                  0.000
 148 -3.01054
                 0.000
                           0.00
 149 0.05080
                 0.000
                           0.00
                 0.000
                           0.00
 150 -3.36621
 151 0.04903
152 -1.81056
153 0.00352
                 0.000
                           0.00
                 0.000
                           0.00
                 0.000
                           0.00
 154 -0.85614
                  0.000
                           0.00
 155 -0.11386
                           0.00
                  0.000
 156 -0.23077
                  0.000
                           0.00
 157 -0.30701
                  0.000
                           0.00
 158 -0.05082
                  0.000
 159 -0.32887
                  0.000
                           0.00
 160 0.20291
                  0.000
                           0.00
 161 -0.24634
                  0.000
                           0.00
 162 -0.00073
                  0.000
                           0.00
 163 -0.20574
                  0.000
                           0.00
                           0.00
 164 -0.21815
165 -0.19985
                  0.000
                  0.000
VPRM
                           0.00
                            HDLEAK (15,3F10.0)
  EL.ID RECH.
     -0.0003
               0.0000
                          0.00
     -0.0003
               0.0000
                          0.00
                0.0000
                          0.00
     -0.0003
     -0.0003
                0.0000
                          0.00
     -0.0002
                0.0000
                          0.00
```

```
6 -0.0002
              0.0000
                        0.00
     -0.0002
              0.0000
                        0.00
    -0.0002
              0.0000
                        0.00
    -0.0002
              0.0000
                        0.00
 10 -0.0002
              0.0000
                        0.00
 31 -0.00147
               0.0000
                        0.00
 33 -0.00115
               0.0000
                        0.00
 35 -0.0000
              0.0000
 65 -0.0123 0.0000
                        0.00
UPDATES FOR PUMPING PERIOD # 6
  PINT PRINTIT CHANGEM (F10.0,4X,A1,1X,A4)
  90.00 Y BOTH
NODEID REC DRCOND DRELEV (15,3F10.0)
  1 0.00000
              0.000
                       0.00
    0.00000
               0.000
                       0.00
    0.00000
               0.000
                       0.00
    0.00000
               0.000
                       0.00
    0.00000
               0.000
                       0.00
    0.00000
               0.000
                       0.00
    0.00000
               0.000
                       0.00
    0.00000
               0.000
                       0.00
    0.00000
               0.000
                       0.00
 10 0,00000
               0.000
                        0.00
    0.00000
               0.000
                        0.00
    0.00000
               0.000
                        0.00
 12
    0.00000
               0.000
                        0.00
 13
    0.00000
               0.000
                        0.00
 14
    0.00000
 15
               0.000
                        0.00
    0.00000
               0.000
                        0.00
 16
     0.35000
 17
               0.000
                        0.00
    0.35000
               0.000
 18
                        0.00
     6.80000
               0.000
                        0.00
 20
     7.00000
               0.000
                        0.00
 21
22
     1.60000
               0.000
                        0.00
    0.00000
               0.000
                        0.00
 23
    8.00000
               0.000
                        0.00
    0.00000
 24
               0.000
                        0.00
 25
    0.00000
               0.000
                        0.00
 26
27
    0.00000
               0.000
                        0.00
    0.00000
               0.000
                        0.00
 28
    1.00000
               0.000
                        0.00
 29
    0.65000
               0.000
                        0.00
 30 0.15706
               0.000
                        0.00
 31
    22.14596
               0.000
                        0.00
    25.45446
 32
               0.000
                        0.00
 33 19.70187
               0.000
                        0.00
    28.98331
               0.000
                        0.00
    0.86893
               0.000
                        0.00
    2.05765
               0.000
                        0.00
 37 59.49770
               0.000
                        0.00
 38 62.53163
               0.000
                        0.00
 39 28.37652
               0.000
                        0.00
 40 52.17334
               0.000
                        0.00
 41
    34.49748
               0.000
                        0.00
 42
    0.65835
               0.000
                        0.00
    3.84962
 43
               0.000
                        0.00
    2.90870
               0.000
                        0.00
 45
    2.59667
               0.000
                        0.00
 46 -1.50010
               0.000
                        0.00
 47 -1.50010
               0.000
                        0.00
 48 -1.50010
               0.000
                        0.00
 49 -1.50010
               0.000
                        0.00
 50 -1.75295
               0.000
                        0.00
51 -1.75295
52 -1.75295
               0.000
                        0.00
               0.000
                        0.00
53 -1.75295
54 -1.17778
               0.000
                        0.00
               0.000
                        0.00
 55 -1.17778
               0.000
                        0.00
 56 -1.17778
               0.000
                        0.00
 57 -1.17778
               0.000
                        0.00
 58 -85.6000
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# REPORT DOCUMENTATION PAGE

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### 13. SUPPLEMENTARY NOTES

#### 14. ABSTRACT

The groundwater flow system at Rocky Mountain Arsenal (RMA) is complex. To evaluate proposed remedial alternatives, interaction of the local groundwater flow system with the present contamination control systems must be understood. The purpose of this modeling effort is to provide a tool for evaluation and relative comparison of groundwater remedial alternatives. The model provides a method to assess the local groundwater impact of each remedial alternative. Results from the modeling effort will be used to compare the preliminary design of various remedial alternatives and allow general modification and reconfiguration of those designs to optimize their performance as part of the Detailed Analysis of Alternatives (DAA) of the Feasibility Study (FS).

Specific objectives of the modeling effort were developed based on the FS modeling needs established by RMA. Objectives are used to assist in defining the goals and associated scope of work of the modeling effort and address the need for modeling during the DAA of the FS, which requires comparison of remedial alternatives that have been retained. Objectives also allow for some flexibility in the analysis, such as combination or addition of remedial alternatives during subsequent phases of the FS.

(Continued)

15. SUBJECT TERMS					
Basin F		Rocky Mountain Arsenal			
Groundwater modeling	ng				
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a. REPORT	b. ABSTRACT	c. THIS PAGE			19b. TELEPHONE NUMBER (include area code)
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## 14. (Concluded)

This modeling effort accounts for groundwater flow in the upper Denver Fm. This approach differs from the majority of previous modeling efforts, which treat unsaturated alluvium areas as impermeable and do not address flow in the Denver Fm. Exchange of groundwater between the alluvium and the Denver Fm sands, basins, and precipitation infiltration is handled by areal inputs.

The model was calibrated by applying the existing concepts of flow in the modeled area to reproduce known water levels, groundwater discharge and recharge, and the flux through the aquifer system and across boundaries.

It is the intent of this modeling effort to incorporate all current pertinent hydrogeologic data into the model. Corrections to the RMA database and data from other ongoing modeling activities were incorporated when possible.